

Improvements in Distillation Design

SULZER
Sulzer Chemtech

Dan Summers | May 24, 2012



What is Distillation?

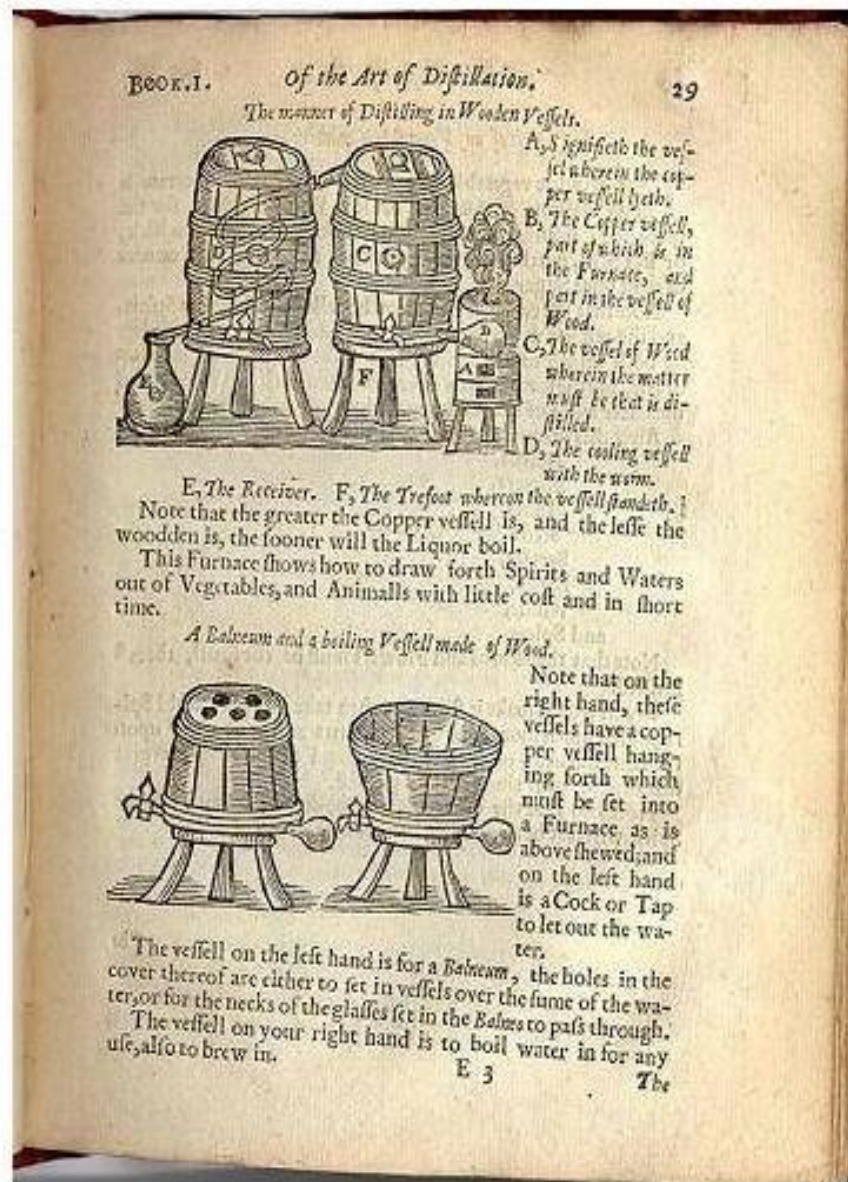
Distillation is purification of gases or liquids by "playing" with their boiling points.

The earliest known distillation was between ethanol and water

What is Distillation?



What is Distillation?



The Art of Distillation by John French 1651

What is Distillation?

"Strong Drink" (different than wine) mentioned in Old Testament nearly 20 times. People believe that some of these passages were written nearly 3500 years ago or 1500 BC.

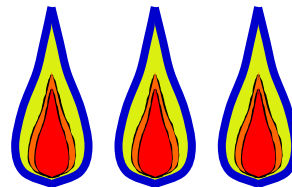
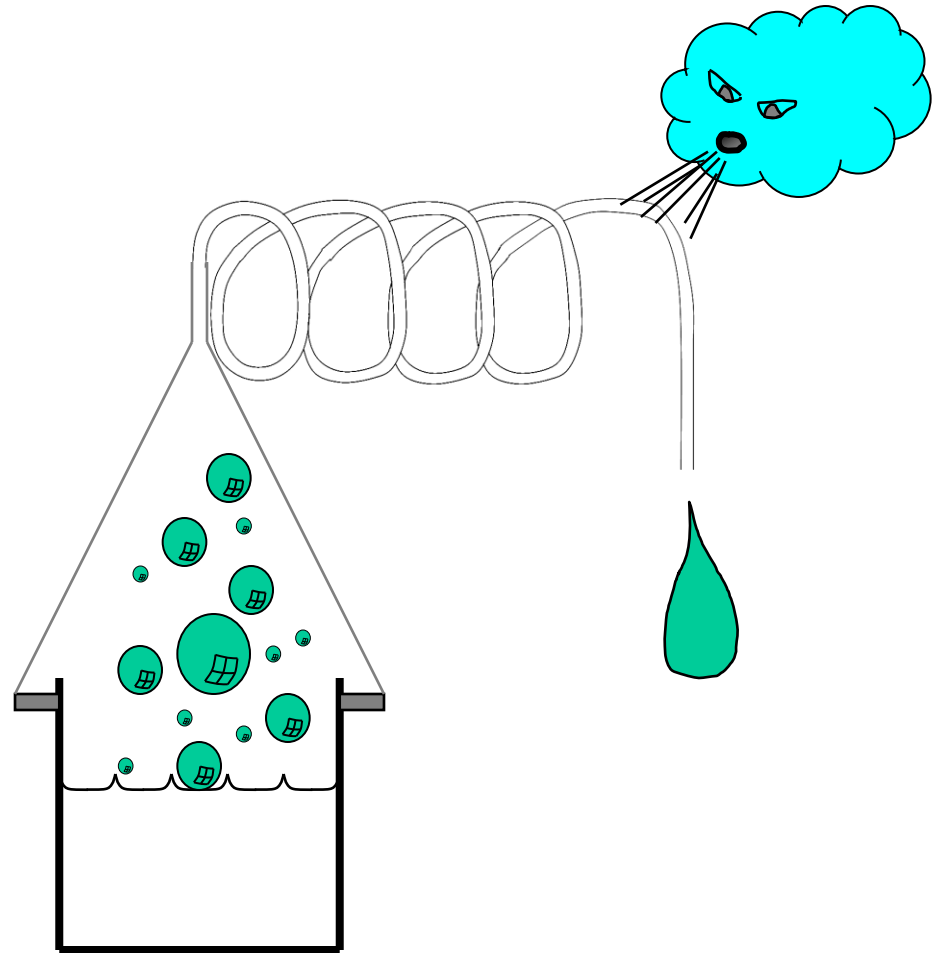
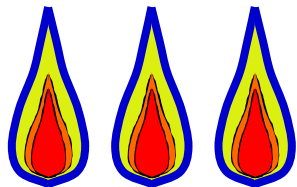
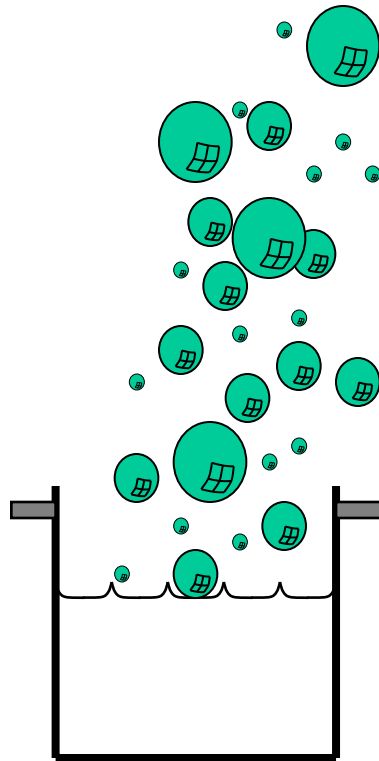
From Wikipedia you can find, "Distillation is a very old technique which was used by the Chinese in 3000 years BC."

I contend that Distillation must have preceded the more commonly referred to "World's Oldest Profession." (This is because the more common one wasn't really a profession until people realized it was wrong.)

What is Distillation?

Early Distillation was typically a single stage – or more simply a pot boiling with a condenser.

What is Distillation?

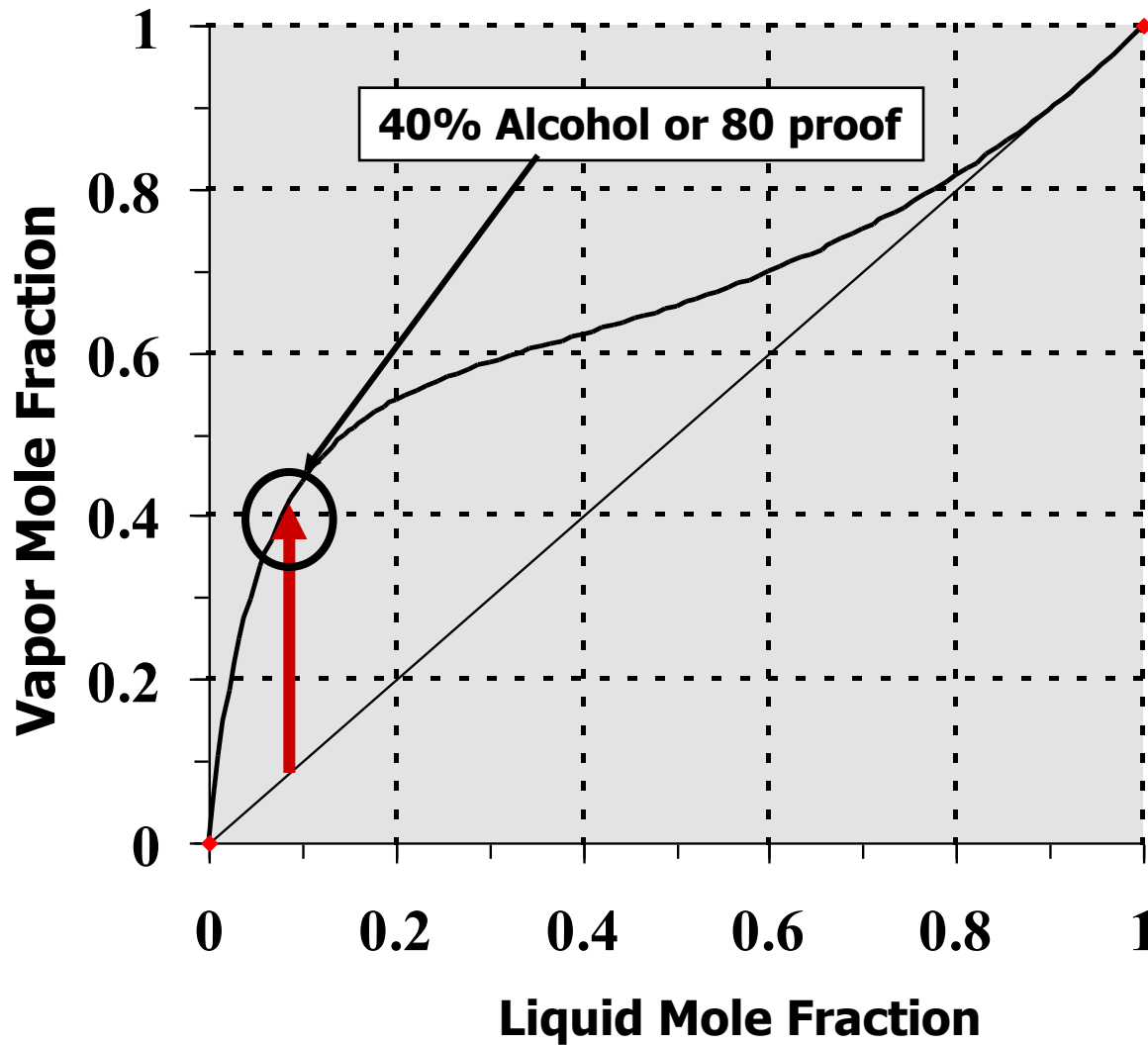


What is Distillation?

The composition of the overhead condensed vapors was found to have a much higher concentration of the lighter component.

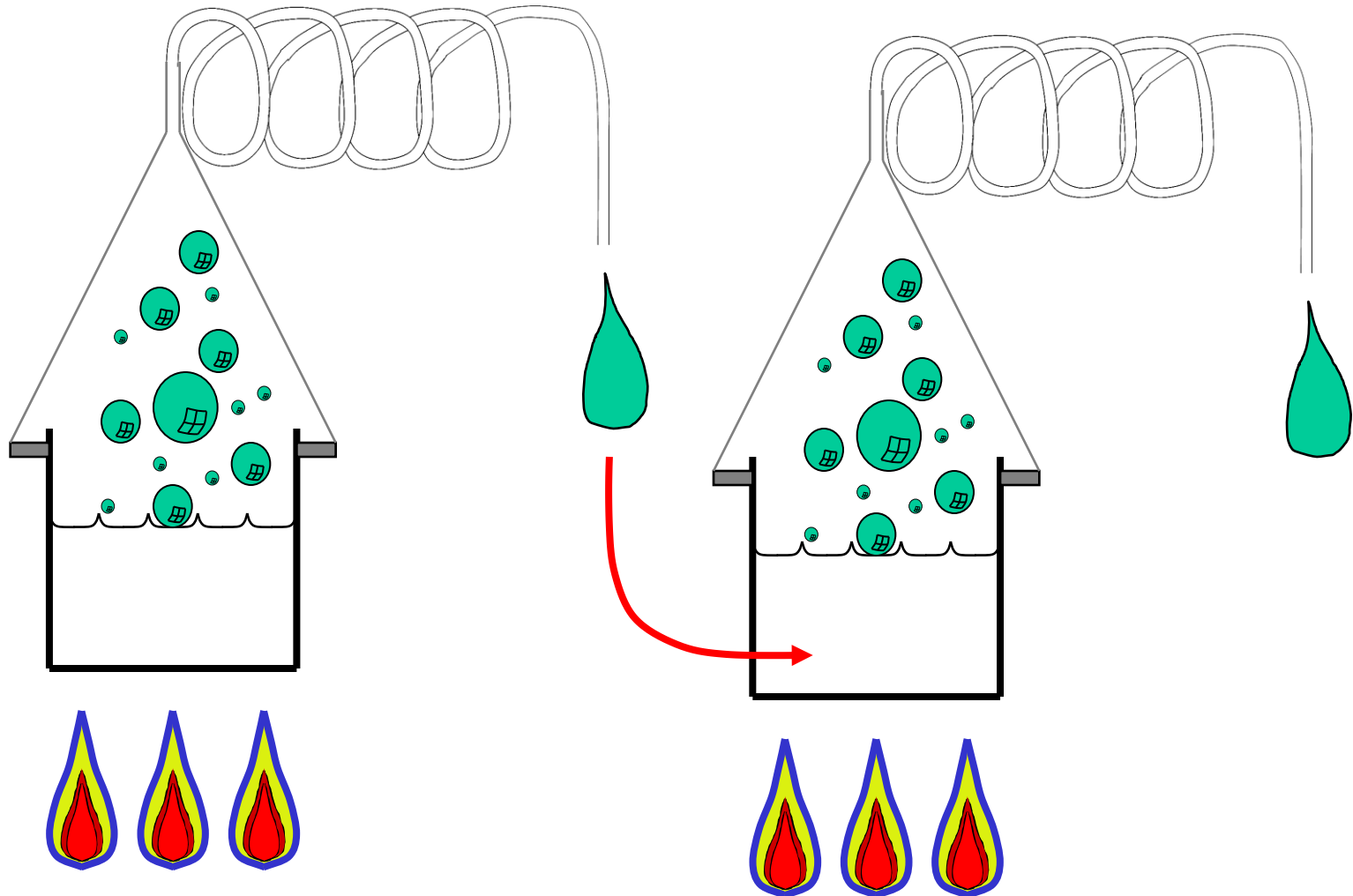
For example, a boiling pot of 6 to 8% ethanol has about 40% ethanol (80 proof) in the condensed vapors.

Ethanol and Water

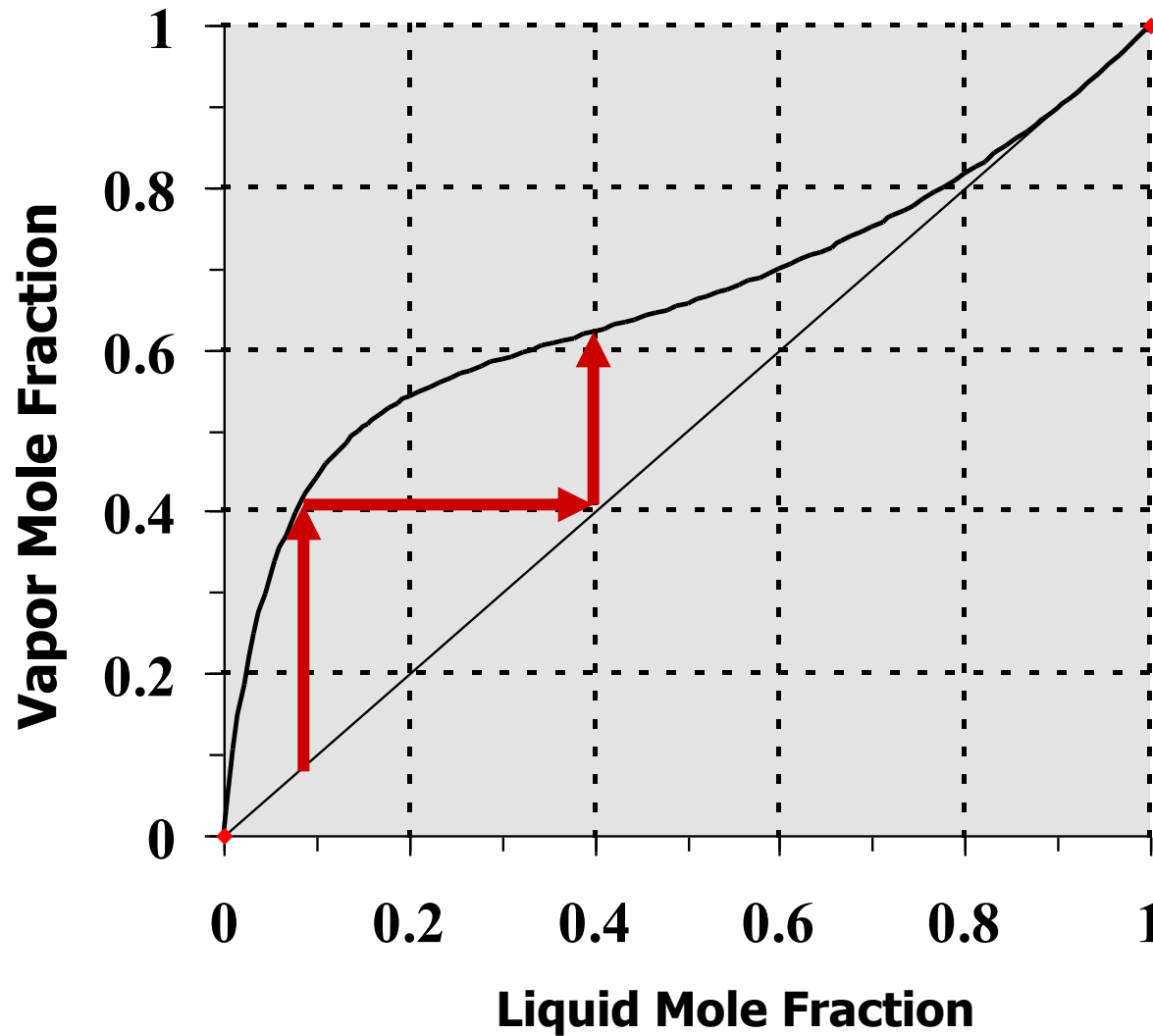


Pressure = 1 atm

What if you do this twice?



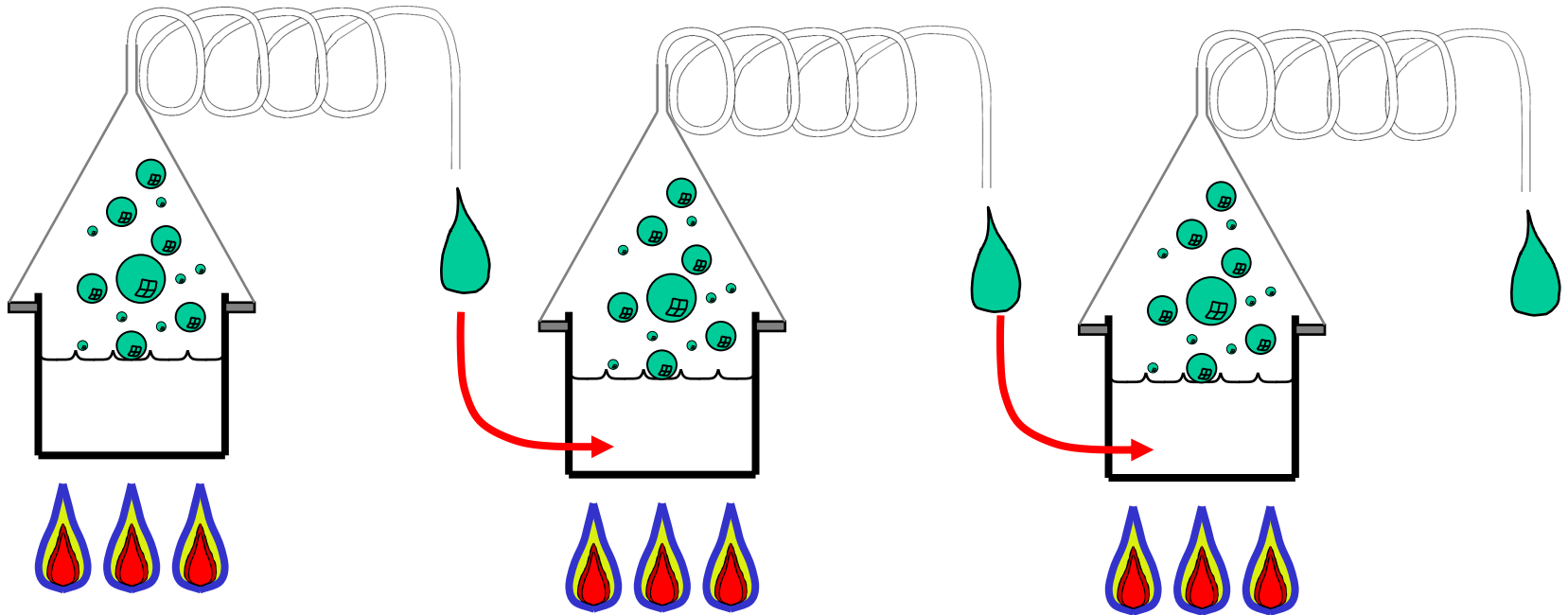
62% Ethanol!



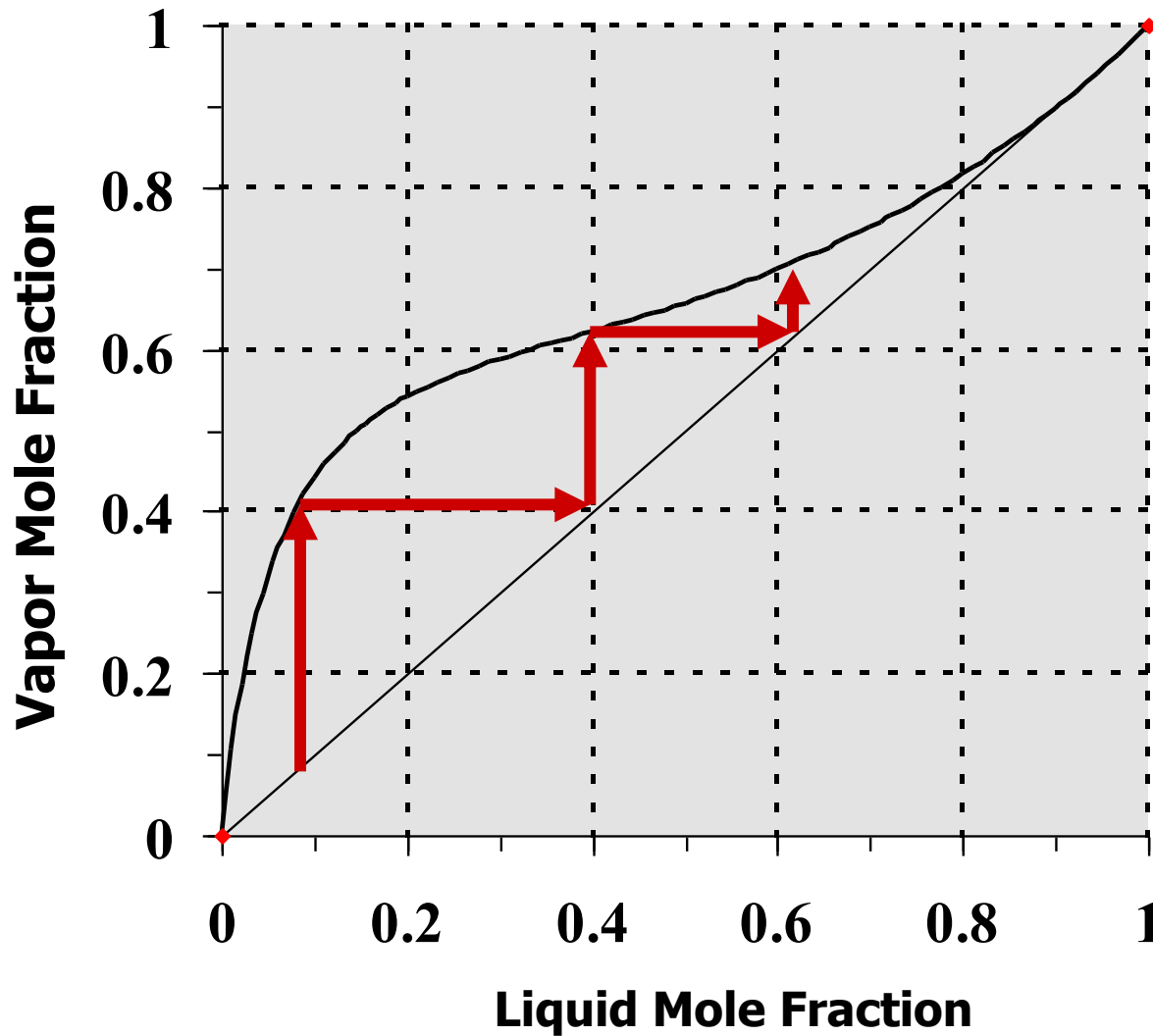
To make cognac
you distill twice

Pressure = 1 atm

How about 3 times or More?



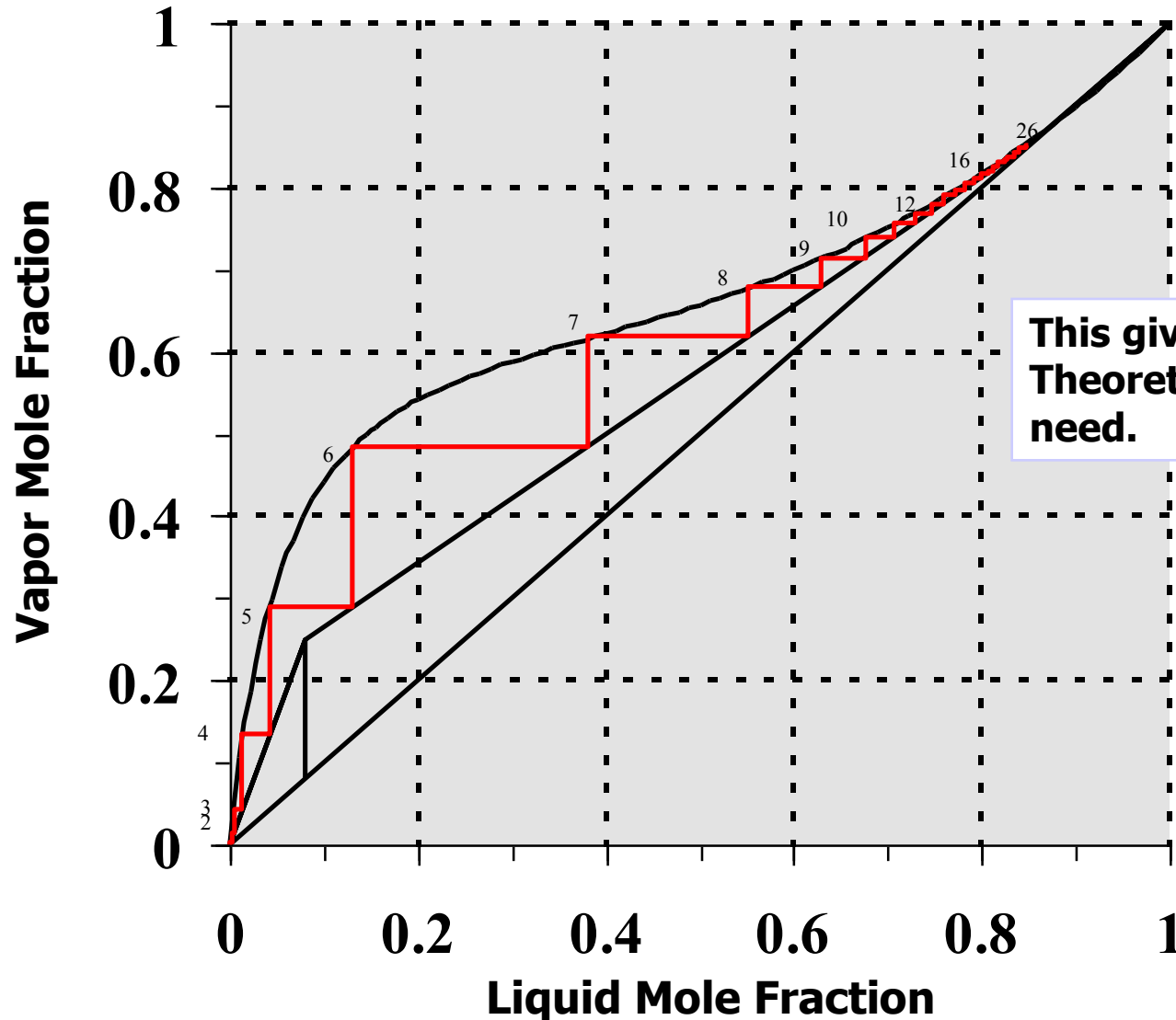
You get 70% Ethanol!



Pressure = 1 atm

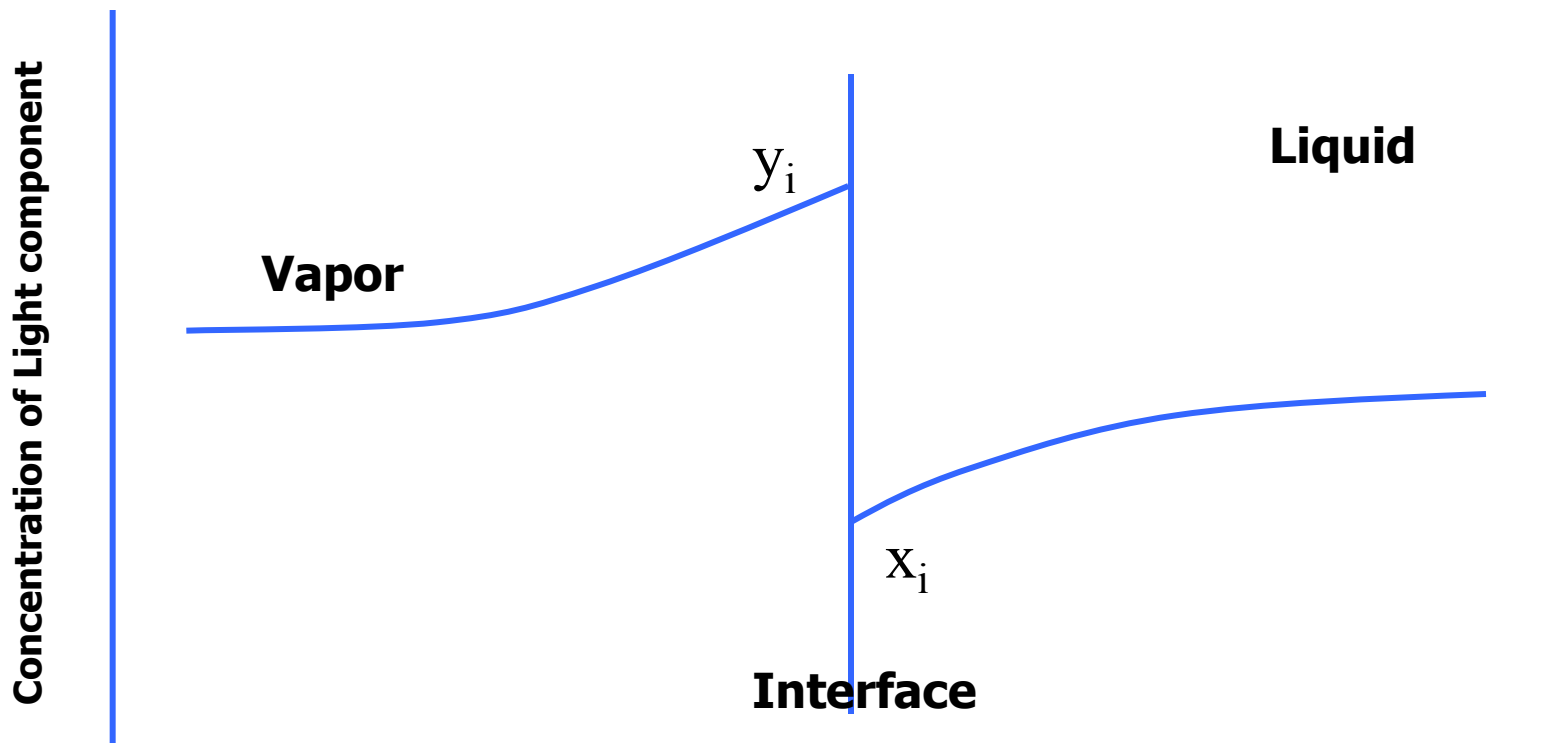
If you turn this into Column with Reflux

Pressure = 1 atm



Mass Transfer

The "Gory Details" are that mass transfer only occurs at the interface between the liquid and vapor phase. In a trayed tower this occurs at the bubble wall, in a packed tower this occurs at the thin film.



Distillation is:

The most common separation technique practiced today.

It consumes enormous amounts of energy in both heating and cooling.

Can contribute to more than 50% of a plant's operating costs.

Has been the focus of numerous studies by the US DOE for over 30 years to reduce energy consumption.

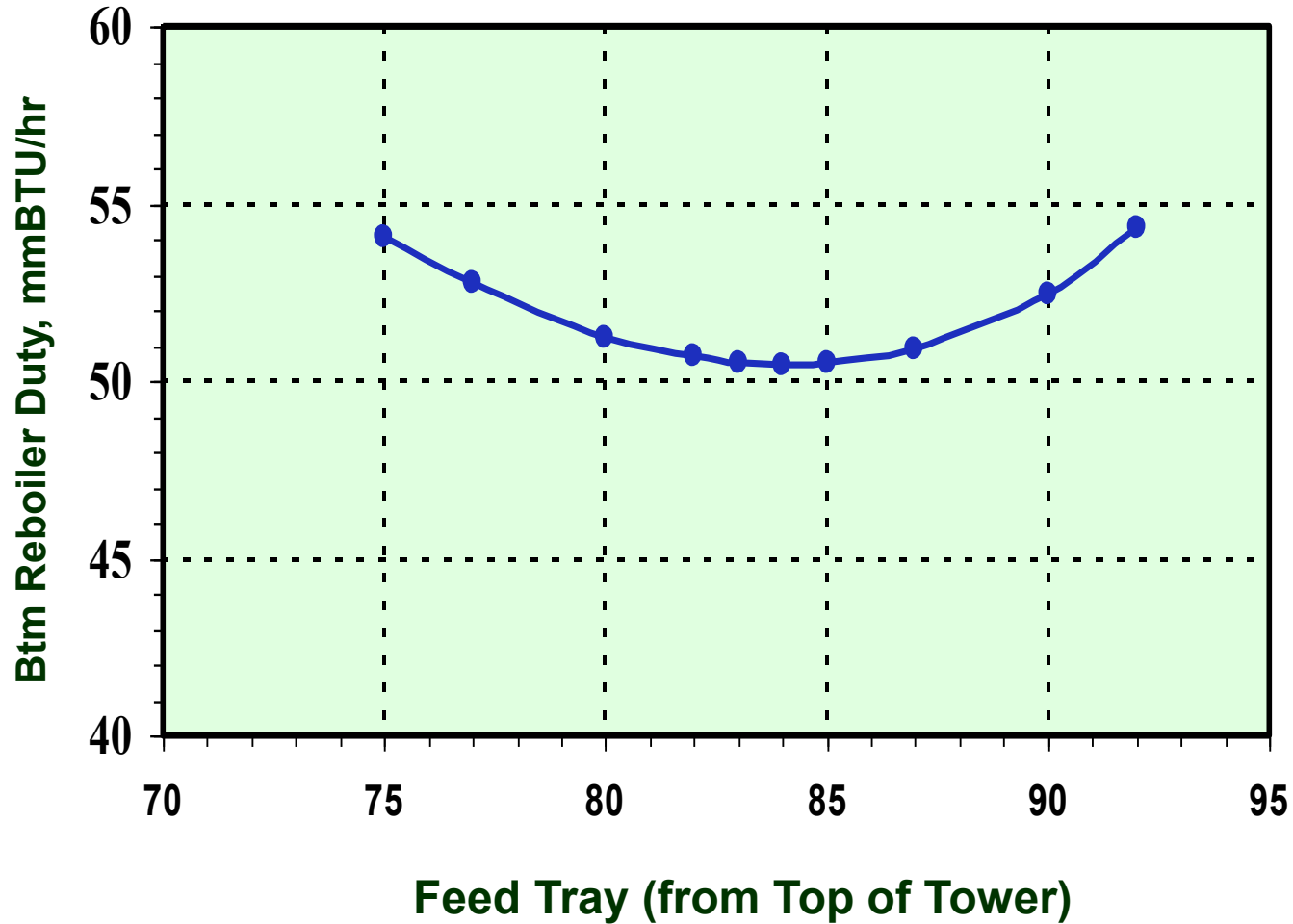
Simulation Tools do little more than what the previous McCabe-Thiele diagram did except add in Heat effect and how to handle multicomponent mixtures.

The key to a good simulation is getting the equilibrium data correct. The set of Equilibrium data is called a Model

Simulations

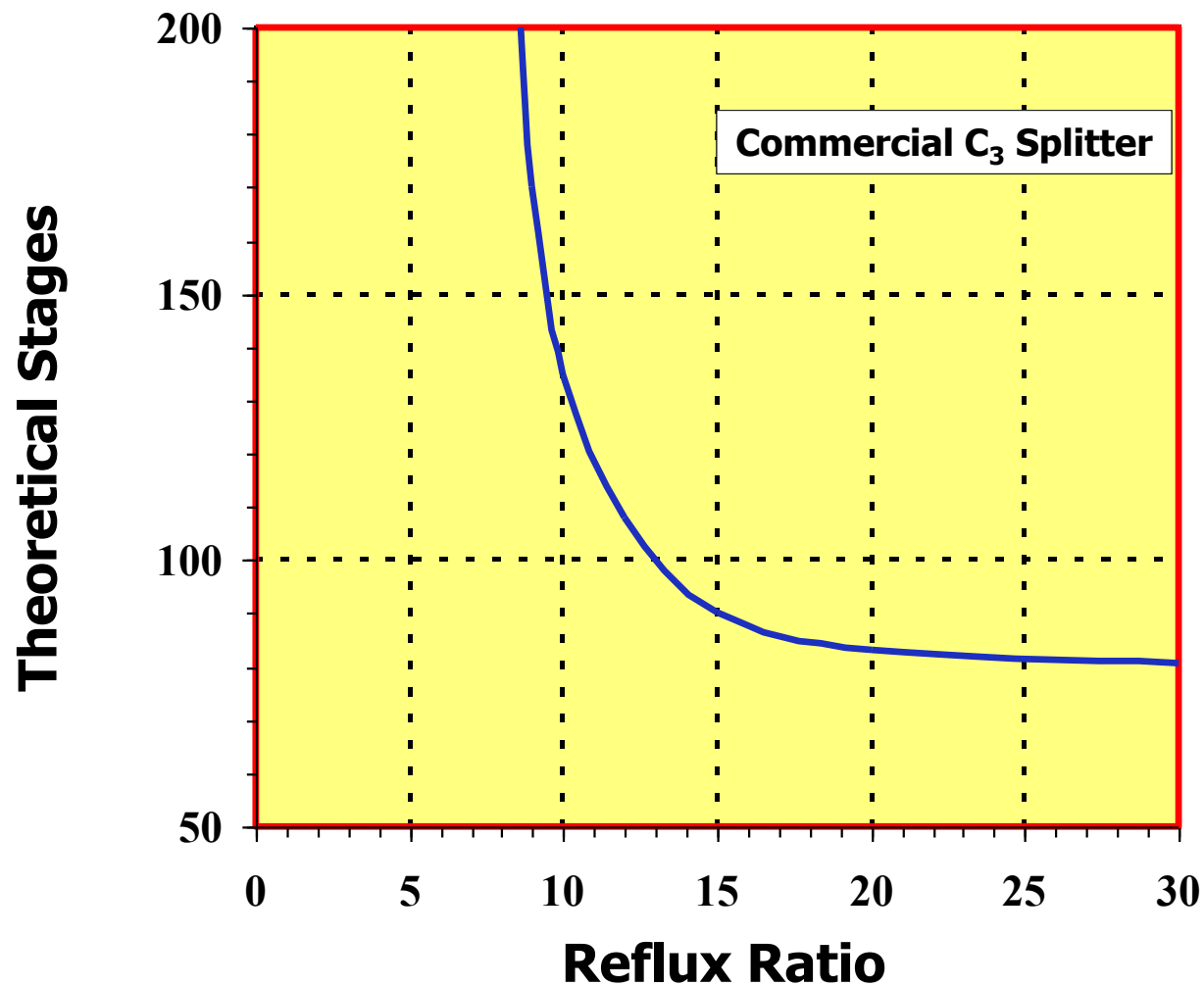
Most Critical Aspect
of
Distillation Technology !

Can help you find the Optimum Feed Point.



Simulations also generate Theoretical Stages vs. Reflux Ratio Curves

Curve at Constant Product Purities



Process Considerations

Optimum Design

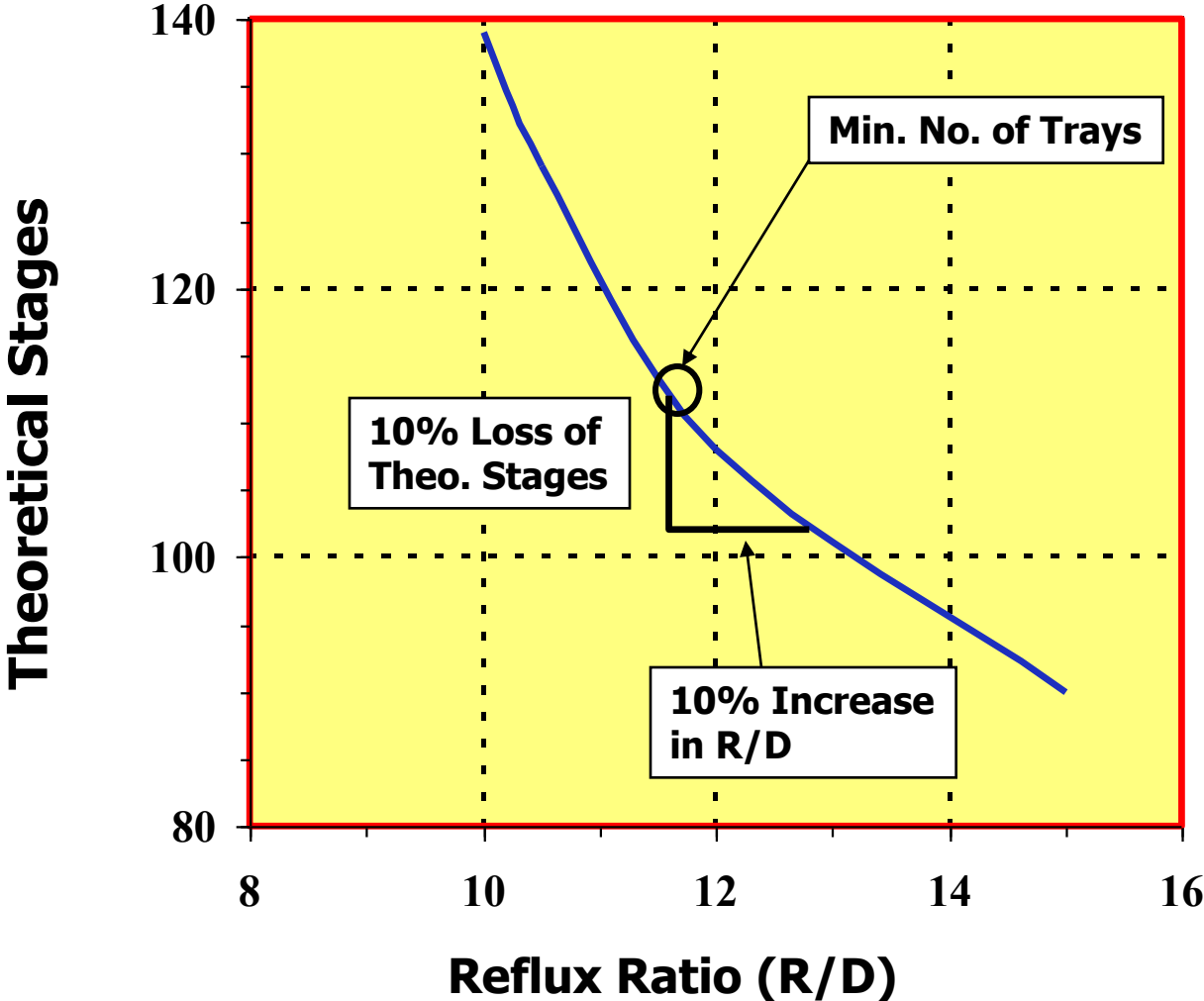
An Optimum Design is one that minimizes Capital Investment while satisfying Operational Needs

Minimum Capital in a Distillation Tower is usually represented as least No. of Actual Trays or Packed Height

Good Operation dictates that a 10% shortfall in performance must be accommodated by a 10% maximum increase in Reflux Ratio.

Optimized Design

Detail of a typical C₃ Splitter Plot



Process Considerations

Design

Be careful with Computer Simulations. They are only as good as the data used to make them.

Superfractionators (i.e. C_2 , C_3 , & Xylene Splitters) simulations need to be checked against or fitted to available VLE data ! These towers have relative volatilities around 1.05 to 1.10 and small errors will result in a large effect on the number of Stages to use for design.

Watch out for Pinch Points and convergence problems!

Process Simulations

The Whole Purpose

Once a Number of Theoretical Stages has been established, a **Heat & Material Balance** can be made for a given Feed and Product Rate.

The **Heat & Material Balance** Simulation allows the designer to determine the **Internal Loads and Physical Properties** needed for Design/Evaluation.

Towers

With the **Internal Loads and Physical Properties** one can size new towers or check the capacity of existing ones.

There are 2 general categories of internals for towers;

Trays and Packings

In the Packing category there is both Random Packing and Structured Packing.

How does one pick between **Trays and Packings**?

Rule #1) If pressure drop is important - use packing

Rule #2) If Liquid Load < 3 gpm/ft², use structured packing

Rule #3) If Liquid Load > 20 gpm/ft², use trays or random packing

Rule #4) All other options are determined with economics.

How does one pick the type **Packing**?

This is very simplistic, but basically use the highest surface area packing that does not flood. To prevent flood, keep the pressure drop per foot of bed height below 0.4 inches of water.

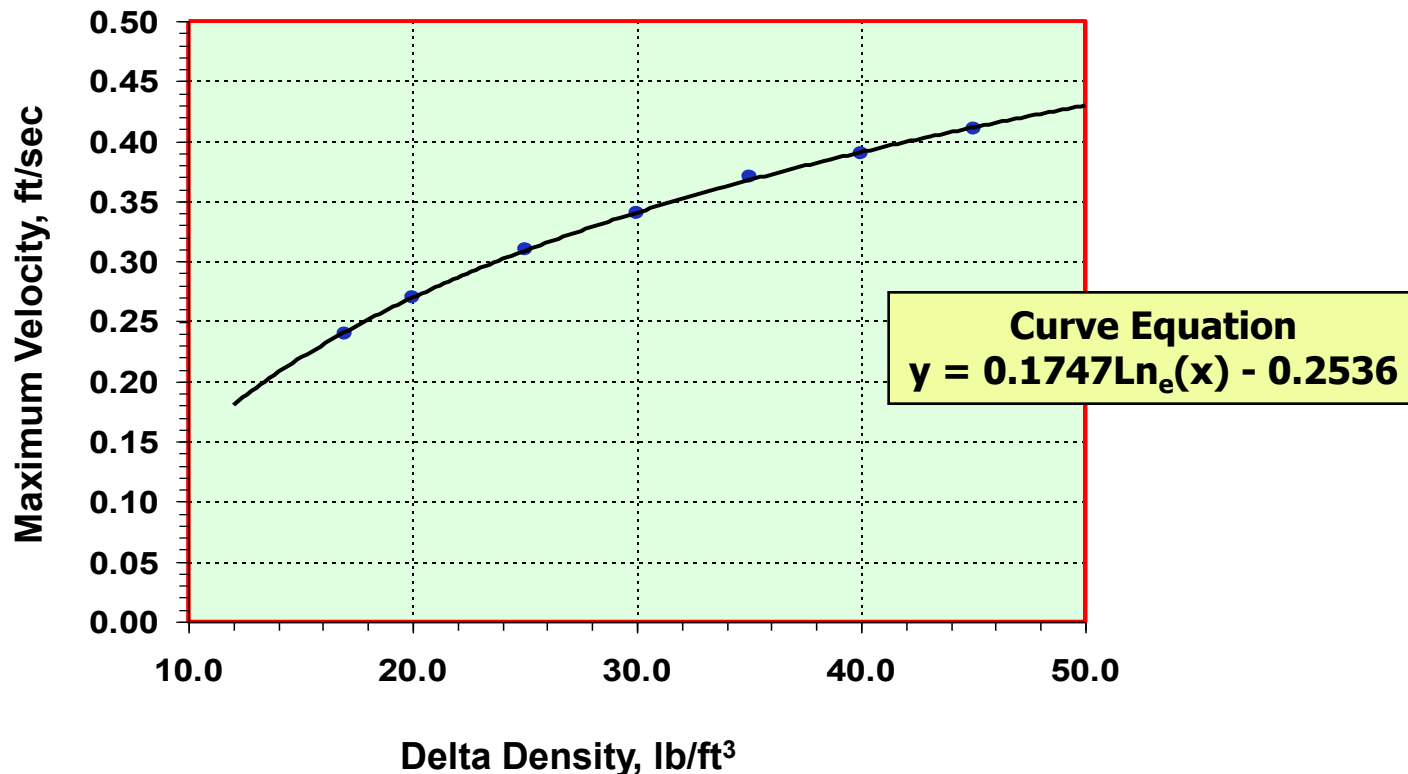
This will give you the lowest HETP (H**eight **E**quivalent to a **T**heoretical **P**late) and the widest operating range.**

Vendor software is very useful in calculating the pressure drop.

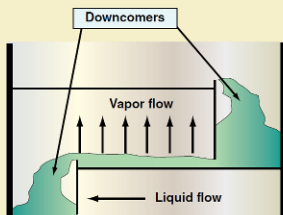
Trays

How does one determine a Tray design?

This is also very simplistic. Determine the downcomer area from the following chart. Then find the Active Area using the equations from June 2010 Chemical Engineering Magazine.



In a distillation column tray, vapor passes upward through liquid that is flowing across a horizontal perforated plate. Vapor passing through the perforated plate forms a two-phase mixture with the liquid and enables mass transfer contacting. This mixture is typically quite turbulent. Tray design must allow the turbulent liquid to fall away from the rising vapor in the space above the tray, while also enabling the vapor bubbles to rise out of the falling liquid in the downcomer. The downcomer is usually a vertical plate that enables the already contacted froth to travel down to the next tray without remixing with the up-flowing vapor from the tray below.

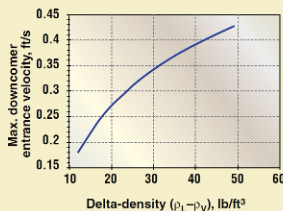


Side view of a simple tray arrangement

Generally, designing a column tray entails determining the minimum downcomer area that still allows vapor bubbles to rise through the liquid, selecting the number of downcomers, determining the active area, and checking the flow path length to see if a person can pass through a tray manway. These factors are the primary drivers for determining overall tower size.

Downcomer area is determined by the maximum recommended downcomer velocity. Divide the volumetric flow of liquid by the downcomer velocity to obtain the downcomer top area. Typically a curve of maximum downcomer velocity versus the density difference between liquid and vapor is consulted during this process.

Maximum downcomer velocity guideline



A downcomer is generally straight unless its area exceeds 8% of the tower

area. In that case, the downcomer is sloped such that its bottom area is 60% of its top area.

Active area

The active area of a distillation tower is where the vapor contacts the liquid to effect mass transfer. Above the active area, where the liquid falls away from the rising vapor, is the volume where the vapor can expand. Typically, the active area is calculated to be the tower cross-sectional area minus the downcomer top and downcomer bottom area.

The minimum active area (ft²) for normal valve trays can be determined from the following relationship, which is a modification of a commonly used correlation [7] taken at 82% of jet flood:

$$\text{Active area} = V_{\text{Load}} / [TS^{0.5} (0.0762 - 0.00092(\rho_v^2)) - 0.011 W_i]$$

Where,

$$V_{\text{Load}} = CFS_v (\rho_v / (\rho_l - \rho_v))^{0.5}$$

TS = Tray spacing, in.

ρ_v = Vapor density, lb/ft³

ρ_l = Liquid density, lb/ft³

W_i = Weir loading, gal/min per in.

CFS_v = Vapor volumetric flow, ft³/s

The required active area is dependant on the vapor density and weir loading. Note that the weir loading need not be known at this point. Assume a weir loading value of 5 gal/min per in. initially. Typical tray spacings are 24 in.

Tower area and diameter

Based on the above areas, the overall tower area and diameter can be determined by the following:

$$A_T = A_{D_{\text{top}}} + A_{D_{\text{bottom}}} + A_A$$

$$D = 2(A_T / \pi)^{0.5}$$

Where,

A_T = Tower area, ft²

$A_{D_{\text{top}}}$ = Downcomer area at top, ft²

$A_{D_{\text{bottom}}}$ = Downcomer area at bottom, ft²

A_A = Active Area, ft²

D = Tower inner dia., ft

Number of downcomers

Once the tower diameter is determined, then the number of downcomers can be chosen. As a starting point, an initial design should use a single downcomer. The resulting weir length is calculated from a standard chord-length calculation, which is iterative for a given downcomer area.

$$B_w = \{[\pi D^2 / 360] \cos^{-1}(2Z/D) - 2A_D\} / Z$$

Where,

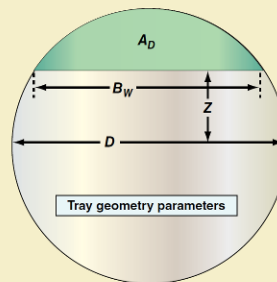
$$Z = [(D^2/4) - B_w^2]^{0.5}$$

B_w = Weir length of one downcomer, ft

Distillation Tray Design

A good place to start the iterative process is with a weir length 0.8 times the tower diameter. If the resulting weir loading is greater than 12 gal/min per in., then increase the number of tray passes to two. Recalculate the outlet weir length for each of the side downcomers of the column by using half the downcomer area. Check the weir loading again (for the tray with side downcomers). If the weir loading continues to exceed 12 gal/min per in., increase the number of tray passes to four. It is assumed that the two-pass tray with side downcomers has the shortest weir length.

The simplest approach to designing 4-pass trays is to assume equal bubbling area and make the side downcomers one-quarter of the total downcomer area, and make the center (and off-center) downcomer



ers one-half of the total downcomer area.

Maintaining the resulting downcomer widths at 6 in. or more will allow a person to reach into the downcomer for installation. In addition, make sure the resulting tray flow path length is 16 in. or greater to enable a person to physically pass through the trays. These minimum size criteria may increase the column diameter to above the previously calculated value.

Other considerations

Other criteria that need to be considered are; downcomer backup, spray fluidization, and entrainment. In addition, minimum load conditions need to be determined. The criteria for determining the low-end vapor and liquid range are weeping, tray stability and dry-tray pressure drop.

Reference

1. Glitsch Inc. "Ballast Tray Design Manual; Bulletin No. 4900." 3rd Ed. Glitsch Inc., Dallas, Tex., 1974.

Note: Material for the June "Facts at Your Fingertips" was supplied by Dan Summers, tray technology manager, Sulzer Chemtech USA Inc.

Chemical Engineering Magazine June 2010

From AIChE Spring 2011 Paper 9e

$$DCVel = 0.1747 L n_e (\rho - \rho_f)^{-0.2536}$$

$$A_D = \frac{L_{load}}{DCVel}$$

$$A_A = \frac{V_{load}}{FS^{0.5} \left(0.07616 - 0.00092 \rho_f^2 \right)^{-0.011} W_L}$$

$$A_T = A_{D_{TOP}} + A_{D_{BOTTOM}} + A_A$$

$$D = \left(\frac{A_T}{\pi} \right)^{0.5}$$

Vendor's public Software, such as Sulzer's SulCol3, is very useful to size and rate Tray and Packing designs.

SulCol version 3.0.8 has recently been upgraded to accommodate Vista and Windows 7 operating systems

SulCol 3 – Hydraulic Input

SULCOL 3.0.8

File Edit Project Window Help

Unit Type: US No NTS/HETP

Loadings

Sec. 1

Packing

Diam [in] Fluid Data Packing Design Packing-Type Height [ft] NTS req. HETP [in]

120.00 Fluid_2 Packing2 M250.Y 20.000 0.0 0

Flows

	G [lb/h]	L [lb/h]	ρG [lb/ft ³]	ρL [lb/ft ³]	σ [dyne/cm]	ηL [cP]	ηG [cP]	Cap [%]	F-F [US]	Liq. load [gpm/ft ²]	$\Delta p/\Delta z$ [in w./ft]	hl [%]	dp [mmHg]
Top	450000.0	240000.0	1.2000	45.00	12.00	0.200	0.0100	73.4	1.45	8.47	0.17		
Btm	450000.0	240000.0	1.2000	45.00	12.00	0.200	0.0100	73.4	1.45	8.47	0.17	3.8	6.43

Text System factor 1.00 Geom. Details

Sec. 2

Tray

Diam [in] Fluid Data Tray Design Tray Type DC Type # Pas. Spac. [in] # Trays Height [ft] NTS required Effic. [%]

132.00 Fluid_3 Tray1 MVG STAND 4 24.00 10 18.000 0 0

Flows

	G [lb/h]	L [lb/h]	ρG [lb/ft ³]	ρL [lb/ft ³]	σ [dyne/cm]	ηL [cP]	ηG [cP]	Jet Fl. [%]	Weir load [gpm/in]	Δp /Tray [mmHg]	dry Δp [in. H2O]	DC vel [ft/s]	DC bkp [%]
Load 1	650000.0	650000.0	1.2000	45.00	12.00	0.200	0.0100	73	5.45	5.31	1.87	0.249	50
Load 2	650000.0	650000.0	1.2000	45.00	12.00	0.200	0.0100	43	3.27	3.04	0.67	0.149	28

Text System factor 1.00 Geom. Details

Total sections Column data

2 p top [mmHg] 0.00 Δp total [mmHg] 48.19

Current Section: 2

SulCol 3 – Tray Detailed Output

SULCOL 3.0.8

File Edit Project Window Help

Unit Type: US No NTS/HETP

Geometry details for tray section no. 2

Section 2 Section: Fluid_3 NTS req.: 0 Effic. [%] 0

Parameter selection
Tray Design -> Tray1 # Trays 10

Tray Type: MVG
Tray Diameter [in]: 132.00
No. of Passes: 4
Material: 304 AISI DIN
Tray Thickness [in]: 0.0787
Tray Spacing [in]: 24.00
Openings #: 1604
Open Area [%]: 13.50
Valve Lift [in]: 0.3543
Valve Density [1/ft²]: 23.1
Side DC Weir Type: Normal
Downcomer Type: STANDARD

	Side	Center	Off-Cntr inboard	Off-Cntr outboard
Top Width [in]:	10.500	10.000		10.000
Bottom Width [in]:	8.000	5.000		5.000
Outlet Weir Hgt [in]:	2.00	2.00		2.00
Clearance Hgt [in]:	1.50	1.50		1.50
Outlet Weir Len [in]:	71.44	263.24	121.96	111.60
Eff. Outl Weir Len [in]:	0.00	187.80	0.00	92.03
Clearance Len [in]:	62.99	263.81	119.77	114.60
Eff. Clear Length [in]:	0.00	0.00	0.00	90.38
Inlet Weir Hgt [in]:	0.00	0.00		0.00
Rec. Pan Depth [in]:	0.00	0.00		0.00
Rec. Pan Width [in]:	0.00	0.00		0.00
Radius Tips:	<input type="checkbox"/>	<input type="checkbox"/>		<input type="checkbox"/>
Anti-Jump-Baffle:	<input type="checkbox"/>	<input type="checkbox"/>		<input type="checkbox"/>
Distance C/L to Tower Wall [in]:	35.75	35.75	<input checked="" type="checkbox"/> linked	

Optimize D.C. Initial Design Detailed Result

Calculated Output

Load	Load 1	Load 2
Flow Multiplier Gas [%]	100	60
Flow Multiplier Liquid [%]	100	60
Gas Flow [lb/h]	650000.0	390000.0
Liquid Flow [lb/h]	650000.0	390000.0
Useful Capacity (L/V=c) [%]	85.7	51.4
Flood (L=c) [%]	73	43
System Limit [%]	57.57	34.54
Weir Loading [gpm/in]	5.45	3.27
DryDrop [in. H2O]	1.87	0.67
Pressure Drop [mmHg]	5.31	3.04
Flow Parameter	0.163	0.163
D.C. Froth Backup [%]	50	28
D.C. Head Loss [in]	0.91	0.33
D.C. Flood [%]	50	30
D.C. Velocity [ft/s]	0.249	0.149
VSF/VSF Min	3.14	1.88
Flow Path Length [in]	22.75	22.75
Spray Factor	3.71	6.57

Detailed Calculated Output

Section Information
Section Remark:
Case: Load 1

Downcomers

	Side	Center	Off-Cntr
D.C. Top Velocity [ft/s]	0.245	0.249	0.247
D.C. Bottom Velocity [ft/s]	0.367	0.497	0.493
D.C. Head Loss [in]	0.91	0.38	0.46
D.C. Clear Liquid [in]	6.40	5.83	5.96
D.C. Froth Backup [%]	50	45	47
D.C. Top Area [%]	3.72	9.64	8.56
D.C. Btm/Top Area Ratio [%]	66.90	50.04	50.06

Tray Panels

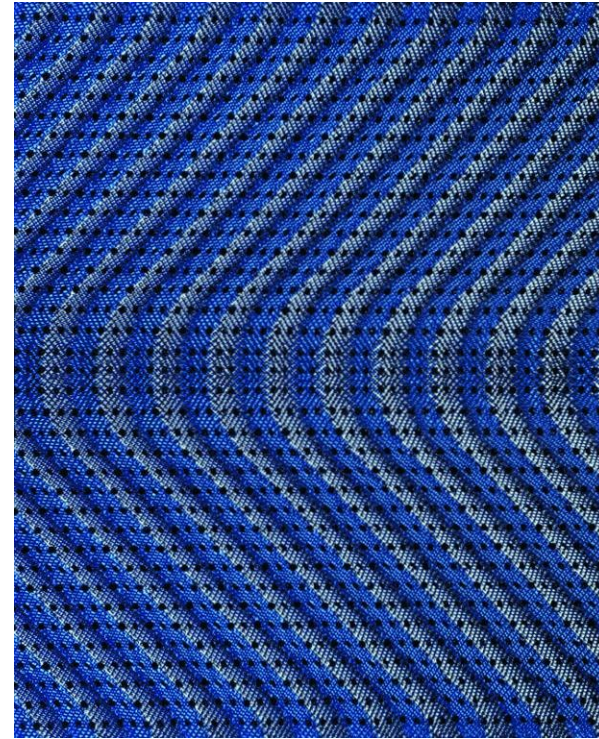
	A	B	C	D
Weir loading [gpm/in]	5.45	5.45	4.23	4.19
Flow Path length [in]	22.75	22.75	22.75	22.75
Active area [ft²]	15.246	20.088	14.451	20.277
Froth height [in]	12.39	12.51	11.68	11.55
Pressure drop [mmHg]	5.23	5.43	5.39	5.18
Clear liquid height [in]	1.29	1.27	1.12	1.13

Other
Constriction factor top: 0.623 btm: 0.564

Sulzer Num On Caps Off

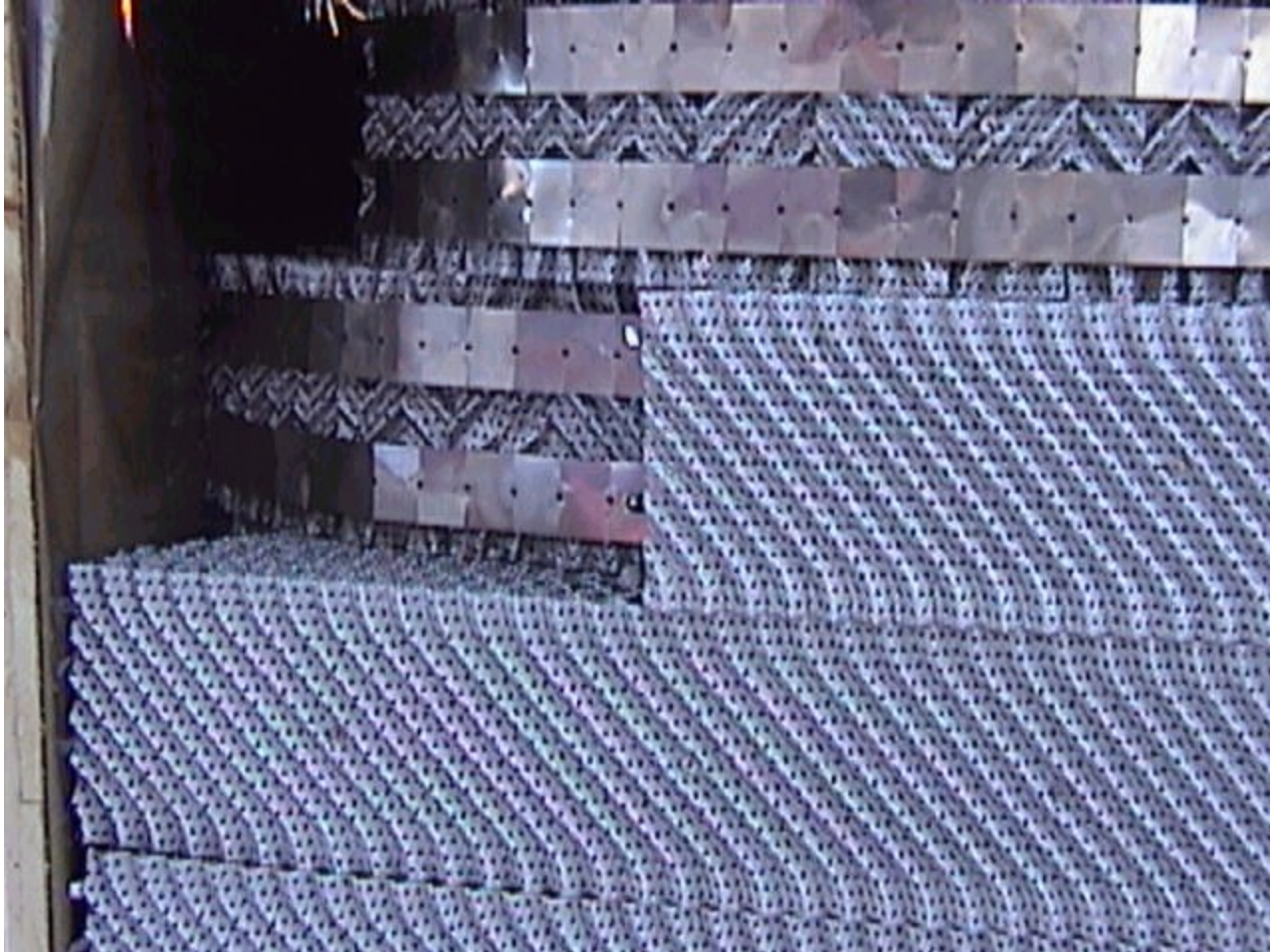
start C:\DRS\VGPlus\Do... AiChE Presentatio... C:\DRS\PAPERS\M... Novel Tray Design ... SULCOL 3.0.8 9:23 AM

Packing Major Improvements



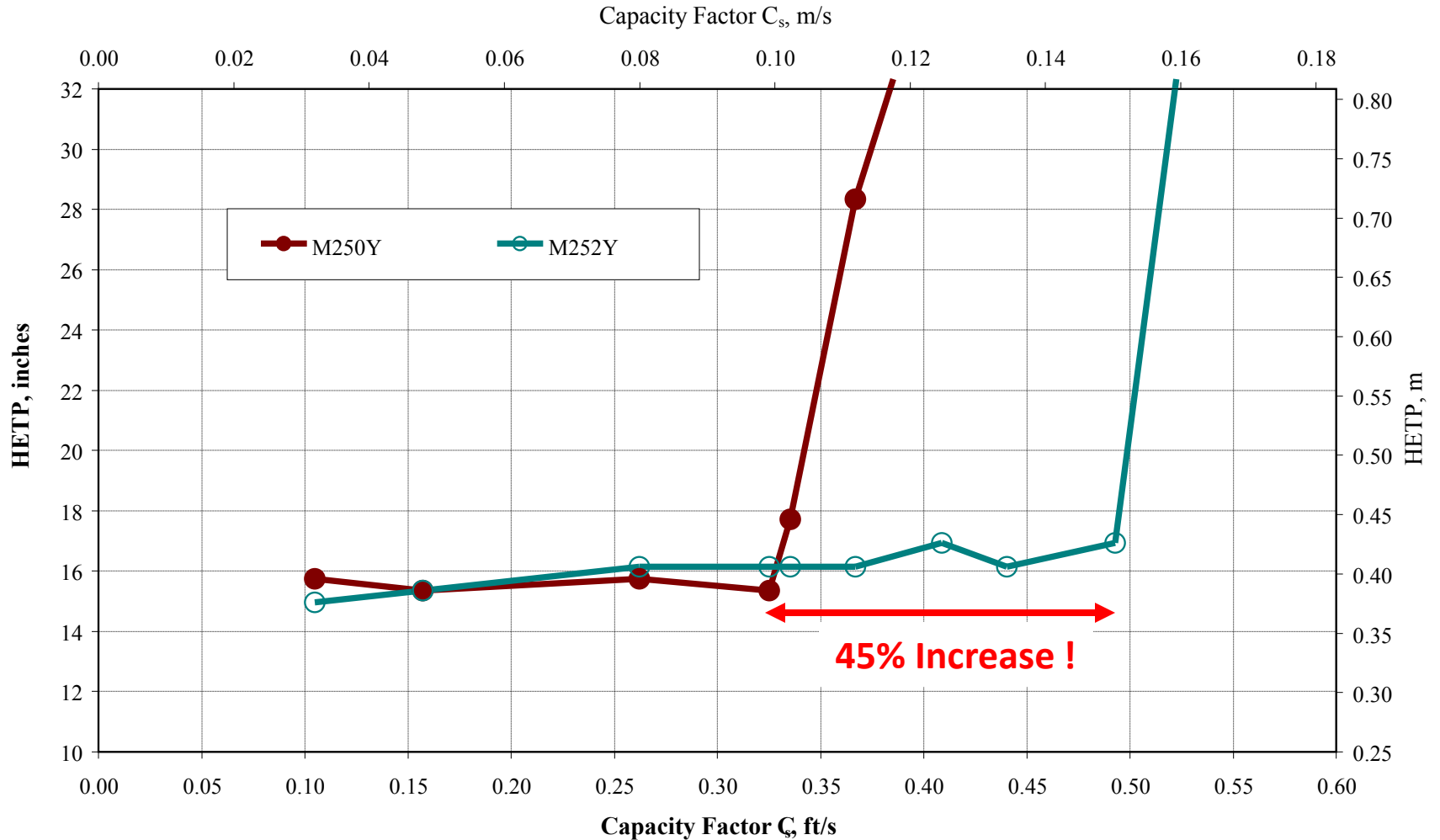
In the past 10 years, the industry recognized that packing capacity was limited at the interface between packing layers. Sulzer's solution was to 'bend' the packing at the top and bottom of the layer reduce liquid holdup at the interface.

M250.Y MellapakPlus in Crate



Packing Major Improvements

Chloro/Ethyl Benzene, 77 mm Hg



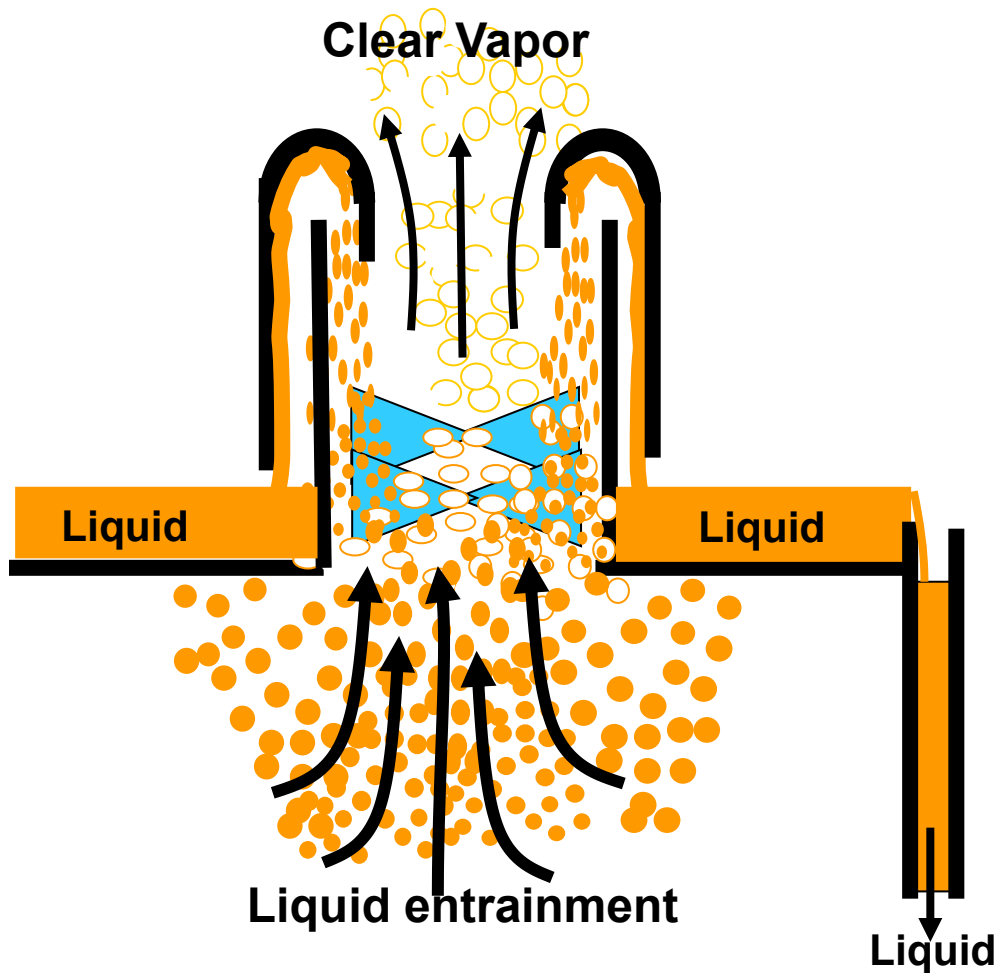
Tray Major Improvements

In the past 10 years, the industry realized that with high capacity trays utilizing truncated and highly sloped downcomers, smaller tray deck openings and tray deck enhancement features, that there is a maximum capacity "wall." This wall is called gravity.

Once every cubic inch of tower volume is utilized for liquid disengagement above a tray, then gravity will limit vapor capacity.

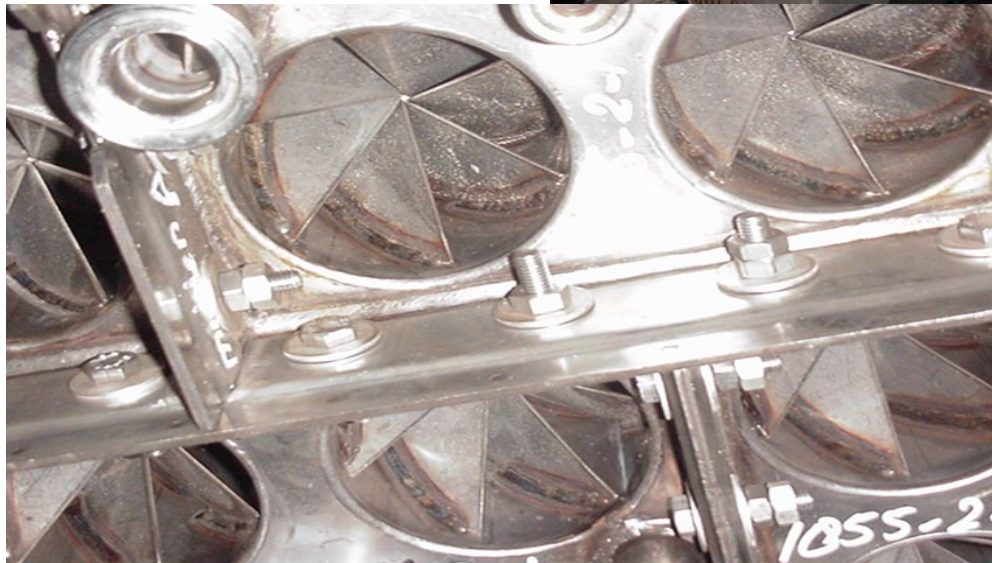
Other forces need to come into play to gain extra capacity in trayed distillation towers.

Tray Major Improvements

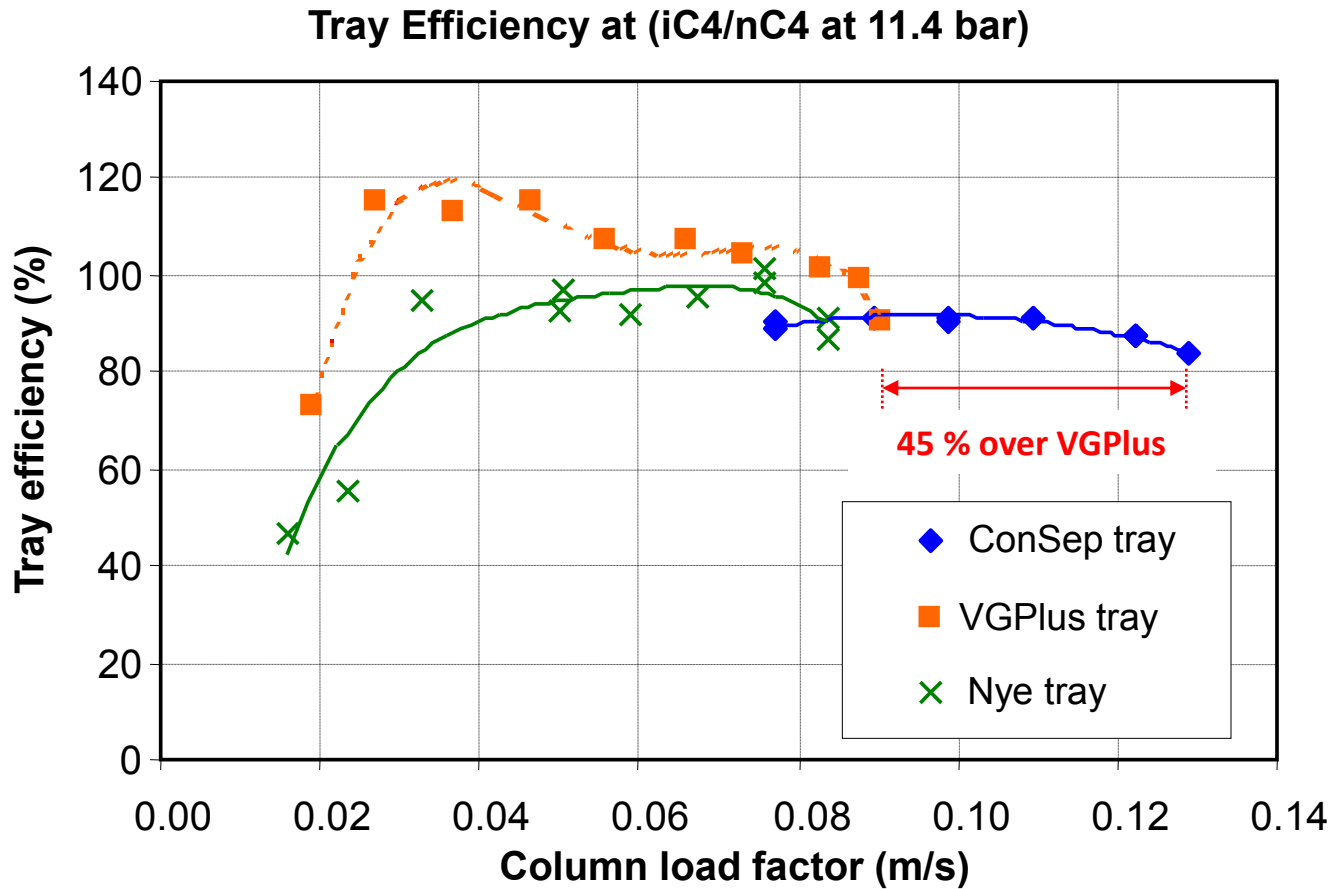


Shell's solution is to use operate a tray flooded and then use Centrifugal force to separate the entrained liquid from the vapor.

ConSep Tray



Tray Major Improvements



This is a substantial increase in Capacity over the best "gravity limited" technologies.

Packing Distributor Technology

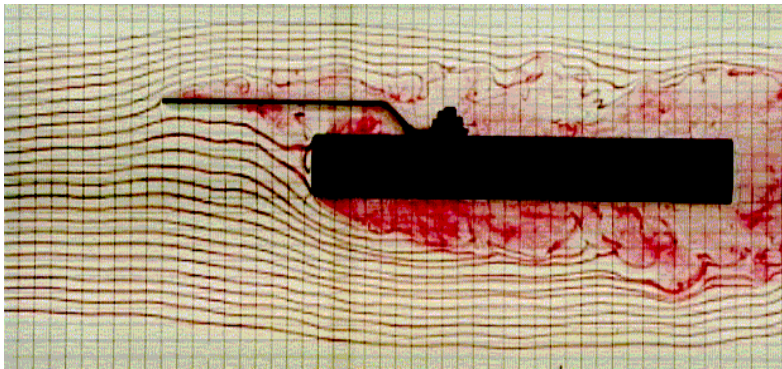
You can have the best packing in the world but this packing can only be as good as the initial distribution. **A poor distributor will make the best packing operate poorly.**

Pour point density, uniformity of distribution and available liquid head are a few of the important parameters that enable a good liquid distributor design.

Recent improvements in distributor design are lower pressure drop (of the vapor passing the distributor) and aerodynamic design.

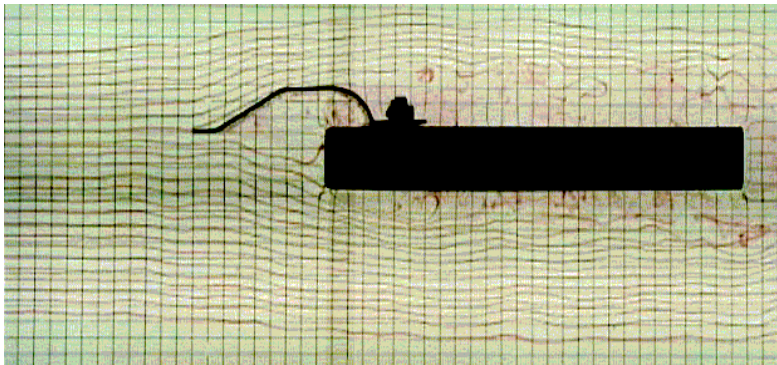
Splash Plate Distributor

Old VEP:

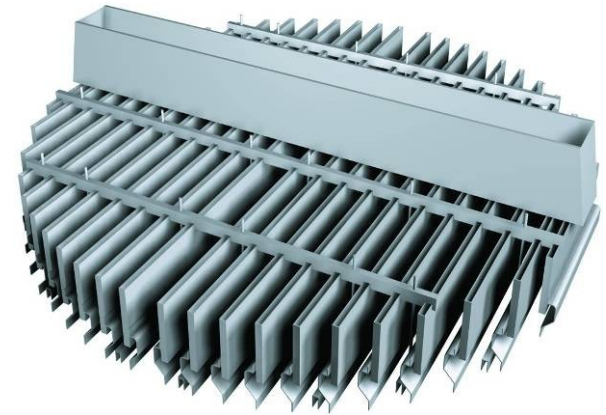


Former VEP

Current VEP:



New VEP



New BDH Tray



Superior Quality Control

Easier, Faster & Trouble-Free Installation

Same resistance to tray deck pop out

Equal or lower Pressure Drop

Same resistance to weeping

Less Expensive

The existence of such companies as Sulzer Chemtech and our competitors such as Koch-Glitsch, Jaeger-Raschig, UOP, Montz and ACS-Amistco depends on the continuous improvement in distillation technology.

We all are trying to make a better "mouse-trap." It was stated more than 20 years ago that Distillation was a mature Science and that no major improvement would be achieved. Since that statement was made, all of the improvements discussed here within were invented and commercialized.

In addition, there is company solely dedicated to promoting continued research into distillation called FRI.

FRI (**Fractionation Research Incorporated**) is a non-profit research consortium supported by memberships which include many of the largest petroleum, chemical, and engineering companies in the world. It was founded in the 1950's to engage in research that was too expensive for any one company.

That research includes the only independent commercial scale distillation experimentation program operating with hydrocarbon systems at pressures ranging from deep vacuum to 500psia. The current membership of over 70 companies includes many leading companies in the field of distillation. Over 60% of the membership is international.

Concluding Remarks

At AIChE National meetings there are annually more than 75 papers presented on Distillation alone. In addition, there are regional meetings, such as the South Texas Region that, has another 6 papers presented (and has more attendance than the national meetings.)

Is this the sign of a mature discipline?

Distillation, as the world's "oldest profession," is far from being a mature science. As long as this unit operation is used as the work horse to provide the overwhelming majority of separations, it will continue to see improvements as the years and decades go by.