



Dynamic Real-Time Optimization: Concepts in Modeling, Algorithms and Properties

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Dynamic Optimization Outline

- I Introduction
 - Typical Applications
 - Problem Statement
- II Dynamic Optimization
 - Sequential Methods
 - Multiple Shooting
 - Simultaneous Methods
- III Off-line Case Studies
 - Unstable Grade Transitions
 - Simulated Moving Beds
 - Parameter Estimation – Reactor Models
- IV On-line Optimization
 - NMPC Case Study
 - Advanced Step NMPC
 - Moving Horizon Estimation
- V Conclusions
 - Summary
 - References

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DAE Models in Process Engineering

Differential Equations
 Conservation Laws (Mass, Energy, Momentum)

Algebraic Equations
 Constitutive Equations, Equilibrium (physical properties, hydraulics, rate laws)
 Semi-explicit form
 Assume to be index one (i.e., algebraic variables can be solved uniquely by algebraic equations)
 If not, DAE can be reformulated to index one (see Ascher and Petzold)

Characteristics
 Large-scale models – not easily scaled
 Sparse but no regular structure
 Direct linear solvers widely used
 Coarse-grained decomposition of linear algebra


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Batch Distillation Multi-product Operating Policies

- Run between distillation batches
- Treat as boundary value optimization problem
 - When to switch from A to offcut to B?
 - How much offcut to recycle?
 - Reflux?
 - Boilup Rate?
 - Operating Time?

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Parameter Estimation

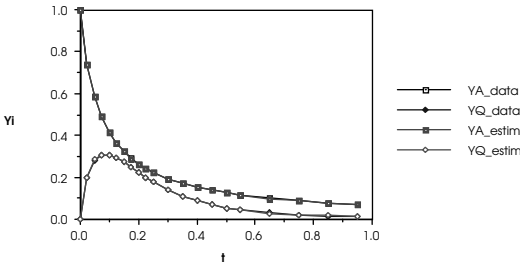
Catalytic Cracking of Gasoil (Tjoa, 1991)

$$A \xrightarrow{p_1} Q, Q \xrightarrow{p_2} S, A \xrightarrow{p_3} S$$

$$\dot{a} = -(p_1 + p_3)a^2$$

$$\dot{q} = -p_1a^2 - p_2q$$

$$a(0) = 1, q(0) = 0$$




number of states and ODEs: 2
 number of parameters: 3
 no control profiles
 constraints: $p_L \leq p \leq p_U$

Objective Function: Ordinary Least Squares

$(p_1, p_2, p_3)^0 = (6, 4, 1)$
 $(p_1, p_2, p_3)^* = (11.95, 7.99, 2.02)$
 $(p_1, p_2, p_3)_{true} = (12, 8, 2)$

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Batch Process Optimization

Optimization of dynamic batch process operation resulting from reactor and distillation column

DAE models:

$$z' = f(z, y, u, p)$$

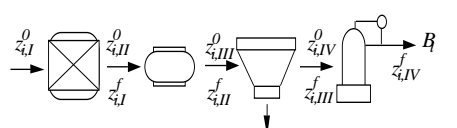
$$g(z, y, u, p) = 0$$

$$A+B \rightarrow C$$

$$C+B \rightarrow P+E$$

$$P+C \rightarrow G$$

number of states and DAEs: $n_z + n_y$
 parameters for equipment design (reactor, column)
 n_u control profiles for optimal operation



Constraints:

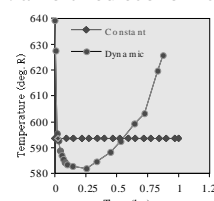
$$u_L \leq u(t) \leq u_U$$

$$y_L \leq y(t) \leq y_U$$

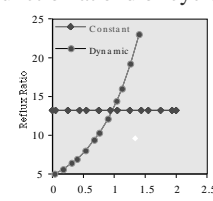
$$z_L \leq z(t) \leq z_U$$

$$p_L \leq p \leq p_U$$

Objective Function: amortized economic function at end of cycle time t_f



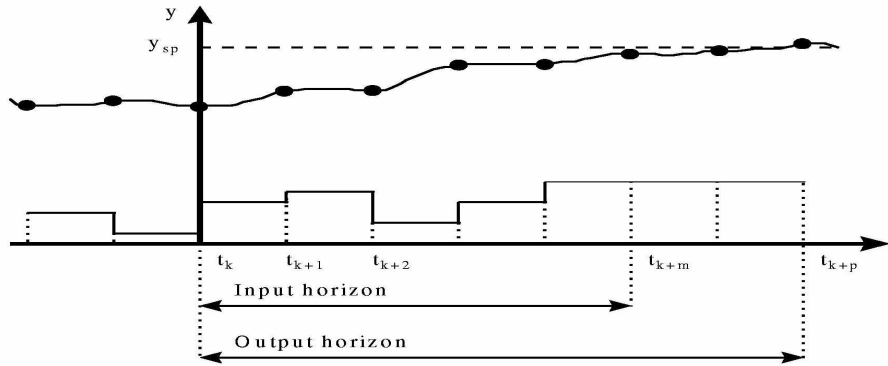
optimal reactor temperature policy



optimal column reflux ratio

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Nonlinear Model Predictive Control (NMPC)



$$\min_u \sum \|y(t) - y^{sp}\|_{Q_y}^2 + \sum \|u(t^k) - u(t^{k-1})\|_{Q_u}^2$$

$$s.t. \quad \begin{aligned} z'(t) &= F(z(t), y(t), u(t), t) \\ 0 &= G(z(t), y(t), u(t), t) \\ z(t) &= z^{init} \\ \text{Bound Constraints} \\ \text{Other Constraints} \end{aligned}$$

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Dynamic Optimization Problem

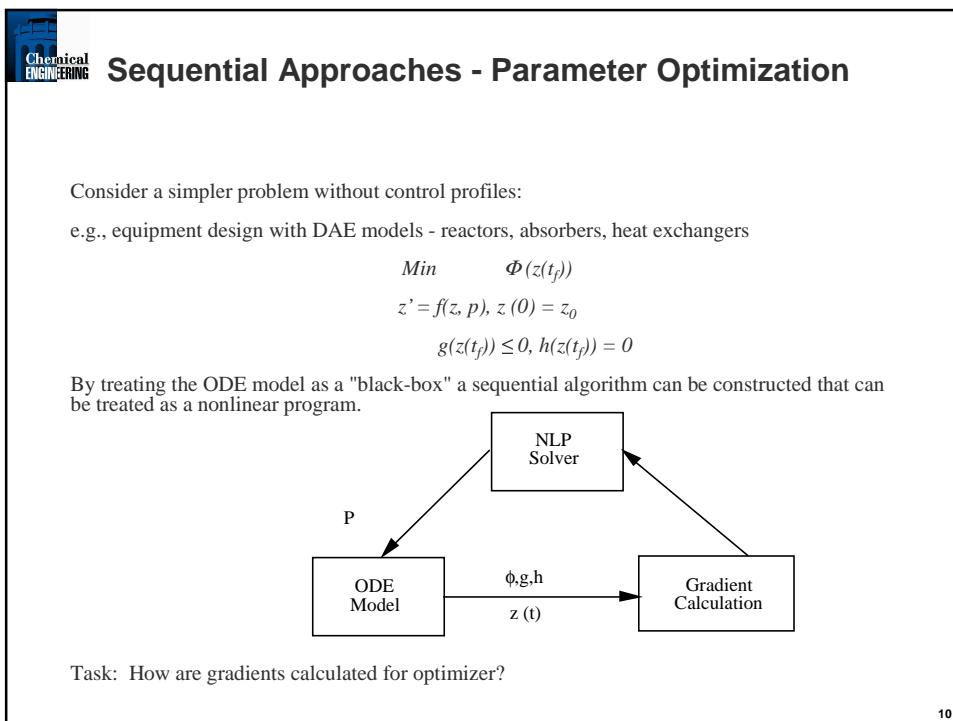
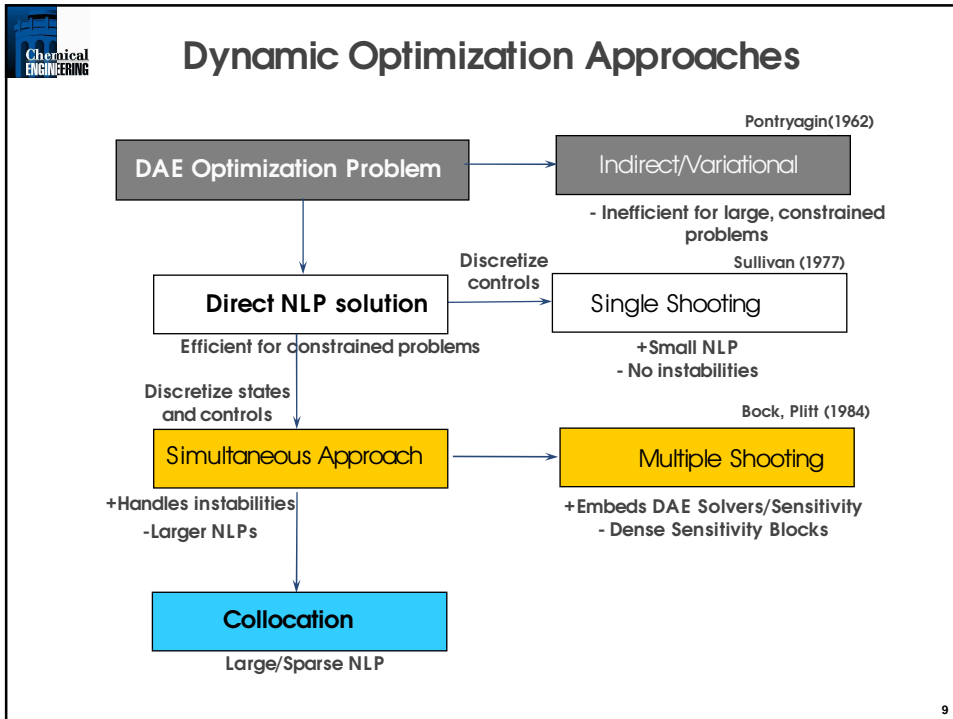
$$\min \Phi(z(t), y(t), u(t), p, t_f)$$

$$s.t. \quad \begin{aligned} \frac{dz(t)}{dt} &= f(z(t), y(t), u(t), t, p) \\ g(z(t), y(t), u(t), t, p) &= 0 \\ z^o &= z(0) \\ z^l &\leq z(t) \leq z^u \\ y^l &\leq y(t) \leq y^u \\ u^l &\leq u(t) \leq u^u \\ p^l &\leq p \leq p^u \end{aligned}$$

t, time
z, differential variables
y, algebraic variables

t_f, final time
u, control variables
p, time independent parameters

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Gradient Calculation

Perturbation

Sensitivity Equations

Adjoint Equations

Perturbation

Calculate approximate gradient by solving ODE model $(np + 1)$ times

Let $\psi = \Phi$, g and h (at $t = t_f$)

$$d\psi/dp_i = \{\psi(p_i + \Delta p_i) - \psi(p_i)\} / \Delta p_i$$

Very simple to set up

Leads to poor performance of optimizer and poor detection of optimum unless roundoff error ($O(1/\Delta p_i)$) and truncation error ($O(\Delta p_i)$) are small.

Work is proportional to np (expensive)

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Direct Sensitivity

From ODE model: $\frac{\partial}{\partial p} \{z' = f(z, p, t), z(0) = z_0(p)\}$

define $s_i(t) = \frac{\partial z(t)}{\partial p_i}$ $i = 1, \dots, np$

$$s'_i = \frac{d}{dt}(s_i) = \frac{\partial f}{\partial p_i} + \frac{\partial f}{\partial z} s_i, \quad s_i(0) = \frac{\partial z(0)}{\partial p_i}$$

($nz \times np$ sensitivity equations)

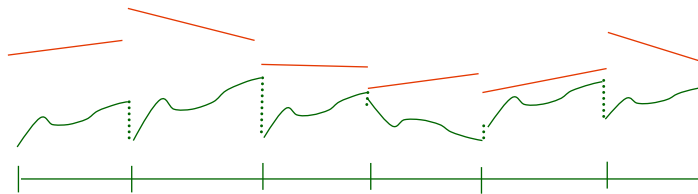
- z and s_i , $i = 1, \dots, np$, can be integrated forward simultaneously.
- for implicit ODE solvers, $s_i(t)$ can be carried forward in time after converging on z
- linear sensitivity equations exploited in ODESSA, DASSAC, DASPK, DSL48s and a number of other DAE solvers

Sensitivity equations are efficient for problems with many more constraints than parameters ($1 + ng + nh > np$)

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Multiple Shooting for Dynamic Optimization

Divide time domain into separate regions



Integrate DAEs state equations over each region

Evaluate sensitivities in each region as in sequential approach wrt u_{ij} , p and z_j

Impose matching constraints in NLP for state variables over each region

Variables in NLP are due to control profiles as well as initial conditions in each region

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Multiple Shooting Nonlinear Programming Problem

$$\begin{aligned}
 & \min_{u_{i,j}, p} \psi(z(t_f), y(t_f)) \\
 \text{s.t.} \quad & z(z_j, u_{i,j}, p, t_{j+1}) - z_{j+1} = 0 \\
 & z_k^l \leq z(z_j, u_{i,j}, p, t_k) \leq z_k^u \\
 & y_k^l \leq y(z_j, u_{i,j}, p, t_k) \leq y_k^u \\
 & u_i^l \leq u_{i,j} \leq u_i^u \\
 & p^l \leq p \leq p^u
 \end{aligned}$$

$$\begin{aligned}
 \left(\frac{dz}{dt}\right) &= f(z, y, u_{i,j}, p), \quad z(t_j) = z_j \\
 g(z, y, u_{i,j}, p) &= 0 \\
 z_0^o &= z(0)
 \end{aligned}$$

$$\begin{aligned}
 & \min_{x \in \mathcal{R}^n} f(x) \\
 \text{s.t.} \quad & c(x) = 0 \\
 & x^L \leq x \leq x^u
 \end{aligned}$$

Solved Implicitly

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Dynamic Optimization – Multiple Shooting Strategies

Larger NLP problem $O(np+nu+NE\ nz)$

- Use SNOPT, MINOS, etc.
- Second derivatives difficult to get

Repeated solution of DAE model and sensitivity/adjoint equations, scales with nz and np

- Dominant computational cost
- May fail at intermediate points

Multiple shooting can deal with unstable systems with sufficient time elements.

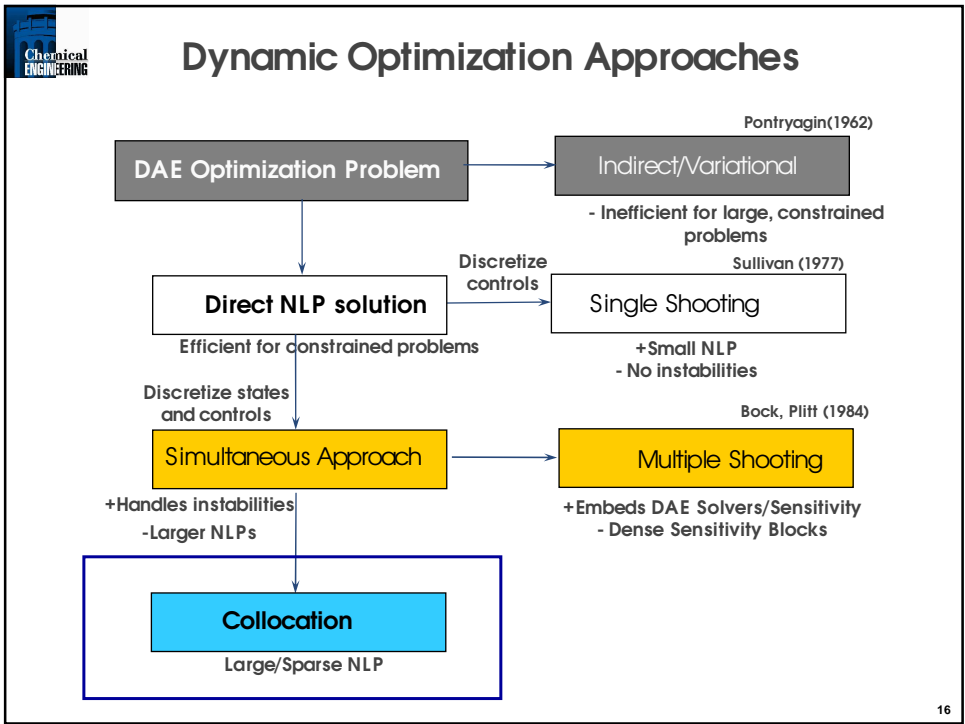
Discretize control profiles to parameters (at what level?)

Path constraints are difficult to handle exactly for NLP approach

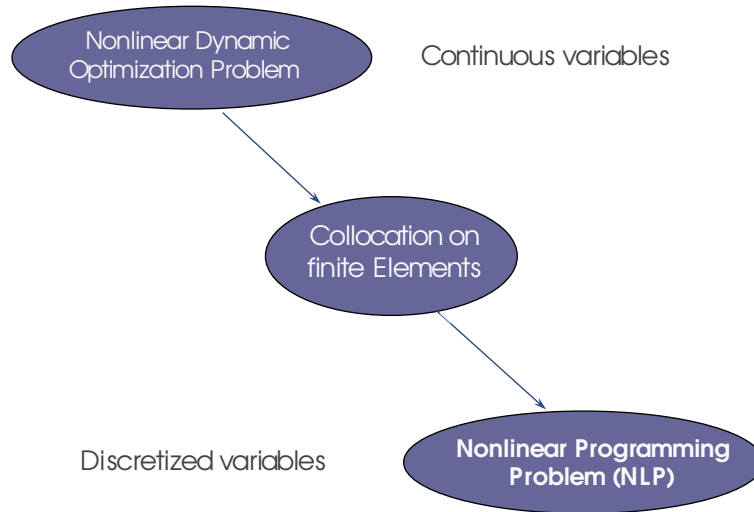
Block elements for each element are dense!

Extensive developments and applications by Bock and coworkers using MUSCOD code

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Nonlinear Programming Formulation



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Discretization of Differential Equations Orthogonal Collocation

Given: $dz/dt = f(z, u, p)$, $z(0) = \text{given}$

Approximate z and u by Lagrange interpolation polynomials (order $K+1$ and K , respectively) with interpolation points, t_k

$$z_{K+1}(t) = \sum_{k=0}^K z_k \ell_k(t), \ell_k(t) = \prod_{\substack{j=0 \\ j \neq k}}^K \frac{(t-t_j)}{(t_k-t_j)} \implies z_{N+1}(t_k) = z_k$$

$$u_K(t) = \sum_{k=1}^K u_k \ell_k(t), \ell_k(t) = \prod_{\substack{j=1 \\ j \neq k}}^K \frac{(t-t_j)}{(t_k-t_j)} \implies u_N(t_k) = u_k$$

Substitute z_{N+1} and u_N into ODE and apply equations at t_k .

$$r(t_k) = \sum_{j=0}^K z_j \dot{\ell}_j(t_k) - f(z_k, u_k) = 0, \quad k = 1, \dots, K$$

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Converted Optimal Control Problem Using Collocation

$$\text{Min } \phi(z(t_f))$$

$$\text{s.t. } z' = f(z, u, p), z(0) = z_0$$

$$g(z(t), u(t), p) \leq 0$$

$$h(z(t), u(t), p) = 0$$

to Nonlinear Program

$$\text{Min } \phi(z_f)$$

$$\sum_{j=0}^K z_j \dot{\ell}_j(t_k) - f(z_k, u_k) = 0, z_0 = z(0)$$

$$g(z_k, u_k) \leq 0$$

$$h(z_k, u_k) = 0$$

} $k = 1, \dots, K$

$$\sum_{j=0}^K z_j \dot{\ell}_j(1) - z_f = 0$$

How accurate is approximation

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Collocation on Finite Elements

$$\frac{dz}{dt} = \frac{1}{h_i} \frac{dz}{d\tau}$$

$$\frac{dz}{d\tau} = h_i f(z, u)$$

$$t_{ij} = \sum_{\tau=1}^{i-1} h_i + h_i \tau_j, \tau_j \in [0, 1]$$

$$z(t) = \sum_{q=0}^K \dot{\ell}_q(t) z_{iq}$$

$$r(t_{ik}) = \sum_{j=0}^K (z_{ij} \dot{\ell}_j(\tau_k)) - h_i f(z_{ik}, u_{ik}, p) = 0, k = 1, \dots, K, i = 1, \dots, NE$$

$$y(t) = \sum_{q=1}^K \dot{\ell}_q(t) y_{iq}$$

$$u(t) = \sum_{q=1}^K \dot{\ell}_q(t) u_{iq}$$

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Nonlinear Programming Problem

$$\begin{aligned} & \min \psi(z_f) \\ \text{s.t.} \quad & \sum_{j=0}^K (z_{ij} \dot{\ell}_j(\tau_k)) - h_i f(z_{ik}, u_{ik}, p) = 0 \\ & g(z_{i,k}, y_{i,k}, u_{i,k}, p) = 0 \\ & \sum_{j=0}^K (z_{i-1,j} \ell_j(1)) - z_{i0} = 0, \quad i = 2, \dots, NE \\ & \sum_{j=0}^K (z_{NE,j} \ell_j(1)) - z_f = 0, \quad z_{10} = z(0) \end{aligned}$$

$$\begin{aligned} z_{i,j}^l &\leq z_{i,j} \leq z_{i,j}^u \\ y_{i,j}^l &\leq y_{i,j} \leq y_{i,j}^u \\ u_{i,j}^l &\leq u_{i,j} \leq u_{i,j}^u \\ p^l &\leq p \leq p^u \end{aligned}$$

$$\begin{aligned} & \min_{x \in \mathcal{X}^n} f(x) \\ \text{s.t.} \quad & c(x) = 0 \\ & x^L \leq x \leq x^u \end{aligned}$$

Finite elements, h_i , can also be variable to determine break points for $u(t)$.

Add $h_u \geq h_i \geq 0, \sum h_i = t_f$

Can add constraints $g(h, z, u) \leq \epsilon$ for approximation error

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Theoretical Properties of Simultaneous Method

A. Stability and Accuracy of Orthogonal Collocation

- Equivalent to performing a *fully implicit* Runge-Kutta integration of DAE models at Gaussian (Radau) points
- 2K order (2K-1) method which uses K collocation points
- Algebraically stable (i.e., possesses A, B, AN and BN stability)

B. Analysis of the Optimality Conditions (Kameswaran, B., 2007)

- An equivalence has been established between the KKT conditions of NLP and the variational necessary conditions
- Rates of convergence have been established for the NLP method

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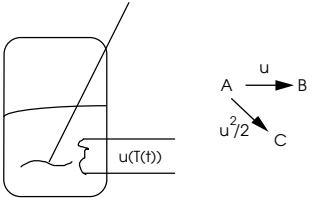
Example: Batch reactor - temperature profile

Maximize yield of B after one hour's operation by manipulating a transformed temperature, $u(t)$.

\Rightarrow Minimize $-z_B(1.0)$
s.t.

$$\begin{aligned} z'_A &= -(u+u^2/2) z_A \\ z'_B &= u z_A \\ z_A(0) &= 1 \\ z_B(0) &= 0 \\ 0 &\leq u(t) \leq 5 \end{aligned}$$

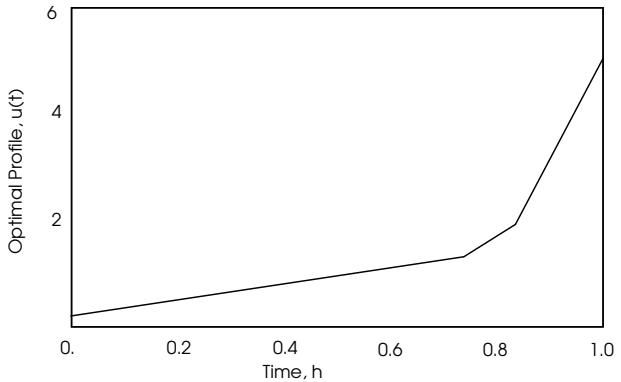
Optimality conditions:

$$\begin{aligned} H &= -\lambda_A(u+u^2/2) z_A + \lambda_B u z_A \\ \partial H/\partial u &= \lambda_A(1+u) z_A + \lambda_B z_A \\ \lambda'_A &= \lambda_A(u+u^2/2) - \lambda_B u, \quad \lambda_A(1.0) = 0 \\ \lambda'_B &= 0, \quad \lambda_B(1.0) = -1 \end{aligned}$$


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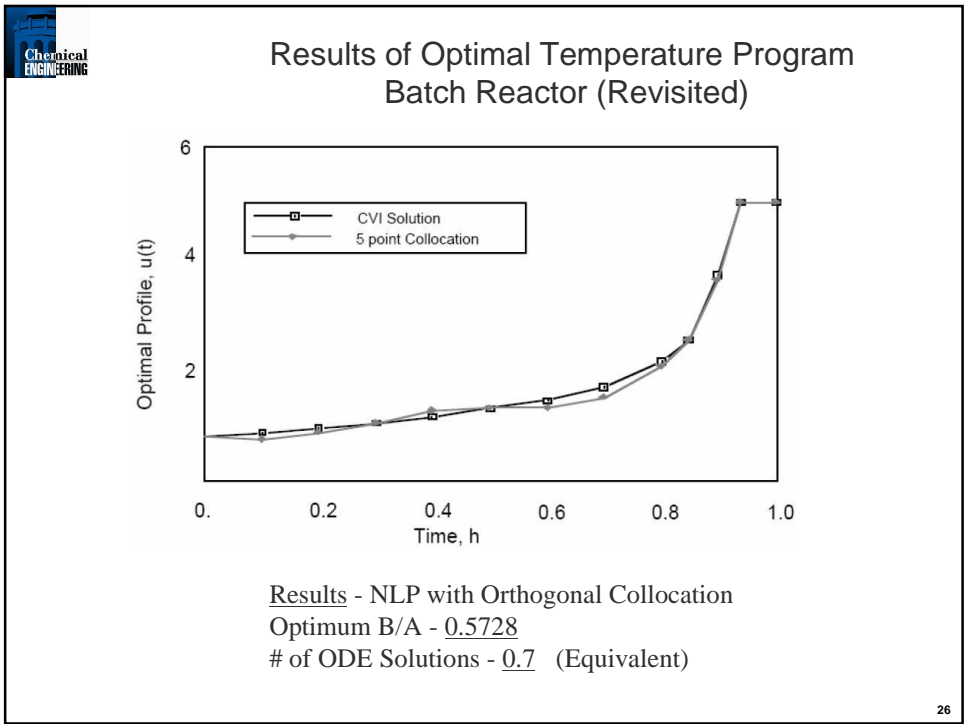
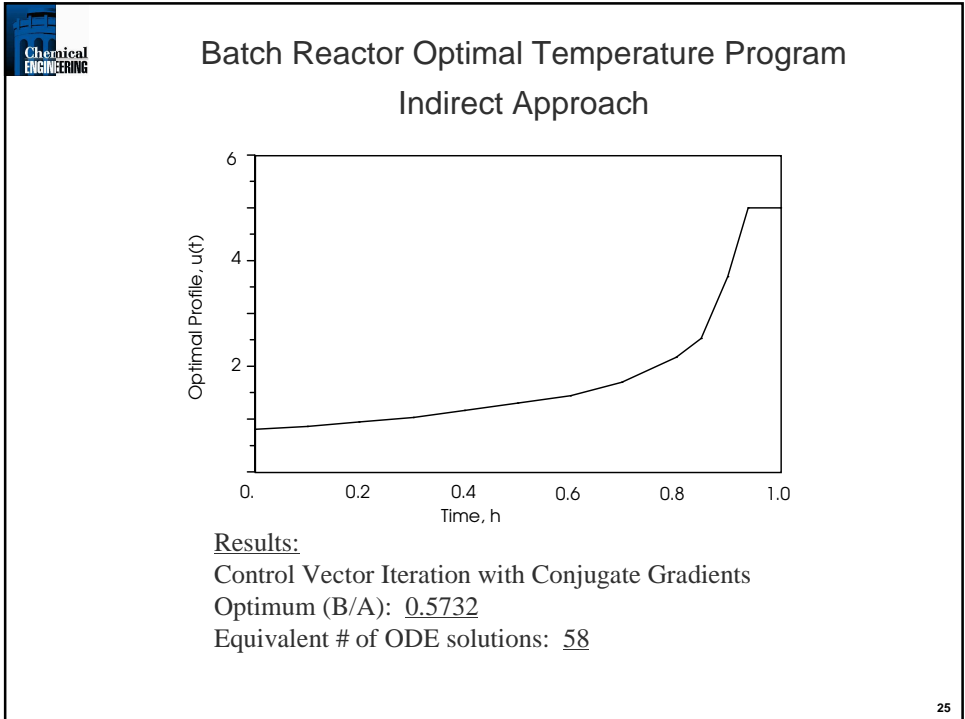
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Batch Reactor Optimal Temperature Program Piecewise Linear



Results:
 Piecewise Linear Approximation with Variable Time Elements
 Optimum B/A: 0.5726
 Equivalent # of ODE solutions: 32

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Dynamic Optimization Engines

Evolution of NLP Solvers:

→ *for dynamic optimization, control and estimation*

SQP

E.g., **NPSOL** and Sequential Dynamic Optimization - over 100 variables and constraints

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Dynamic Optimization Engines

Evolution of NLP Solvers:

→ *for dynamic optimization, control and estimation*

SQP → rSQP

E.g., **SNOPT** and Multiple Shooting - over 100 d.f.s but over 10^5 variables and constraints

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Dynamic Optimization Engines

Evolution of NLP Solvers:

→ *for dynamic optimization, control and estimation*

SQP → rSQP → Full-space Barrier

E.g., *IPOPT* - Simultaneous dynamic optimization over 1 000 000 variables and constraints

Object Oriented Codes tailored to structure, sparse linear algebra and computer architecture (e.g., IPOPT 3.3)

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Barrier Methods for Large-Scale Nonlinear Programming

Original Formulation

$$\begin{aligned} \min_{x \in \mathcal{R}^n} & f(x) \\ \text{s.t.} & c(x) = 0 \\ & x \geq 0 \end{aligned}$$

Can generalize for

$$a \leq x \leq b$$

Barrier Approach

$$\begin{aligned} \min_{x \in \mathcal{R}^n} & \varphi_\mu(x) = f(x) - \mu \sum_{i=1}^n \ln x_i \\ \text{s.t.} & c(x) = 0 \end{aligned}$$

⇒ As $\mu \rightarrow 0$, $x^*(\mu) \rightarrow x^*$ Fiacco and McCormick (1968)

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Solution of the Barrier Problem

⇒ Newton Directions (KKT System)

$$\begin{aligned} \nabla f(x) + A(x)\lambda - v &= 0 \\ Xv - \mu e &= 0 \\ e^T &= [1, 1, 1, \dots] \\ X &= \text{diag}(x) \\ c(x) &= 0 \end{aligned}$$

⇒ Solve



$$\begin{bmatrix} W & A & -I \\ A^T & 0 & 0 \\ V & 0 & X \end{bmatrix} \begin{bmatrix} d_x \\ d_\lambda \\ d_v \end{bmatrix} = - \begin{bmatrix} \nabla f + A\lambda - v \\ c \\ Xv - \mu e \end{bmatrix}$$

IPOPT Code – www.coin-or.org

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Solution of the Barrier Problem

⇒ Newton Directions (KKT System)

$$\begin{aligned} \nabla f(x) + A(x)\lambda - v &= 0 \\ Xv - \mu e &= 0 \\ e^T &= [1, 1, 1, \dots] \\ X &= \text{diag}(x) \\ c(x) &= 0 \end{aligned}$$

⇒ Reducing the System

$$d_v = \mu X^{-1}e - v - X^{-1}Vd_x$$

$$\begin{bmatrix} W + \Sigma & A \\ A^T & 0 \end{bmatrix} \begin{bmatrix} d_x \\ \lambda^+ \end{bmatrix} = - \begin{bmatrix} \nabla \phi_\mu \\ c \end{bmatrix} \quad \Sigma = X^{-1}V$$

IPOPT Code – www.coin-or.org

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IPOPT Algorithm – Features

Line Search Strategies for Globalization

- l_2 exact penalty merit function
- augmented Lagrangian merit function
- Filter method (adapted and extended from Fletcher and Leyffer)

Hessian Calculation

- BFGS (full/LM and reduced space)
- SR1 (full/LM and reduced space)
- Exact full Hessian (direct)
- Exact reduced Hessian (direct)
- Preconditioned CG

Algorithmic Properties

Globally, superlinearly convergent (Wächter and B., 2005)

Easily tailored to different problem structures

Freely Available

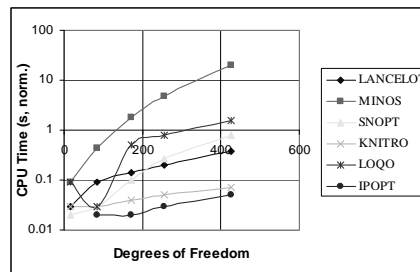
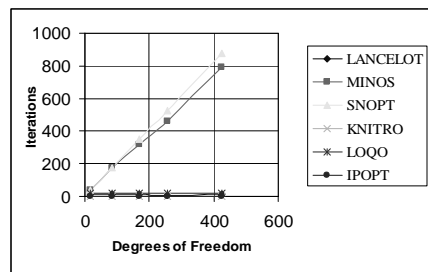
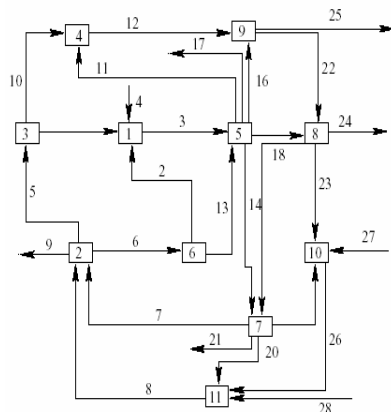
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IPOPT 3.x recently rewritten in C++

Solved on thousands of test problems and applications

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Comparison of NLP Solvers: Data Reconciliation (Poku, Kelly, B. (2004))



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Comparison of Computational Complexity


($\alpha \in [2, 3]$, $\beta \in [1, 2]$, n_w, n_u - assume $N_m = O(N)$)

	Single Shooting	Multiple Shooting	Simultaneous
DAE Integration	$n_w^\beta N$	$n_w^\beta N$	---
Sensitivity	$(n_w N) (n_u N)$	$(n_w N) (n_u + n_w)$	$N (n_u + n_w)$
Exact Hessian	$(n_w N) (n_u N)^2$	$(n_w N) (n_u + n_w)^2$	$N (n_u + n_w)$
NLP Decomposition	---	$n_w^3 N$	---
Step Determination	$(n_u N)^\alpha$	$(n_u N)^\alpha$	$((n_u + n_w)N)^\beta$
Backsolve	---	---	$((n_u + n_w)N)$

$O((n_u N)^\alpha + N^2 n_w n_u + N^3 n_w n_u^2)$
 $O((n_u N)^\alpha + N n_w^3 + N n_w (n_w + n_u)^2)$
 $O((n_u + n_w)N)^\beta$

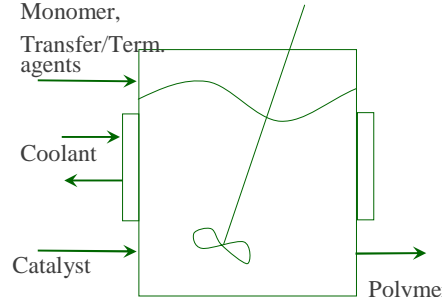
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- Chemical Engineering**
- ### Simultaneous DAE Optimization
- #### Case Studies
- Reactor - Based Flowsheets
 - Fed-Batch Penicillin Fermenter
 - Temperature Profiles for Batch Reactors
 - Parameter Estimation of Batch Data
 - Synthesis of Reactor Networks
 - Batch Crystallization Temperature Profiles
 - Ramping for Continuous Columns
 - Reflux Profiles for Batch Distillation and Column Design
 - Air Traffic Conflict Resolution
 - Satellite Trajectories in Astronautics
 - Batch Process Integration
 - Source Detection for Municipal Water Networks
 - **Optimization of Simulated Moving Beds**
 - **Grade Transition of Polymerization Processes**
 - **Parameter Estimation of Tubular Reactors**
 - **Nonlinear MPC**
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Production of High Impact Polystyrene (HIPS)

Startup and Transition Policies (Flores et al., 2005a)

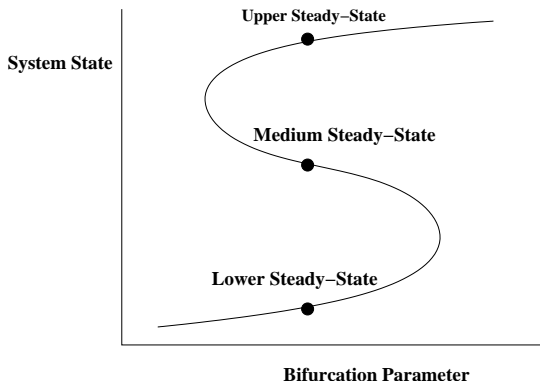


Initiation reactions	
Thermal	$3M_S \xrightarrow{k_{i0}} 2R_S^1$
Chemical	$I \xrightarrow{f_i k_{i1}} 2R$
	$R + M_S \xrightarrow{k_{i1}} R_S^1$
	$R + B_0 \xrightarrow{k_{i2}} B_R$
	$B_R + M_S \xrightarrow{k_{i3}} B_{RS}^1$
Propagation reactions	
	$R_S^j + M_S \xrightarrow{k_p} R_S^{j+1}$
	$B_{RS}^j + M_S \xrightarrow{k_p} B_{RS}^{j+1}$
Definite termination reactions	
Homopolymer	$R_S^j + R_S^m \xrightarrow{k_t} P^{j+m}$
Grafting	$R_S^j + B_R \xrightarrow{k_t} B_P^j$
	$R_S^j + B_{RS}^m \xrightarrow{k_t} B_{RS}^{j+m}$
Crosslinking	$B_R + B_R \xrightarrow{k_t} B_{EB}$
	$B_{RS}^j + B_R \xrightarrow{k_t} B_{PB}^j$
	$B_{RS}^j + B_{RS}^m \xrightarrow{k_t} B_{RS}^{j+m}$
Transfer reactions	
Monomer	$R_S^j + M_S \xrightarrow{k_{fs}} P^j + R_S^1$
	$B_{RS}^j + M_S \xrightarrow{k_{fs}} B_P^j + B_S^1$
Grafting sites	$R_S^j + B_0 \xrightarrow{k_{fs}} P^j + B_R$
	$B_{RS}^j + B_0 \xrightarrow{k_{fs}} B_P^j + B_R$

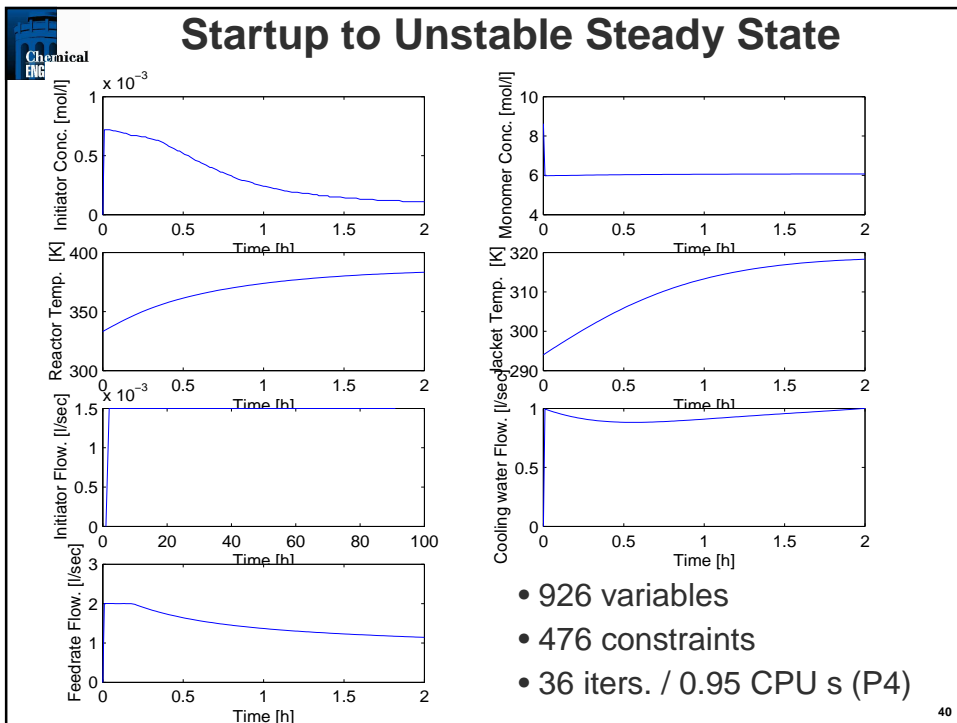
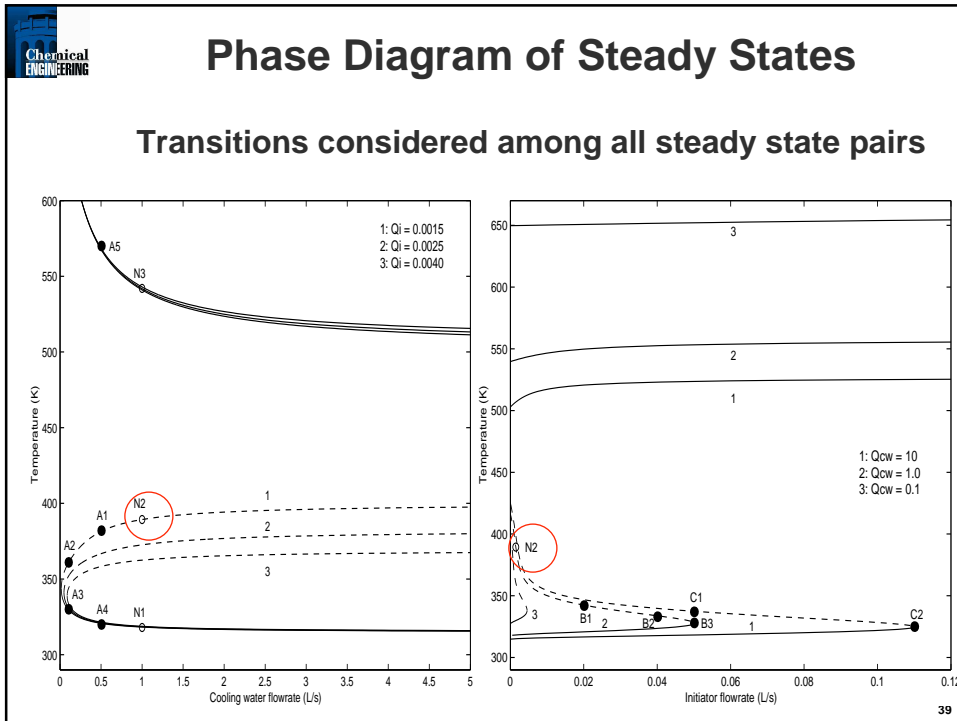


Phase Diagram of Steady States

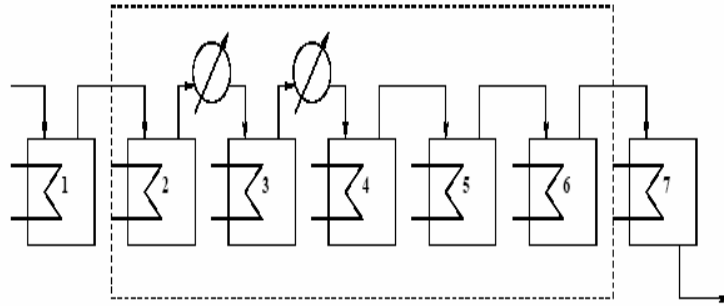
Transitions considered among all steady state pairs



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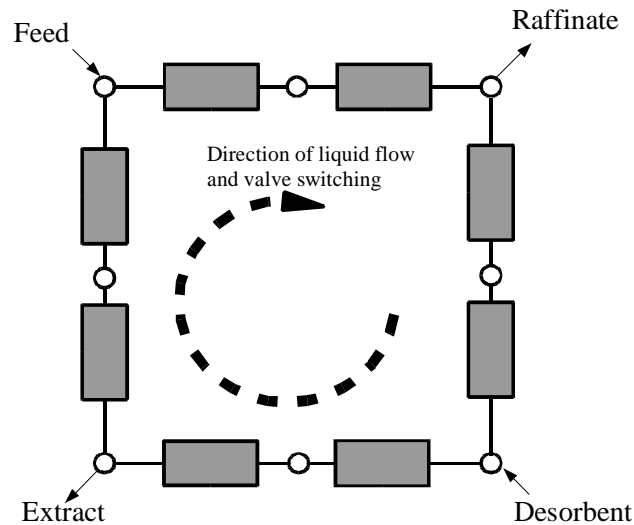
HIPS Process Plant (Flores et al., 2005b)



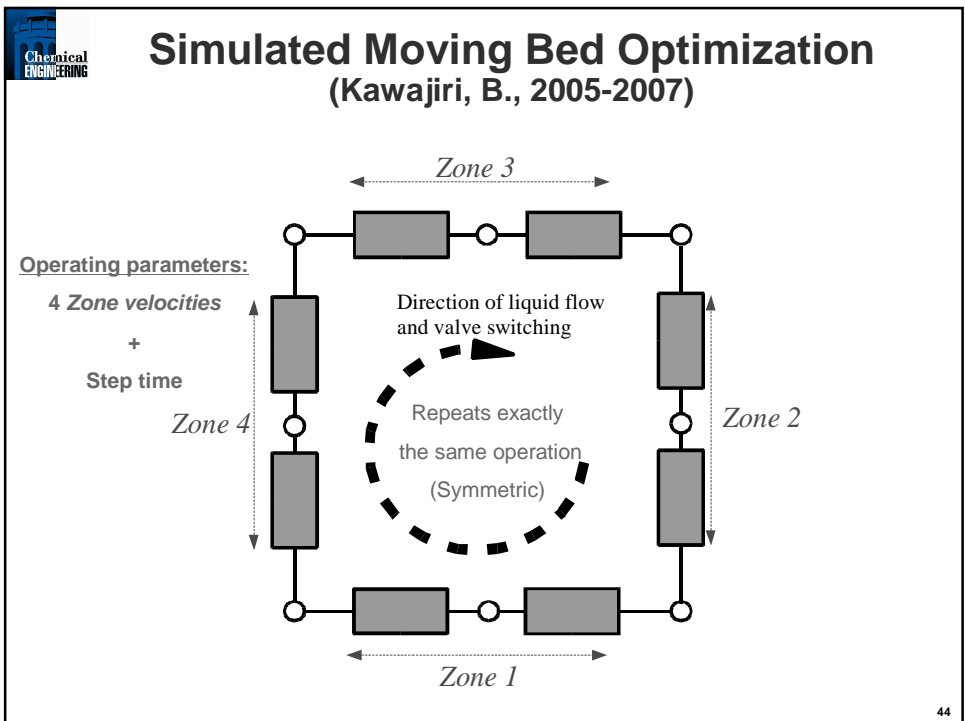
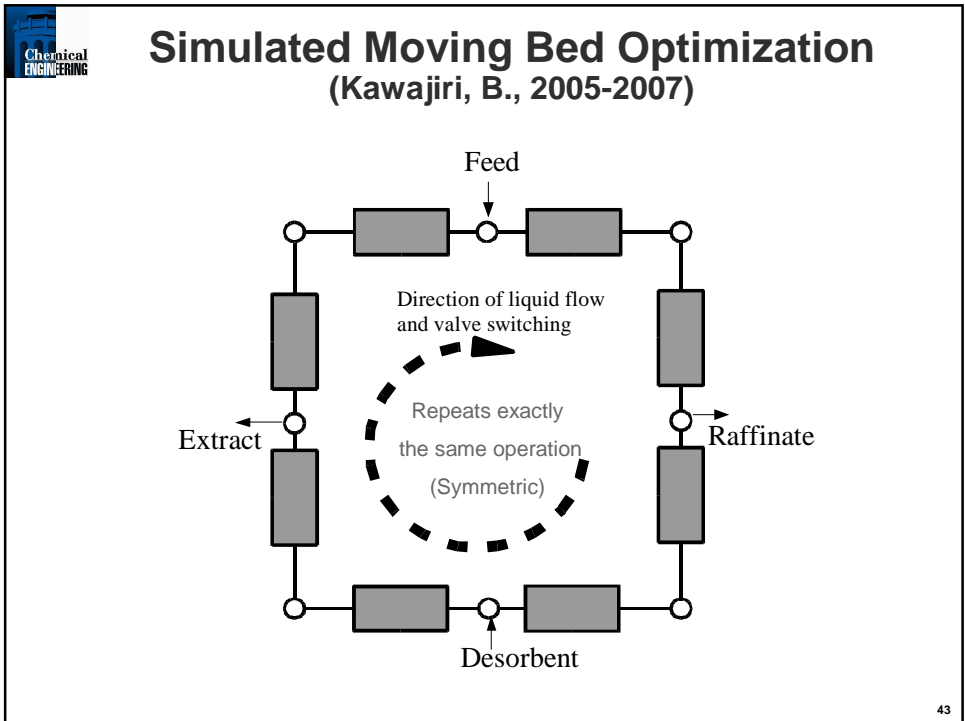
- Many grade transitions considered with stable/unstable pairs
- 1-6 CPU min (P4) with IPOPT
- Study shows benefit for sequence of grade changes to achieve wide range of grade transitions.

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Simulated Moving Bed Optimization (Kawajiri, B., 2005-2007)



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Formulation of Optimization Problem

Zone velocities Step time

$$\max_{u_I(t), u_{II}(t), u_{III}(t), u_{IV}(t)} t_{step}$$

$$\bar{u}_F := \frac{1}{t_{step}} \int_0^{t_{step}} u_F(t) dt$$

(Maximize average feed velocity)

Product requirements

$$(\text{Extract Product Purity}) = \frac{\int_0^{t_{step}} u_E(t) C_{E,k}(t) dt}{\sum_{i=1}^{N_c} \int_0^{t_{step}} u_E(t) C_{E,i}(t) dt} \geq Pur_{min}$$

$$(\text{Extract Product Recovery}) = \frac{\int_0^{t_{step}} u_E(t) C_{E,k}(t) dt}{\int_0^{t_{step}} u_F(t) C_{F,k}(t) dt} \geq Rec_{min}$$

Bounds on liquid velocities

$$u_l \leq u_m(t) \leq u_u \quad m = I, II, III, IV$$

SMB model

$$\epsilon \frac{\partial C_i(x, t)}{\partial t} + (1 - \epsilon) \frac{\partial q_i(x, t)}{\partial t} + u_m \frac{\partial C_i(x, t)}{\partial x} = 0$$

$$(1 - \epsilon) \frac{\partial q_i(x, t)}{\partial t} = K_{app, i} (C_i(x, t) - C_i^{eq}(x, t))$$

$$q_{n,i}(x, t) = K_i C_{n,i}^{eq}(x, t)$$

CSS constraint

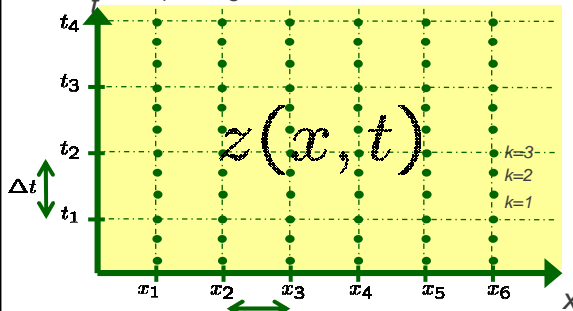
$$C_i(x, t) = C_i(x, t + t_{step})$$

$$q_i(x, t) = q_i(x, t + t_{step})$$

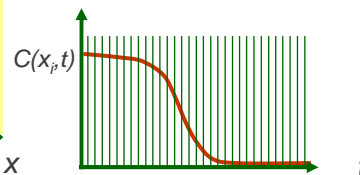
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Treatment of PDEs: Simultaneous Approach

(Orthogonal Collocation on Finite Elements)



Step size is determined a priori



Huge number of variables (handled by optimizer)

$$\min_p \Phi(z(x, t_f))$$

subject to:

$$f_{i,j,k} \left(p, \left(\frac{\Delta z}{\Delta x} \right)_{i,j,k}, \left(\frac{dz}{dt} \right)_{i,j,k} \right) = 0, \quad \left(\frac{\Delta z}{\Delta x} \right)_{i,j,k} = \frac{z_{i+1,j,k} - z_{i-1,j,k}}{x_{i+1,j} - x_{i-1,j}}$$

$$g(p, z(x, t)) \leq 0$$

$$z_{i,j,k} = z_{i,j}^0 + h_j \sum_{k=1}^3 \Omega_{j,k} \left(\frac{dz}{dt} \right)_{i,j,k}$$

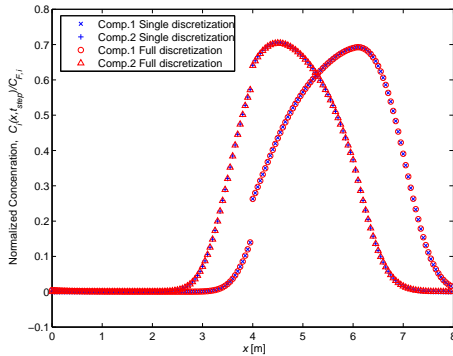
$$h(p, z(x, t)) = 0$$

PDE → Algebraic equations

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Comparison of two approaches

(Linear isotherm, fructose/glucose separation)



Sequential and Simultaneous methods find same optimal solution

Initial feed velocity: 0.01 m/h



Optimization

Optimal feed velocity: 0.52 m/h

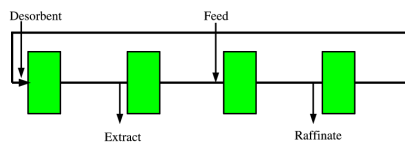
*On Pentium IV 2.8GHz

	# of variables	CPU Time*	# of iteration
Sequential Approach <i>Implemented on gPROMS, solved using SRQPD</i>	644	111.8 min <i>(89% spent by integrator)</i>	49
Simultaneous Approach <i>Implemented on AMPL, solved using IPOPT</i>	33999	1.53 min	47

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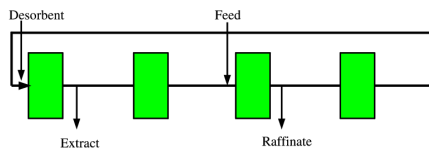
Nonstandard SMB: Addressed by Extended Superstructure NLP

- **Standard SMB**



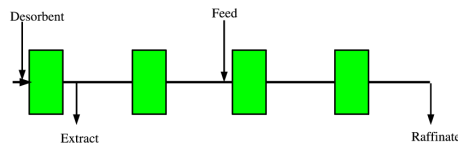
- **VARICOL**

(Asynchronous switching)

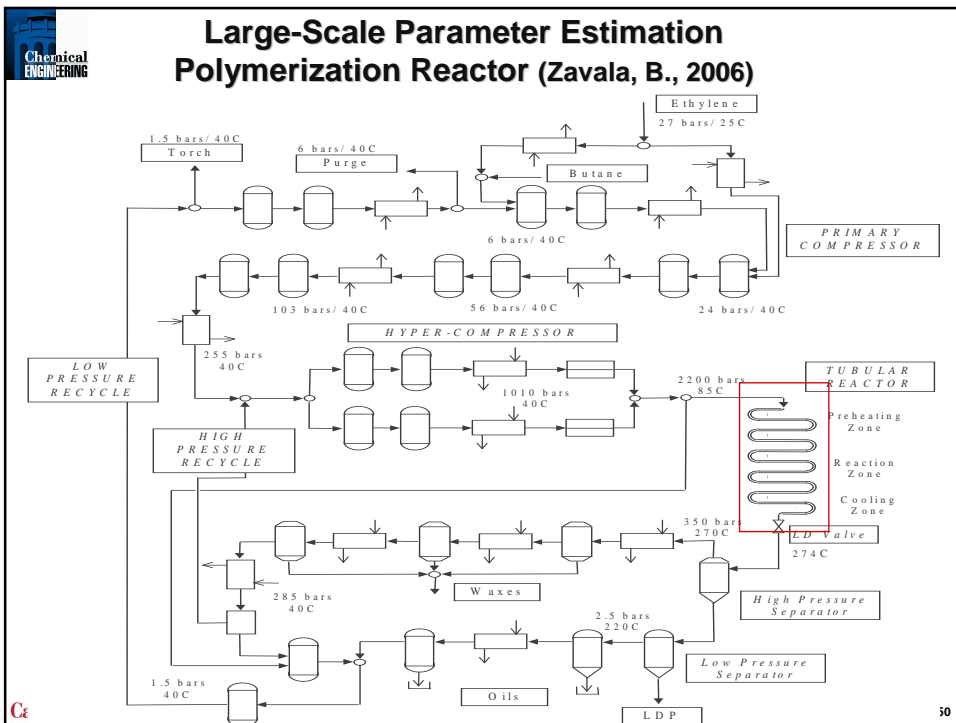
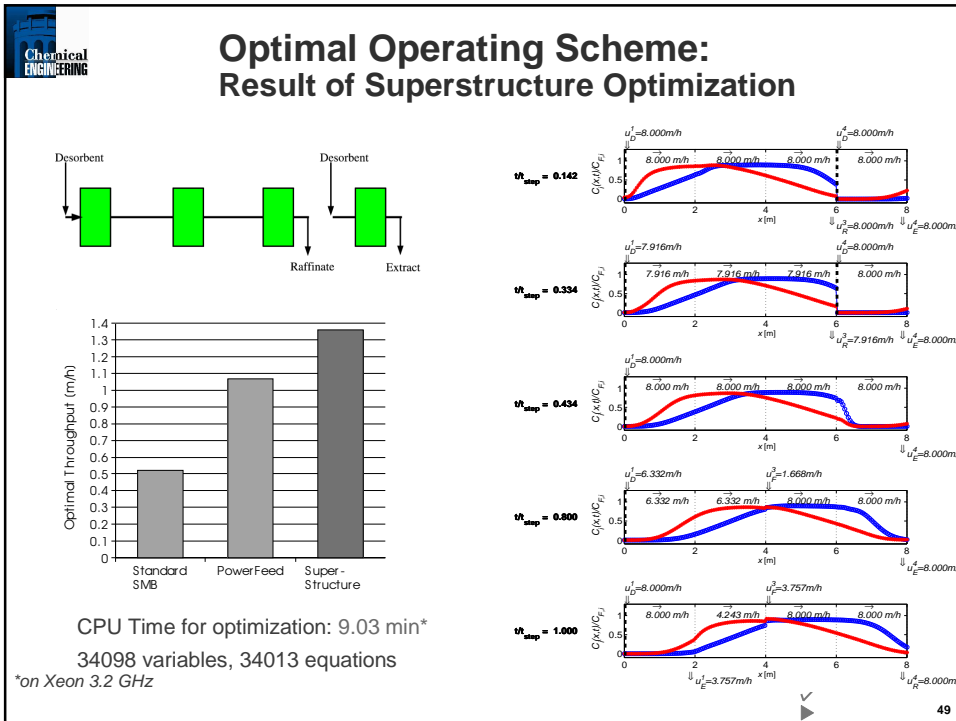


- **Three Zone**

(Circulation loop is cut open)



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Large-Scale Parameter Estimation

Material & Energy $\left\{ \begin{array}{l} F_j \left[\frac{dy_j(z)}{dz}, y_j(z), w_j(z), z, \pi_j, \Pi \right] = 0 \\ G_j \left[y_j(z), w_j(z), z, \pi_j, \Pi \right] = 0 \\ y_j(0) = \phi(y_{j-1}(z_{L_{j-1}}), F_{fj}) \end{array} \right\} j \in \{1..NZ\}$
Physical Properties
Zone Transitions
500 ODEs
1000 AEs

× Stiffness + Highly Nonlinear + Parametric Sensitivity + Algebraic Coupling

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Large-Scale Parameter Estimation

□ Complex Kinetic Mechanisms

Initiator decomposition

$$I_i \xrightarrow{k_{d_i}} 2R \quad i = 1, N_I$$

Chain Initiation

$$R + M_1 \xrightarrow{k_{i1}} P_{1,0}$$

$$R + M_2 \xrightarrow{k_{i2}} Q_{0,1}$$

Chain Propagation

$$P_{r,s} + M_1 \xrightarrow{k_{p11}} P_{r+1,s}$$

$$P_{r,s} + M_2 \xrightarrow{k_{p12}} Q_{r,s+1}$$

$$Q_{r,s} + M_1 \xrightarrow{k_{p21}} P_{r+1,s}$$

$$Q_{r,s} + M_2 \xrightarrow{k_{p22}} Q_{r,s+1}$$

Chain Transfer to Monomer

$$P_{r,s} + M_1 \xrightarrow{k_{fm11}} P_{1,0} + M_{r,s}$$

$$P_{r,s} + M_2 \xrightarrow{k_{fm12}} Q_{0,1} + M_{r,s}$$

$$Q_{r,s} + M_1 \xrightarrow{k_{fm21}} P_{1,0} + M_{r,s}$$

$$Q_{r,s} + M_2 \xrightarrow{k_{fm22}} Q_{0,1} + M_{r,s}$$

Chain Transfer to Solvent

$$P_{r,s} + S_i \xrightarrow{k_{s1i}} P_{1,0} + M_{r,s}$$

$$Q_{r,s} + S_i \xrightarrow{k_{s2i}} Q_{0,1} + M_{r,s}$$

Chain Transfer to Polymer

$$P_{r,s} + M_{x,y} \xrightarrow{k_{fp11}} P_{x,y} + M_{r,s}$$

$$P_{r,s} + M_{x,y} \xrightarrow{k_{fp12}} Q_{x,y} + M_{r,s}$$

$$Q_{r,s} + M_{x,y} \xrightarrow{k_{fp21}} P_{x,y} + M_{r,s}$$

$$Q_{r,s} + M_{x,y} \xrightarrow{k_{fp22}} Q_{x,y} + M_{r,s}$$

Termination by Combination

$$P_{r,s} + P_{x,y} \xrightarrow{k_{tc11}} M_{r+x,s+y}$$

$$P_{r,s} + Q_{x,y} \xrightarrow{k_{tc12}} M_{r+x,s+y}$$

$$Q_{r,s} + Q_{x,y} \xrightarrow{k_{tc22}} M_{r+x,s+y}$$

Termination by Disproportionation

$$P_{r,s} + P_{x,y} \xrightarrow{k_{td11}} M_{r,s} + M_{x,y}$$

$$P_{r,s} + Q_{x,y} \xrightarrow{k_{td12}} M_{r,s} + M_{x,y}$$

$$Q_{r,s} + Q_{x,y} \xrightarrow{k_{td22}} M_{r,s} + M_{x,y}$$

Backbiting

$$P_{r,s} \xrightarrow{k_{b1}} P_{r,s} \text{ or } Q_{r,s}$$

$$P_{r,s} \xrightarrow{k_{b2}} Q_{r,s} \text{ or } P_{r,s}$$

β-scission

$$P_{r,s} \xrightarrow{k_{\beta 1}} M_{r,s}^= + P_{1,0}$$

$$P_{r,s} \xrightarrow{k_{\beta 2}} M_{r,s}^= + Q_{0,1}$$

$k = k_0 \exp\left(-\frac{E_a + P E_v}{RT}\right)$

~ 35 Elementary Reactions
~ 100 Kinetic Parameters

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Large-Scale Parameter Estimation

- Parameter Estimation for Industrial Applications
 - Use Rigorous Model to Match Plant Data Directly
 - Start with Standard Least-Squares Formulation

$$\min_{\Pi, \pi_{k,j}} \sum_{k=1}^{NS} \sum_{j=1}^{NZ} \sum_{i=1}^{NM(j)} (y_{k,j}(z_i) - y_{k,j,i}^M)^T V_y^{-1} (y_{k,j}(z_i) - y_{k,j,i}^M) + \sum_{k=1}^{NS} (w_{k,NZ} - w_{k,NZ}^M)^T V_w^{-1} (w_{k,NZ} - w_{k,NZ}^M)$$

s.t.

$$F'_{k,j} \left[\frac{dy_{k,j}(z)}{dz}, y_{k,j}(z), w_{k,j}(z), z, \pi_{k,j}, \Pi \right] = 0$$

$$G_{k,j} [y_{k,j}(z), w_{k,j}(z), z, \pi_{k,j}, \Pi] = 0$$

$$y_{k,j}(0) = \phi(y_{k,j-1}(z_{L_{k,j-1}}), F_{f_{k,j}})$$

$$j \in \{1..NZ\}, k \in \{1..NS\}$$

Least-Squares

Rigorous Reactor Model

- Special Case of Multi-Stage Dynamic Optimization Problem
 - Solve using Simultaneous Collocation-Based Approach

1 data set 6 data sets
 500 ODEs x 6 3000 ODEs
 1000 AEs → 6000 AEs

Large-Scale Parameter Estimation

- Multi-Zone Tubular Reactor – Quasi Steady-State
 - Data Sets: Operating Conditions and Properties for Different Grades
 - Match: Temperature Profiles and Product Properties
 - On-line Adjusting Parameters → Track Evolution of Disturbances
 - Kinetic Parameters → Development and Discrimination among Rigorous Models
- Results
 - Single Data Set (On-line Adjusting Parameters)

Grade	Constraints	Parameters	LB	UB	Iterations	CPUs	NZJ	NZH
A	11955	32	374	361	11	17.03	166425	87954
B	11283	32	374	361	8	10.06	138666	76890

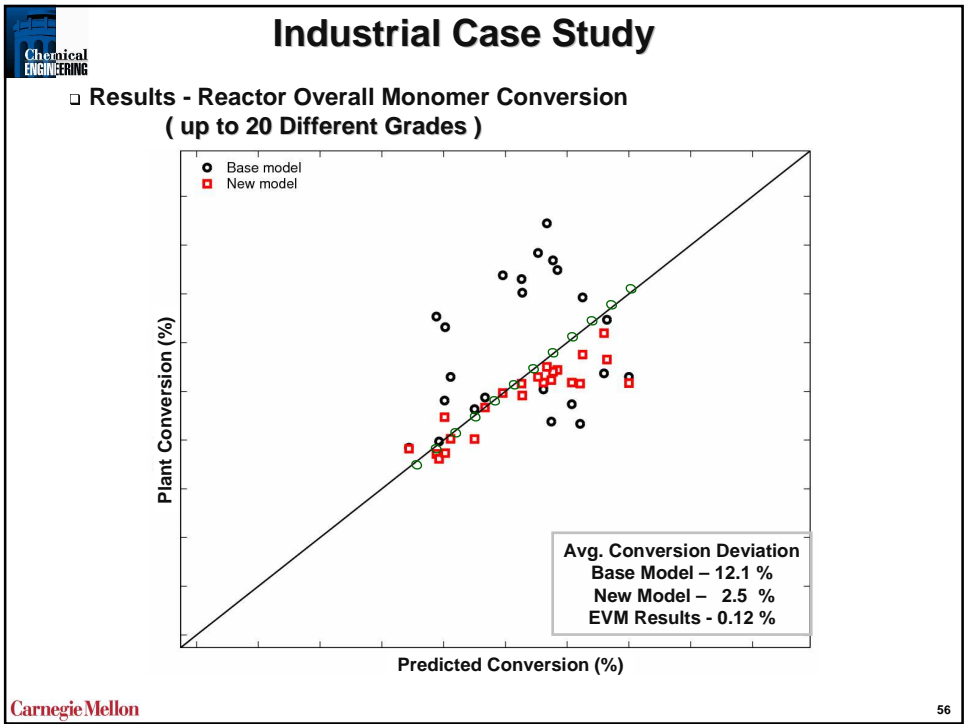
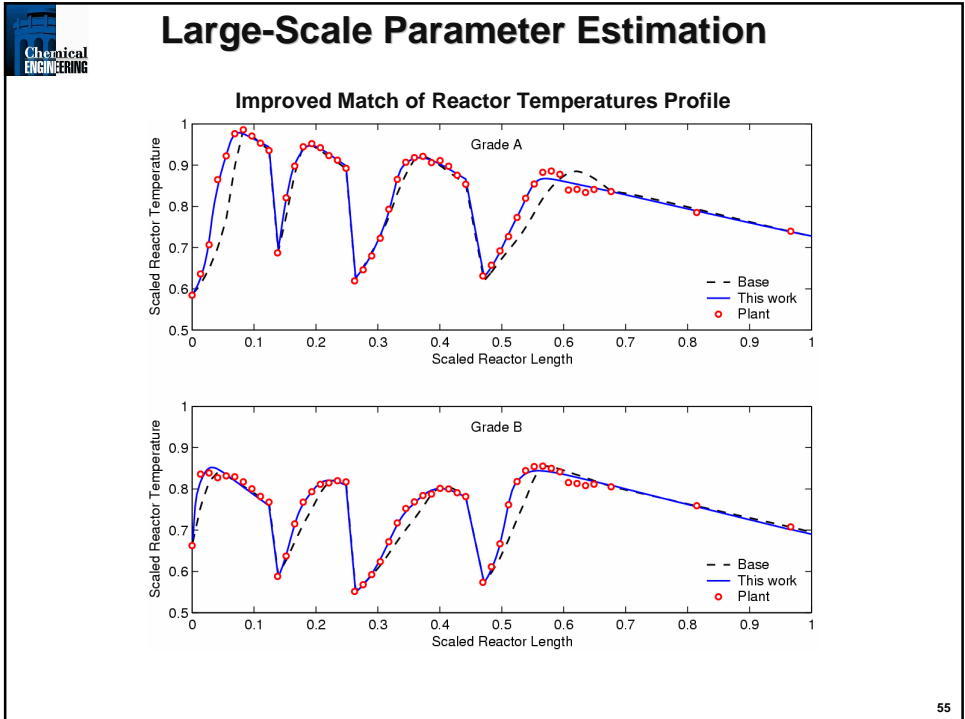
- Multiple Data Sets (On-line Adjusting Parameters + Kinetics)


Data Sets	Constraints	DOF	LB	UB	Iterations	CPUs	NZJ	NZH
3	33900	121	1246	1207	68	451.51	520275	552738
6	68421	217	2467	2389	58	900.21	1058412	1119258

Bottleneck (Memory Requirements) Factorization Step

$$\begin{bmatrix} W(x_k, \lambda_k) & A(x_k) & -I \\ A(x_k)^T & 0 & 0 \\ V_k & 0 & X_k \end{bmatrix} \begin{bmatrix} \Delta x \\ \Delta \lambda \\ \Delta \nu \end{bmatrix} = - \begin{bmatrix} \nabla f(x_k) + A(x_k) \lambda_k - \nu_k \\ c(x_k) \\ X_k V_k e - \mu e \end{bmatrix}$$

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Parameter Estimation in Parallel Architectures

Exploit Structure of KKT Matrix – Laird, B. 2006

$$\min_{\Pi, \pi_{k,j}} \sum_{k=1}^{NS} \sum_{j=1}^{NZ} \sum_{i=1}^{NM(j)} (y_{k,j}(z_i) - y_{k,j,i}^M)^T V_y^{-1} (y_{k,j}(z_i) - y_{k,j,i}^M)$$

$$+ \sum_{k=1}^{NS} (w_{k,NZ} - w_{k,NZ}^M)^T V_w^{-1} (w_{k,NZ} - w_{k,NZ}^M)$$

s.t.

$$\mathbf{F}_{k,j} \begin{bmatrix} \frac{dy_{k,j}(z)}{dz} \\ y_{k,j}(z) \\ w_{k,j}(z) \\ z, \pi_{k,j}, \Pi \end{bmatrix} = 0$$

$$\mathbf{G}_{k,j} [y_{k,j}(z), w_{k,j}(z), z, \pi_{k,j}, \Pi] = 0$$

$$y_{k,j}(0) = \phi(y_{k,j-1}(z_{L_{k,j-1}}), F_{f_{k,j}})$$

$$j \in \{1..NZ\}, k \in \{1..NS\}$$

$$\min f(x)$$

s.t. $c(x) = 0$

$$x \geq 0$$

$$\begin{bmatrix} H_k & A_k & -I \\ A_k^T & 0 & 0 \\ V_k & 0 & X_k \end{bmatrix} \begin{bmatrix} \Delta x \\ \Delta \lambda \\ \Delta \nu \end{bmatrix} = - \begin{bmatrix} r_x \\ r_\lambda \\ X_k V_k e - \mu_\ell e \end{bmatrix}$$

$$\text{in } \sum_{k=1}^{NS} f_k(x_k)$$

s.t. $c_k(x_k, \Pi) = 0$

$$x_k, \Pi \geq 0$$

Direct Factorization MA27

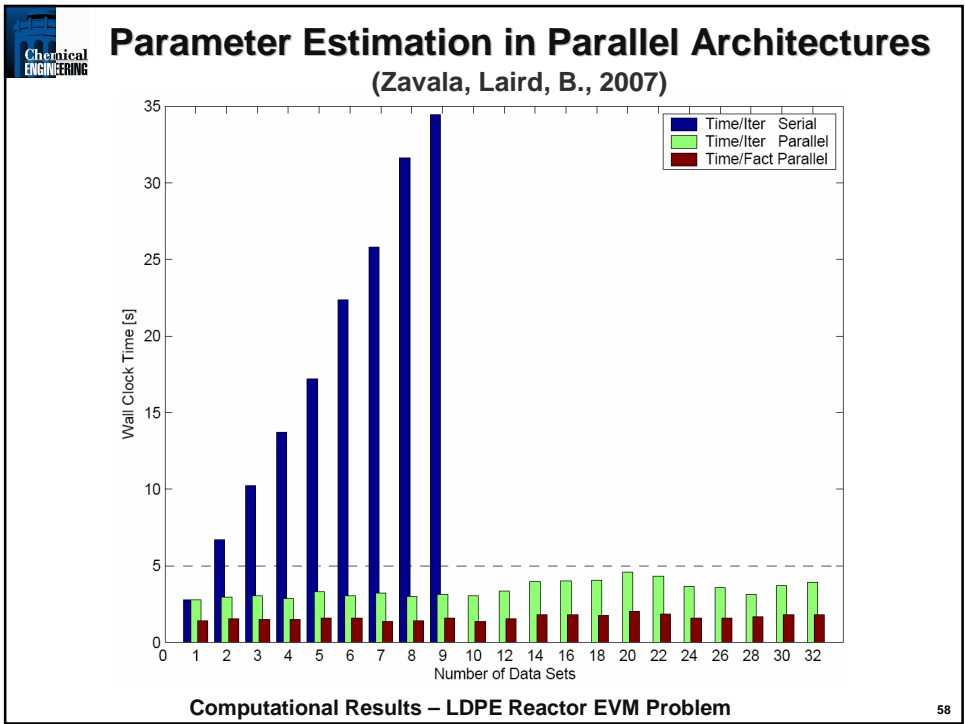
- Memory Bottlenecks
- Factorization Time Scales
- Superlinearly with Data sets



Block-bordered Diagonal Structure

Coarse-Grained Parallelization using Schur Complement Decomposition

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Decision-making in Chemical Industries

Supply Chain, Planning and Scheduling

- Large LP and MILP models
- Many Discrete Decisions
- Few Nonlinearities
- Essential link needed to process models
- **Decisions need to be feasible at lower levels**

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Decision Pyramid for Process Operations

Real-time Optimization and Advanced Process Control

- Fewer discrete decisions
- Many nonlinearities
- Frequent, “on-line” time-critical solutions
- Higher level decisions must be feasible
- Performance communicated for higher level decisions

Off-line (open loop)

On-line (closed loop)

$MPC \subset APC$

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Chemical Engineering

Dynamic Real-time Optimization

Integrate On-line Optimization/Control with Off-line Planning

- Consistent, first-principle models
- Consistent, long-range, multi-stage planning
- Increase in computational complexity
- Time-critical calculations

Applications

- Batch processes
- Grade transitions
- Cyclic reactors (coking, regeneration...)
- Cyclic processes (PSA, SMB...)

Continuous processes are never in steady state:

- Feed changes
- Nonstandard operations
- Optimal disturbance rejections

Simulation environments and first principle dynamic models are widely used for off-line studies

Can these results be implemented directly on-line for large-scale systems?

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Chemical Engineering

Nonlinear Model Predictive Control (NMPC)

NMPC Estimation and Control

Why NMPC?

- Track a profile
- Severe nonlinear dynamics (e.g, sign changes in gains)
- Operate process over wide range (e.g., startup and shutdown)

NMPC Subproblem

$$\min_u \sum \|y(t) - y^{sp}\|_{Q_y}^2 + \sum \|u(t^k) - u(t^{k-1})\|_{Q_u}^2$$

s.t.

$$z'(t) = F(z(t), y(t), u(t), t)$$

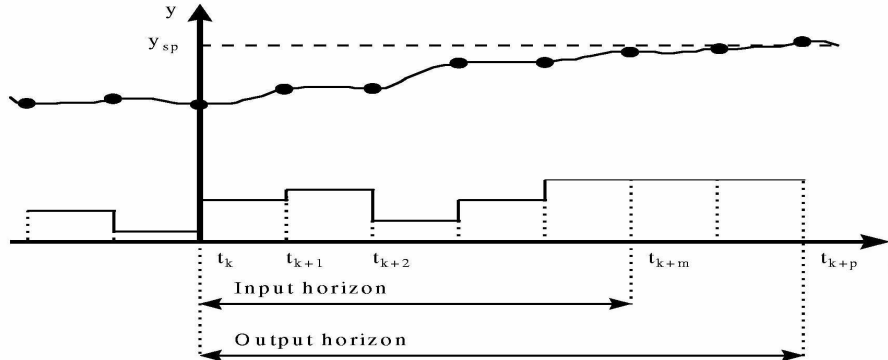
$$0 = G(z(t), y(t), u(t), t)$$

$$z(t) = z^{init}$$

Bound Constraints
Other Constraints

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Nonlinear Model Predictive Control (NMPC)



$$\min_u \sum \|y(t) - y^{sp}\|_{Q_y}^2 + \sum \|u(t^k) - u(t^{k-1})\|_{Q_u}^2$$

$$s.t. \quad z'(t) = F(z(t), y(t), u(t), t)$$

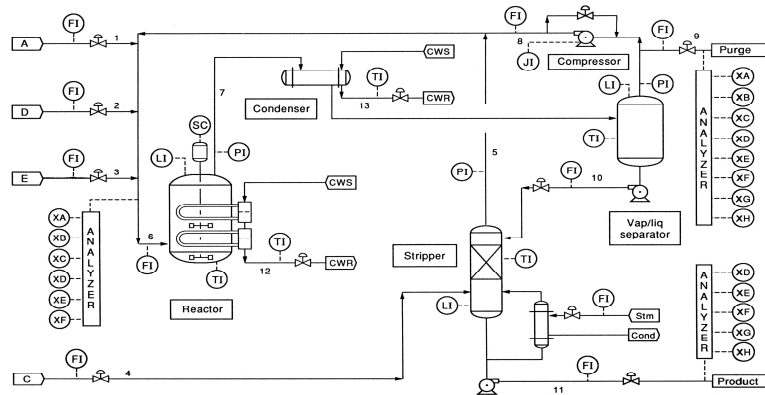
$$0 = G(z(t), y(t), u(t), t)$$

$$z(t) = z^{init}$$

Bound Constraints
Other Constraints

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Tennessee Eastman Process (Downs and Vogel, 1993)



Unstable Reactor

11 Controls; Product, Purge streams

Model extended with energy balances

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Tennessee Eastman NMPC Model (Jockenhövel, Wächter, B., 2003)

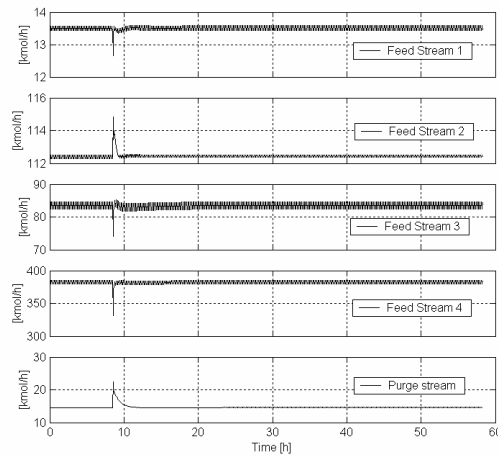
DAE Model		NLP Optimization problem	
Number of differential equations	30	Number of variables of which are fixed	10920 0
Number of algebraic variables	152	Number of constraints	10260
Number of algebraic equations	141	Number of lower bounds	780
Difference (control variables)	11	Number of upper bounds	540
		Number of nonzeros in Jacobian	49230
		Number of nonzeros in Hessian	14700

Method of Full Discretization of State and Control Variables

Large-scale Sparse block-diagonal NLP

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Case Study: Change Reactor pressure by 60 kPa



Control profiles

All profiles return to their base case values

Same production rate

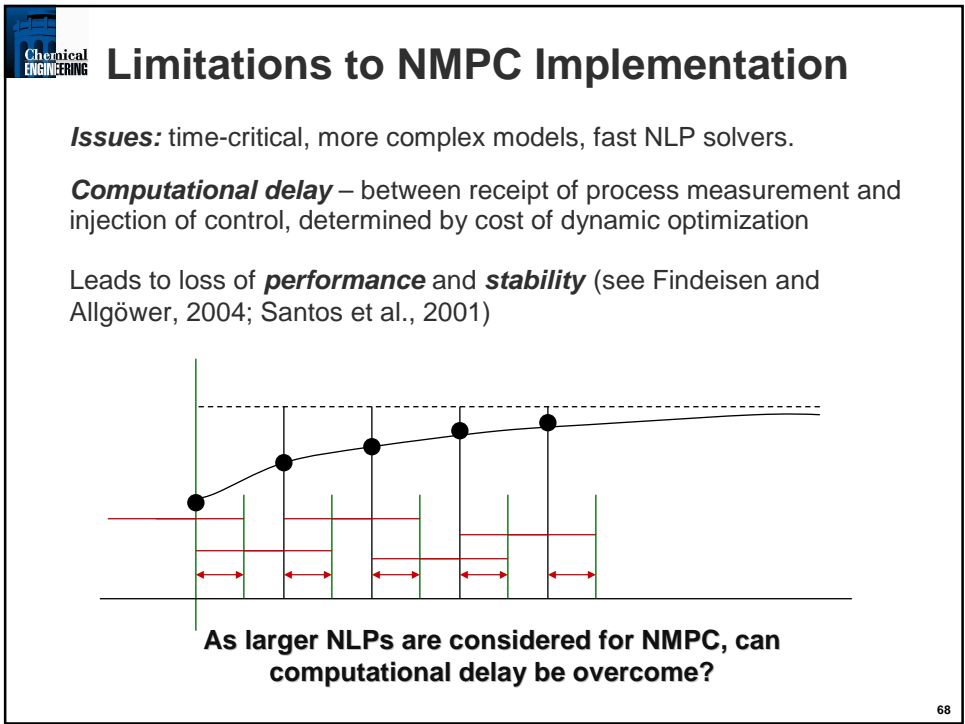
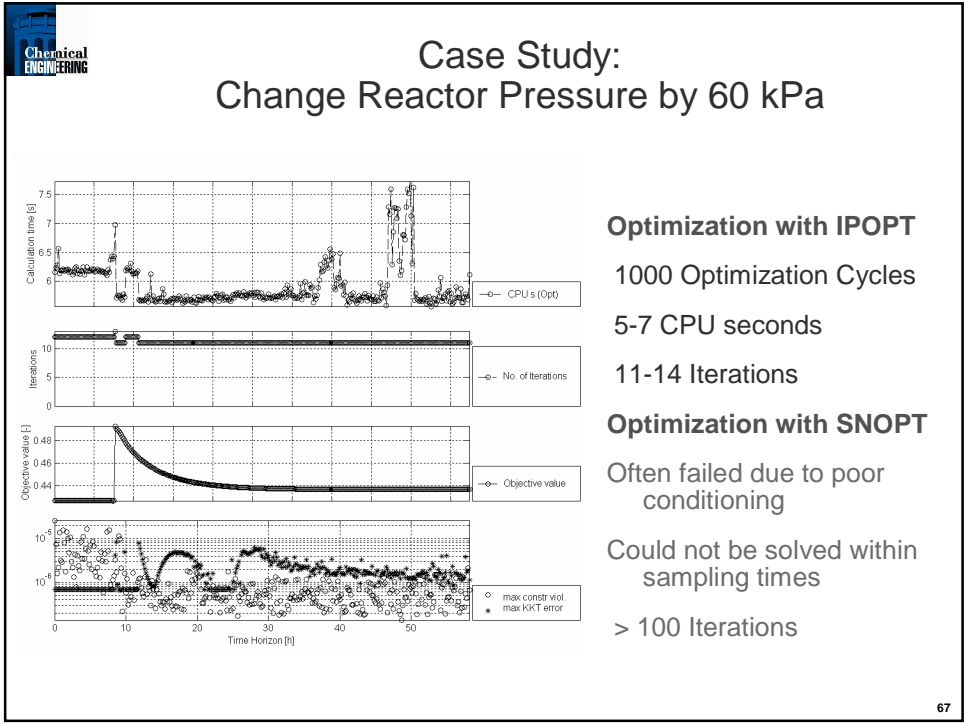
Same product quality

Same control profile

Lower pressure – leads to larger gas phase (reactor) volume

Less compressor load

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Avoid computational delay due to on-line optimization?

Real-time Iteration

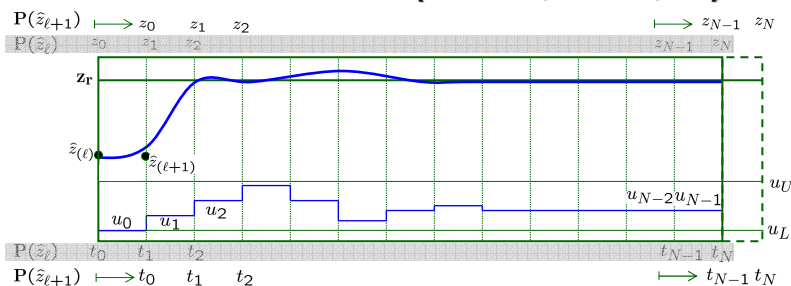
- preparation, feedback response and transition stages
- solve perturbed (linearized) problem on-line
 - Li, de Oliveira, Santos, B. (1990+)
 - Diehl, Findeisen, Bock, Allgöwer et al. (2000+)
 - > two orders of magnitude reduction in on-line computation
- solve complete NLP in background (“between” sampling times as part of preparation and transition stages)

Based on NLP sensitivity for dynamic systems

- Extended to Simultaneous Collocation approach – Zavala et al. (2007)
- Develop Advanced Step NMPC
- Related to MPC with linearization constantly updated one step behind

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Nonlinear Model Predictive Control – Parametric Problem (Zavala, Laird, B.)



$$\begin{aligned}
 \mathcal{P}(x(k), N) \quad & \min_{v_{l|k}} J(x(k), N) = F(z_{k+N|k}) + \sum_{l=k}^{k+N-1} \psi(z_{l|k}, v_{l|k}) \\
 \text{s. t.:} \quad & z_{l+1|k} = f(z_{l|k}, v_{l|k}), \quad l = k, \dots, k+N-1 \\
 & \boxed{z_{k|k} = x(k) = p_0} \\
 & z_{l|k} \in \mathbb{X}, z_{k+N|k} \in \mathbb{X}_f, v_{l|k} \in \mathbb{U}.
 \end{aligned}
 \left. \vphantom{\begin{aligned} \min_{v_{l|k}} J(x(k), N) = F(z_{k+N|k}) + \sum_{l=k}^{k+N-1} \psi(z_{l|k}, v_{l|k}) \\ z_{l+1|k} = f(z_{l|k}, v_{l|k}), \quad l = k, \dots, k+N-1 \\ z_{k|k} = x(k) = p_0 \\ z_{l|k} \in \mathbb{X}, z_{k+N|k} \in \mathbb{X}_f, v_{l|k} \in \mathbb{U}. \end{aligned}} \right\} \mathcal{P}(p_0)$$

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Chemical Engineering

Nonlinear Model Predictive Control – Parametric Problem (Zavala, Laird, B.)

$$\begin{aligned}
 \mathcal{P}(x(k), N) \quad & \min_{v_{l|k}} J(x(k), N) = F(z_{k+N|k}) + \sum_{l=k}^{k+N-1} \psi(z_{l|k}, v_{l|k}) \\
 \text{s. t.} \quad & z_{l+1|k} = f(z_{l|k}, v_{l|k}), \quad l = k, \dots, k+N-1 \\
 & z_{k|k} = x(k) = p_0 \\
 & z_{l|k} \in \mathbb{X}, z_{k+N|k} \in \mathbb{X}_f, v_{l|k} \in \mathbb{U}.
 \end{aligned}
 \left. \vphantom{\begin{aligned} \mathcal{P}(x(k), N) \\ \text{s. t.} \end{aligned}} \right\} \mathcal{P}(p_0)$$

$$\underbrace{\left. \begin{aligned}
 \mathcal{P}(x(k+1), N) \quad & \min_{v_{l|k+1}} J(x(k+1), N) = F(z_{k+N+1|k+1}) + \sum_{l=k+1}^{k+N} \psi(z_{l|k+1}, v_{l|k+1}) \\
 \text{s. t.} \quad & z_{l+1|k+1} = f(z_{l|k+1}, v_{l|k+1}), \quad l = k+1, \dots, k+N \\
 & z_{k|k+1} = x(k+1) = p \\
 & z_{l|k+1} \in \mathbb{X}, z_{k+N+1|k+1} \in \mathbb{X}_f, v_{l|k+1} \in \mathbb{U}.
 \end{aligned} \right\} \mathcal{P}(p)$$

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Chemical Engineering

NLP Sensitivity

Parametric Programming

$$\begin{aligned}
 \min \quad & f(x, p) \\
 \text{s. t.} \quad & c(x, p) = 0 \\
 & x \geq 0
 \end{aligned}
 \left. \vphantom{\begin{aligned} \min \\ \text{s. t.} \end{aligned}} \right\} \mathcal{P}(p)$$

Solution Triplet

$$s^*(p)^T = [x^{*T} \quad \lambda^{*T} \quad \nu^{*T}]$$

Optimality Conditions $\mathcal{P}(p)$

$$\begin{aligned}
 \nabla_x f(x, p) + \nabla_x c(x, p) \lambda - \nu &= 0 \\
 c(x, p) &= 0 \\
 XVe &= 0
 \end{aligned}$$

NLP Sensitivity → Rely upon Existence and Differentiability of $s^*(p)$

→ Main Idea: Obtain $\left. \frac{\partial s}{\partial p} \right|_{p_0}$ and find $\tilde{s}^*(p_1)$ by Taylor Series Expansion $\tilde{s}^*(p_1)$

$$\tilde{s}^*(p_1) \approx s^*(p_0) + \left. \frac{\partial s^T}{\partial p} \right|_{p_0} (p_1 - p_0)$$

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NLP Sensitivity

Obtaining $\left. \frac{\partial s}{\partial p} \right|_{p_0}$

Optimality Conditions of $P(p)$

$$\left. \begin{aligned} \nabla_x \mathcal{L} = \nabla_x f(x, p) + \nabla_x c(x, p) \lambda - \nu &= 0 \\ c(x, p) &= 0 \\ XVe &= 0 \end{aligned} \right\} Q(s, p) = 0$$

Apply Implicit Function Theorem to $Q(s, p) = 0$ around $(p_0, s^*(p_0))$

$$\frac{\partial Q(s^*(p_0), p_0)}{\partial s} \left. \frac{\partial s}{\partial p} \right|_{p_0} + \frac{\partial Q(s^*(p_0), p_0)}{\partial p} = 0$$

$$\begin{bmatrix} W(s^*(p_0)) & A(x^*(p_0)) & -I \\ A(x^*(p_0))^T & 0 & 0 \\ V^*(p_0) & 0 & X^*(p_0) \end{bmatrix} \begin{bmatrix} \frac{\partial x}{\partial p} \\ \frac{\partial \lambda}{\partial p} \\ \frac{\partial \nu}{\partial p} \end{bmatrix} + \begin{bmatrix} \nabla_{x,p} \mathcal{L}(s^*(p_0)) \\ \nabla_p c(x^*(p_0)) \\ 0 \end{bmatrix} = 0$$

KKT Matrix IPOPT

- $\begin{bmatrix} W(x_k, \lambda_k) & A(x_k) & -I \\ A(x_k)^T & 0 & 0 \\ V_k & 0 & X_k \end{bmatrix}$ → **Already Factored at Solution**
- **Sensitivity Calculation from Single Backsolve**
- **Approximate Solution Retains Active Set**

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Key Concept – Relate to Previous Horizon

$P(x(k), N) \quad \min_{v_{l|k}} J(x(k), N) = F(z_{k+N|k}) + \sum_{l=k}^{k+N-1} \psi(z_{l|k}, v_{l|k})$

s. t.:

- $z_{l+1|k} = f(z_{l|k}, v_{l|k}), \quad l = k, \dots, k+N-1$
- $z_{k|k} = x(k) = p_0$
- $z_{l|k} \in \mathbb{X}, z_{k+N|k} \in \mathbb{X}_f, v_{l|k} \in \mathbb{U}$

Solutions to both problems are equivalent in nominal case (ideal plant model, no disturbances)

$$\bar{P}(x(k-1), N+1) \quad \min_{v_{l|k}} J(x(k-1), N) = F(z_{k+N|k-1}) + \sum_{l=k}^{k+N-1} \psi(z_{l|k}, v_{l|k})$$

s. t.:

- $z_{l+1|k-1} = f(z_{l|k}, v_{l|k}), \quad l = k, \dots, k+N-1$
- $z_{k|k-1} = f[x(k-1), u(k-1)]$
- $z_{l|k} \in \mathbb{X}, z_{k+N|k-1} \in \mathbb{X}_f, v_{l|k} \in \mathbb{U}$

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Advanced Step NMPC
 Combine advanced step with sensitivity to solve NLP in background (between steps) – not on-line

$$\min_{v_{l|k}} J(x(k), N) = F(z_{k+N|k}) + \sum_{l=k}^{k+N-1} \psi(z_{l|k}, v_{l|k})$$

$$\text{s. t.: } z_{k+1|k} = f(x(k), u(k)),$$

$$z_{l+1|k} = f(z_{l|k}, v_{l|k}), \quad l = k+1, \dots, k+N-1$$

$$z_{k|k} = z_0$$

$$\begin{bmatrix} W_k & A_k & -I \\ A_k^T & 0 & 0 \\ V_k & 0 & X_k \end{bmatrix} \begin{bmatrix} \Delta x \\ \Delta \lambda \\ \Delta v \end{bmatrix} = K \Delta v$$

$$z_{l|k} \in \mathbb{X}, z_{k+N|k} \in \mathbb{X}_f, v_{l|k} \in \mathbb{U}.$$

Solve $P(z_\ell)$ in background (between t_0 and t_1)

Advanced Step NMPC
 Combine advanced step with sensitivity to solve NLP in background (between steps) – not on-line

$$\min_{v_{l|k}} J(x(k), N) = F(z_{k+N|k}) + \sum_{l=k}^{k+N-1} \psi(z_{l|k}, v_{l|k})$$

$$\text{s. t.: } z_{k+1|k} = f(x(k), u(k)),$$

$$z_{l+1|k} = f(z_{l|k}, v_{l|k}), \quad l = k+1, \dots, k+N-1$$

$$z_{k|k} = z_0 + \Delta s$$

$$z_{k+1|k} = z_1 = x(k+1)$$

$$\begin{bmatrix} K & E_0 \\ E_1^T & 0 \end{bmatrix} \begin{bmatrix} \Delta v \\ \Delta s \end{bmatrix} = - \begin{bmatrix} 0 \\ \hat{z}(\ell+1) - z_1^* \end{bmatrix}$$

$$z_{l|k} \in \mathbb{X}, z_{k+N|k} \in \mathbb{X}_f, v_{l|k} \in \mathbb{U}.$$

Solve $P(z_\ell)$ in background (between t_0 and t_1)
 Sensitivity to updated problem to get (z_0, u_0)

Advanced Step NMPC

Combine advanced step with sensitivity to solve NLP in background (between steps) – not on-line

$$\min_{v_{l|k}} J(x(k), N) = F(z_{k+N|k}) + \sum_{l=k}^{k+N-1} \psi(z_{l|k}, v_{l|k})$$

$$\text{s. t.: } z_{k+1|k} = f(x(k), u(k)),$$

$$z_{l+1|k} = f(z_{l|k}, v_{l|k}), \quad l = k+1, \dots, k+N-1$$

$$z_{k|k} = z_0 + \Delta s$$

$$z_{k+1|k} = z_1 = x(k+1)$$

$$z_{l|k} \in \mathbb{X}, z_{k+N|k} \in \mathbb{X}_f, v_{l|k} \in \mathbb{U}.$$

$$\begin{bmatrix} W_k & A_k & -I \\ A_k^T & 0 & 0 \\ V_k & 0 & X_k \end{bmatrix} \begin{bmatrix} \Delta x \\ \Delta \lambda \\ \Delta v \end{bmatrix} = K \Delta v$$

$$\begin{bmatrix} K & E_0 \\ E_1^T & 0 \end{bmatrix} \begin{bmatrix} \Delta v \\ \Delta s \end{bmatrix} = - \begin{bmatrix} 0 \\ \bar{z}(\ell+1) - z_1^* \end{bmatrix}$$

Solve $P(z_\ell)$ in background (between t_0 and t_1)

Sensitivity to updated problem to get (z_0, u_0)

Solve $P(z_{\ell+1})$ in background with new (z_0, u_0)

AS-NMPC Stability Analysis

Nominal NMPC stability proof

- Nominal case – no noise: perfect model
- General formulation with local asymptotic controller for $t \rightarrow \infty$
- Advanced step controller satisfies same relations, has same input sequence
→ shares identical stability property

Plant
$$x_{k+1} = \bar{f}(x_k, u_k) = f(x_k, u_k) + g(x_k, u_k, w_k)$$

$$\|g(x_k, u_k, w_k)\| \leq L_J \|x_k\| + \sigma(\|w_k\|)$$

Model
$$z_{l+1} = f(z_l, u_l), z_0 = x_k$$

Robust Stability Margins

- Analysis similar to Limon, Alamo, Camacho (2004), Magni and Scattolini (2005)
- Advanced step NMPC is ISS and tolerates some model mismatch
- ISS property (Jiang and Wang, 2001; Magni and Scattolini, 2005)
- Advanced step NMPC has smaller margin than Ideal NMPC,
→ but can be implemented without computational delay

CSTR NMPC Example (Hicks and Ray)

$$\min_{v_{|k}} \sum_{l=k}^{k+N-1} Q_c(z_{l|k}^c)^2 + Q_t(z_{l|k}^t)^2 + R(v_{l|k})^2$$

$$\text{s.t. } z_{l+1|k}^c = \frac{1}{\theta}(1 - (z_{l|k}^c + z_{ss}^c)) - k_0 \exp\left(-\frac{E_a}{z_{l|k}^t + z_{ss}^t}\right)(z_{l|k}^c + z_{ss}^c)$$

$$z_{l+1|k}^t = \frac{1}{\theta}(t_f - (z_{l|k}^t + z_{ss}^t)) + k_0 \exp\left(-\frac{E_a}{z_{l|k}^t + z_{ss}^t}\right)z_{l|k}^c - \alpha(v + v_s s)((z_{l|k}^t + z_{ss}^t) - t_c)$$

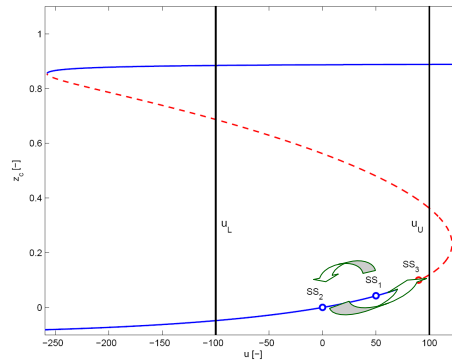
$$z_{k|k}^c = x^c(k), \quad z_{k|k}^t = x^t(k)$$

$$z_{k+N|k}^c = 0 \quad z_{k+N|k}^t = 0, \quad u^U \leq v_{l|k} \leq u^L$$

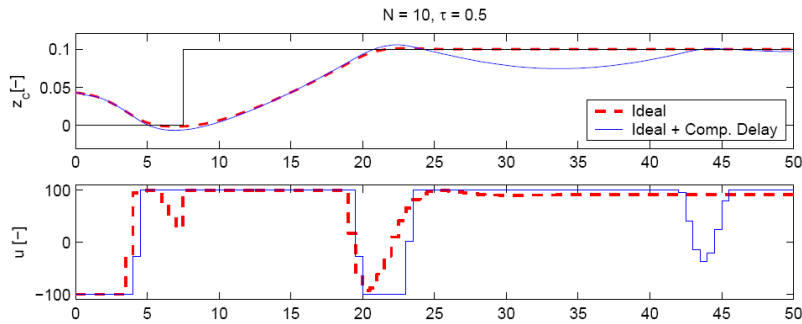
- Maintain unstable setpoint
- Close to bound constraint
- Final time constraint for stability

Effects of:

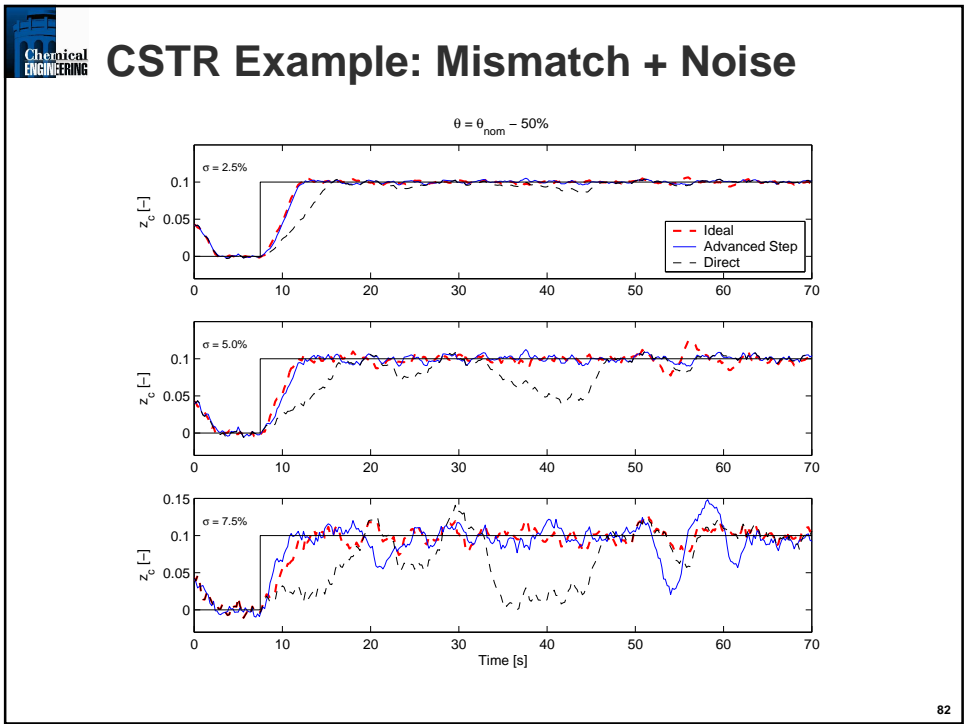
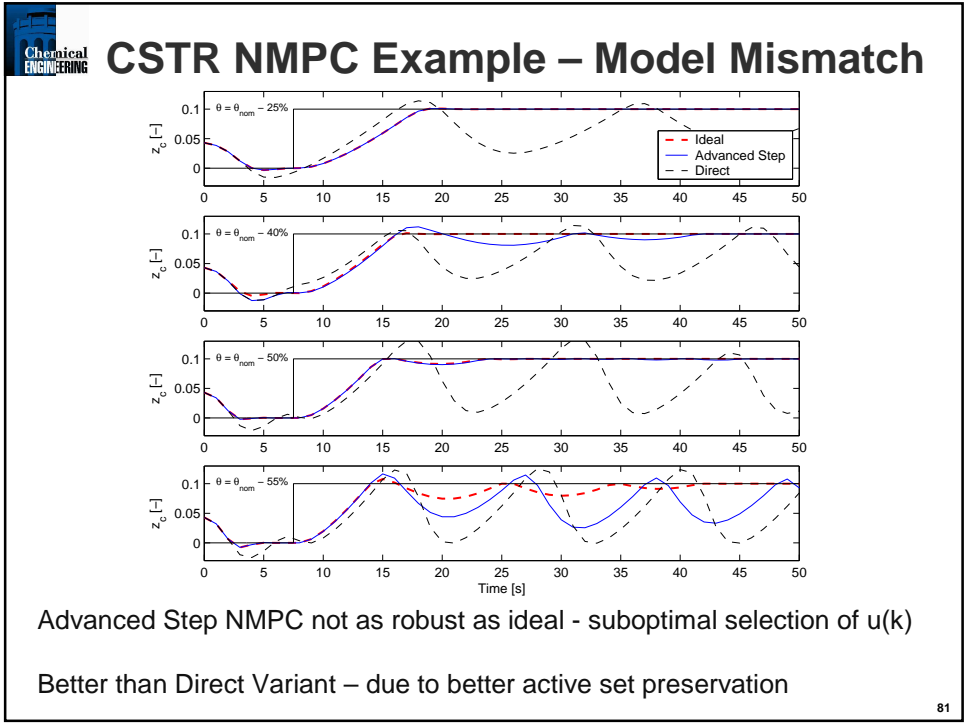
- Computational Delay
- Measurement Noise
- Model Mismatch
- Advanced Step NMPC



CSTR NMPC Example – Nominal Case



- NMPC applied with $N = 10$, $\tau = 0.5$ sampling time
- Stable ($z = 0$) and unstable ($z = 0.1$) steady states
- u_2^* close to upper bound
- Computational delay = 0.5, leads to instabilities



Chemical Engineering

Industrial Case Study – Grade Transition Control

Process Model: 289 ODEs, 100 AEs

$$\min \int_{t_\ell}^{t_\ell+t_p} (w_{C_4}(t) - w_{C_4}^r)^2 + (F_{C_4}(t) - F_{C_4}^r)^2 + (F_{pu}(t) - F_{pu}^r)^2$$

s.t.

PDEs+ODEs

$z(t = t_\ell) = \tilde{z}(\ell)$

$z_L \leq z \leq z_U$

$y_L \leq y \leq y_U$

$u_L \leq u \leq u_U$

Simultaneous Collocation-Based Approach

↓

$$\min \sum_{m=0}^{M-1} \left\{ \sum_{k=0}^{K_m-1} \varphi_m^k(z_m^k, y_m^k, u_m^k, \pi_m, \Pi) \right\}$$

s.t.

$z_{m+1}^k = z_m^k + A_m y_m^k$

$0 = h_{m,k}(z_m^k, y_m^k, u_m^k, \pi_m, \Pi)$

$z_{m+1}^0 = \bar{f}_m(z_m^k, y_m^k, u_m^k, \pi_m)$

$z_m^0 = \tilde{z}(\ell) = p$

$m = 0, \dots, M-1 \quad k = 0, \dots, K_m-1$

27,135 constraints, 9630 LB & UB

Off-line Solution with IPOPT

Algorithmic Step	CPU(s)
Full Solution (10 iterations)	351.5
Single Factorization of KKT Matrix	33.9
Step Computation (single backsolve)	0.94
Rest of Steps	0.12

→ **Feedback Every 6 min**

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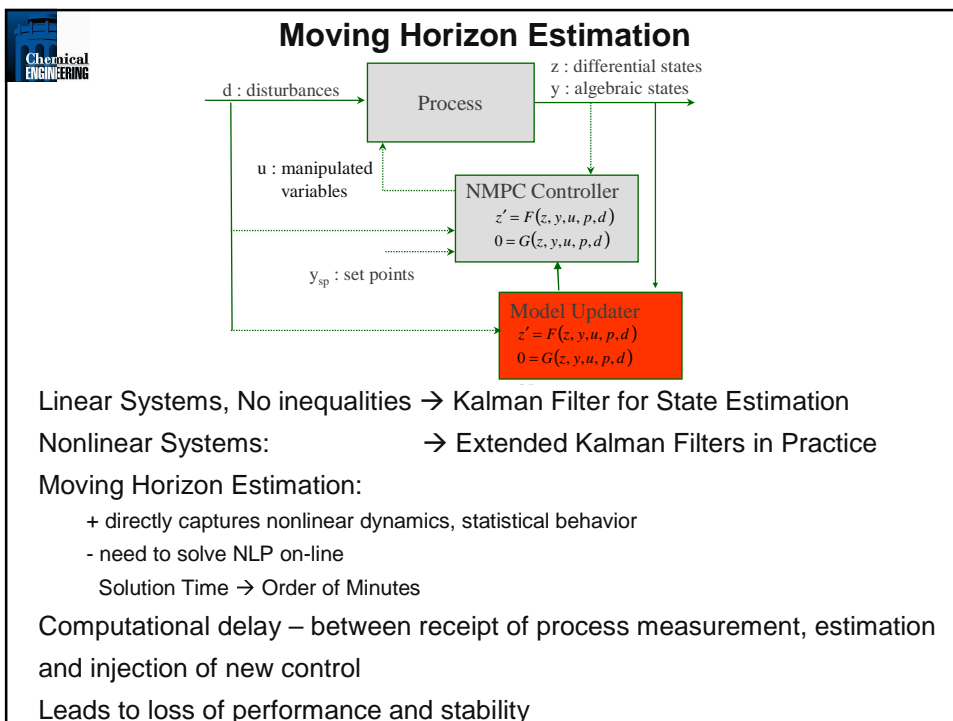
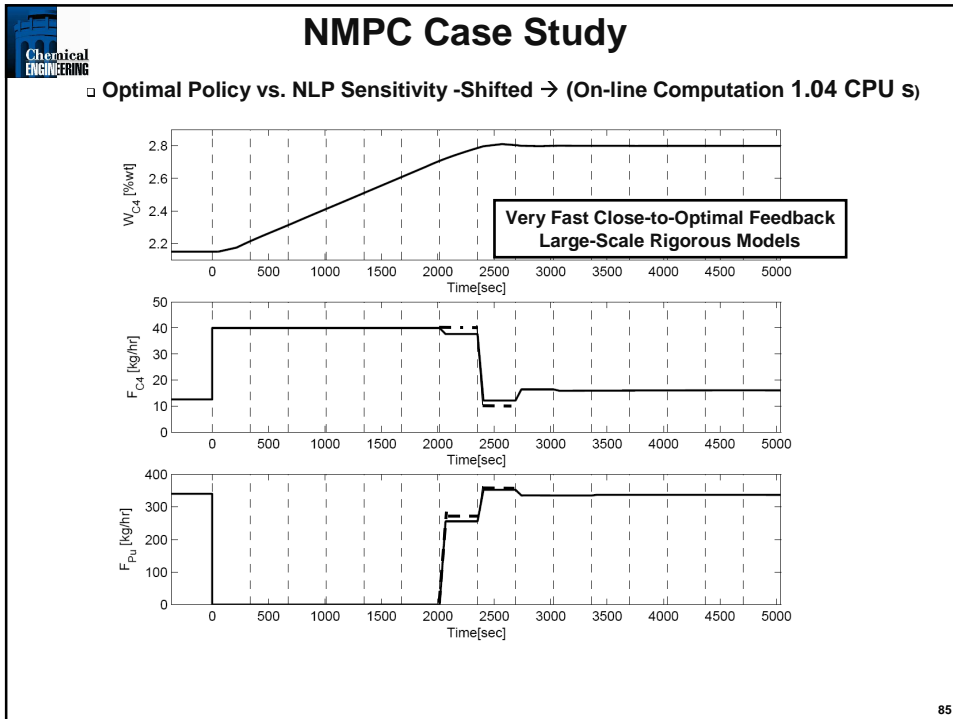
Chemical Engineering

NMPC Case Study

□ **Optimal Feedback Policy → (On-line Computation 351 CPU s)**

Ideal NMPC controller - computational delay not considered
Time delays as disturbances in NMPC

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Chemical Engineering

Moving Horizon Estimation

Linear Systems, No inequalities → Kalman Filter for State Estimation
 Nonlinear Systems: → Extended Kalman Filters in Practice
 Moving Horizon Estimation:
 + directly captures nonlinear dynamics, statistical behavior
 - need to solve NLP on-line
 Solution Time → Order of Minutes
 Computational delay – between receipt of process measurement, estimation and injection of new control
 Leads to loss of performance and stability

Chemical Engineering

Moving Horizon Estimation

$\min_{x_0, w_k} (x_0 - \bar{x}_0^\ell)^T \Pi_0^{-1} (x_0 - \bar{x}_0^\ell) + \sum_{k=0}^N L_k(v_k, w_k)$
 s.t.
 $x_{k+1} = f_k(x_k, w_k)$
 $\bar{y}_{k+\ell-N} = h_k(x_k) + v_k$

P(ℓ)

P($\ell + 1$) $\left\{ \begin{array}{l} \min_{x_0, w_k} (x_0 - \bar{x}_0^{\ell+1})^T \Pi_0^{-1} (x_0 - \bar{x}_0^{\ell+1}) + \sum_{k=0}^N L_k(v_k, w_k) \\ \text{s.t.} \\ x_{k+1} = f_k(x_k, w_k) \\ \bar{y}_{k+\ell-N+1} = h_k(x_k) + v_k \end{array} \right.$

Computational Delay - MHE Impractical
NLPs are Parametric
Solve P(ℓ) in Background
Fast Approximation to P($\ell + 1$) On-line

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Fast Moving Horizon Estimation

Chemical
Engineering

Dummy
Measurement

$P(\ell)$ t_0 t_1 t_2 t_{N-1} t_ℓ t_{l+1}

1) Solve **Extended Problem** Between t_ℓ and t_{l+1}

$$\min_{x_0, w_k, y_{l+1}} (x_0 - \bar{x}_0^f)^T \Pi_0^{-1} (x_0 - \bar{x}_0^f) + \sum_{k=0}^N L_k(v_k, w_k) + L_{N+1}(v_{N+1}, w_{N+1})$$

s.t.

$$\begin{aligned} x_{k+1} &= f_k(x_k, w_k), & k &= 0, \dots, N-1 \\ \bar{y}_{k+l-N} &= h_k(x_k) + v_k, & k &= 0, \dots, N \\ x_{N+1} &= f_N(x_N, w_N) \\ y_{l+1} &= h_{N+1}(x_{N+1}) + v_{N+1} \end{aligned}$$

$\bar{P}(\ell)$

Re-use KKT Matrix Available At Solution of $\bar{P}(\ell)$ Analyze Terms due to Extended Horizon

$$\begin{bmatrix} W(x_k, \lambda_k) & A(x_k) & -I \\ A(x_k)^T & 0 & 0 \\ V_k & 0 & X_k \end{bmatrix} \begin{bmatrix} \Delta x \\ \Delta \lambda \\ \Delta v \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

$$\begin{aligned} \Delta \bar{\lambda}_{N+1} &= 0 \\ R_{N+1}^{-1} \Delta v_{N+1} + \Delta \bar{\lambda}_{N+1} &= 0 \\ \Delta y_{l+1} - \nabla_x h_{N+1} \Delta x_{N+1} - \Delta v_{N+1} &= 0 \end{aligned}$$

$y_{l+1}^* = h_{N+1}(x_{N+1}^*)$ **Dummy Measurement = Model Prediction at t_{l+1}**

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Fast Moving Horizon Estimation

Chemical
Engineering

Plant-Model Mismatch

$P(\ell)$ t_0 t_1 t_2 t_{N-1} t_ℓ t_{l+1}

2) At t_{l+1} once we know \bar{y}_{l+1}

$$\Delta \bar{\lambda}_{N+1} = 0$$

$$R_{N+1}^{-1} \Delta v_{N+1} + \Delta \bar{\lambda}_{N+1} = 0$$

$$\Delta y_{l+1} - \nabla_x h_{N+1} \Delta x_{N+1} - \Delta v_{N+1} = 0$$

KKT System At Solution of $\bar{P}(\ell)$

$$\begin{bmatrix} W(x_k, \lambda_k) & A(x_k) & -I \\ A(x_k)^T & 0 & 0 \\ V_k & 0 & X_k \end{bmatrix} \begin{bmatrix} \Delta x \\ \Delta \lambda \\ \Delta v \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

$$\mathbf{K} \Delta s = 0$$

Find perturbation Δp that enforces

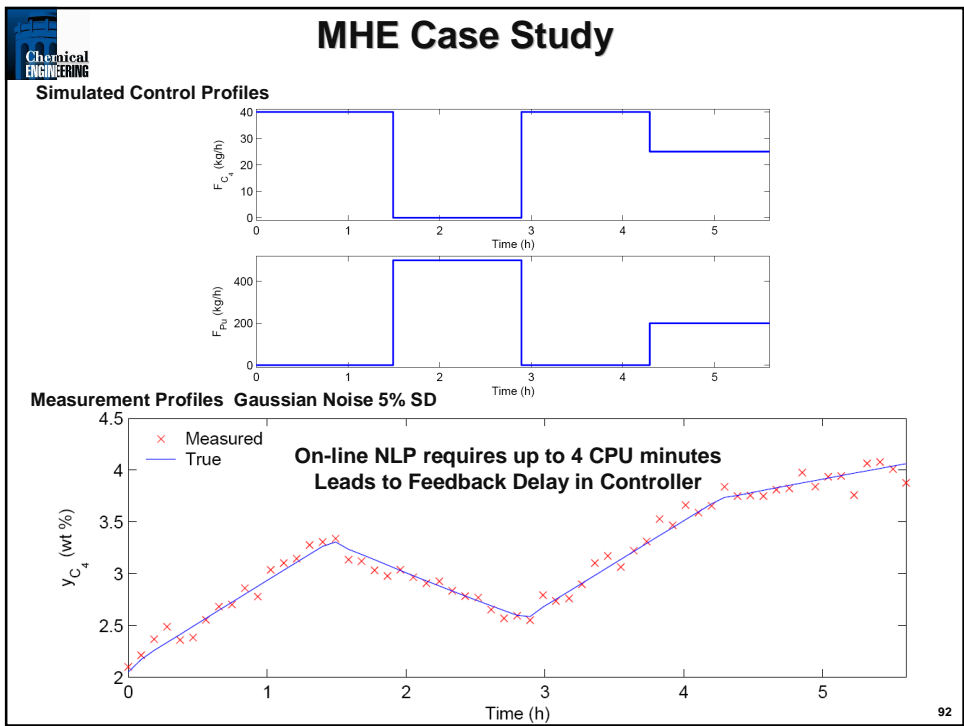
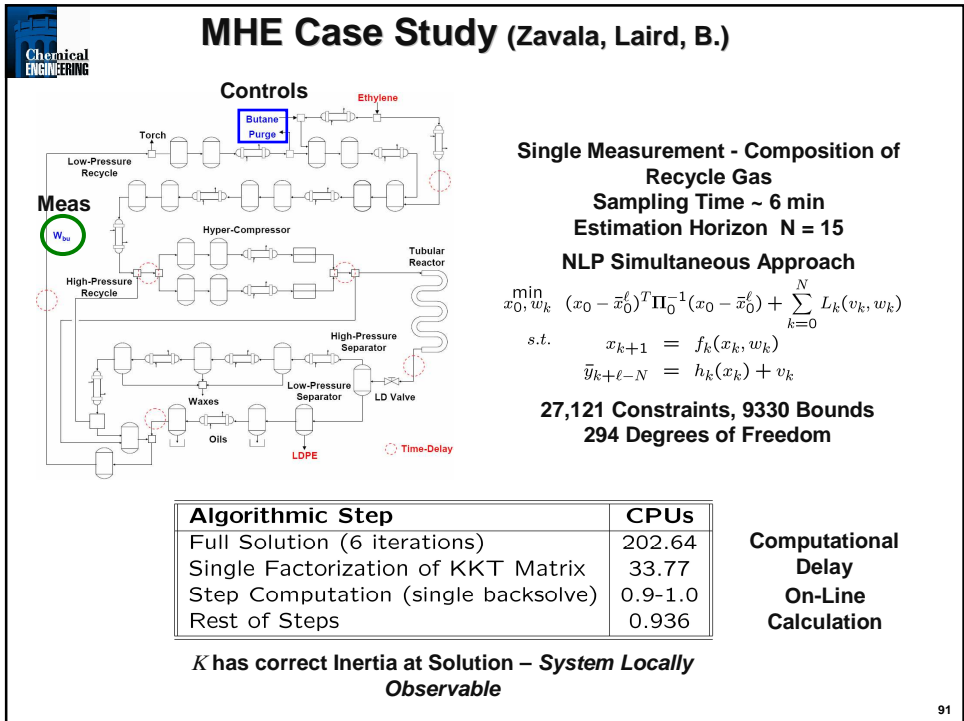
$$y_{l+1} = \bar{y}_{l+1}$$

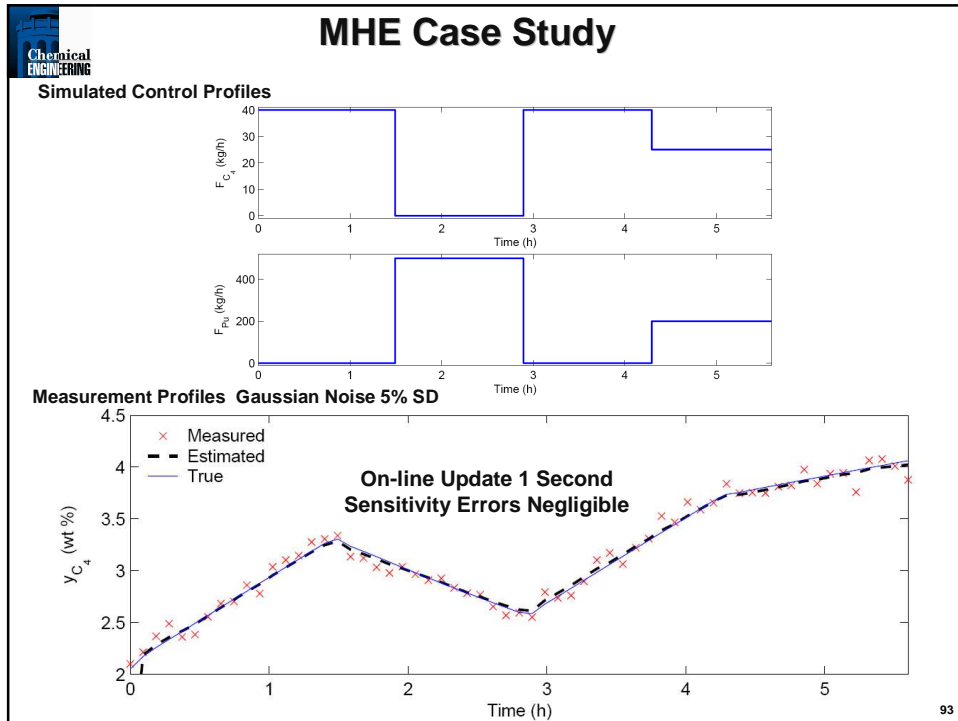
K is already factorized
Solve as Schur complement problem
On-line Cost is a simple backsolve

Augmented KKT System

$$\begin{bmatrix} \mathbf{K} & \mathbf{E}_p \\ \mathbf{E}_y^T & 0 \end{bmatrix} \begin{bmatrix} \Delta s \\ \Delta p \end{bmatrix} = - \begin{bmatrix} 0 \\ \bar{y}_{l+1} - y_{l+1}^* \end{bmatrix}$$

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Summary: Dynamic Optimization

Sequential Approaches – Use DAE Integrators

- Parameter Optimization
 - Gradients by: Direct (and Adjoint) Sensitivity Equations
- Optimal Control (Profile Optimization)
 - Variational Methods
 - NLP-Based Methods - Single and Multiple Shooting
- Require Repeated Solution of Model
- State Constraints are Difficult to Handle

Simultaneous Collocation Approach

- Discretize ODE's using orthogonal collocation on finite elements
- Straightforward addition of state constraints.
- Deals with unstable systems
- Solve model only once
- Avoid difficulties at intermediate points

Large-Scale Extensions

- Exploit structure of DAE discretization through decomposition
- Large problems solved efficiently with IPOPT

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Summary: On-line Extensions

RTO and MPC widely used for refineries, ethylene and, more recently, chemical plants

- Inconsistency in models → operating problems?

Off-line dynamic optimization is widely used

- Polymer processes (especially grade transitions)
- Batch processes
- Periodic processes

NMPC provides link for off-line and on-line optimization

- Stability and robustness properties
- Advanced step controller leads to very fast calculations
 - Analogous stability and robustness properties
 - On-line cost is negligible

Multi-stage planning and on-line switches

- Avoids conservative performance
- Update model with MHE
- Evolve from regulatory NMPC to Large-scale DRTO

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<http://dynopt.cheme.cmu.edu>

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