

# AUTOMOTIVE CO<sub>2</sub> MITIGATION USING AN ONBOARD BOSCH REACTOR: ANALYSIS

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# OBJECTIVE

- Determine the technical and economic requirements of an automotive CO<sub>2</sub> reduction system
  - Determine preferred carbon product and method of expulsion from vehicle
  - Determine cost contributors
- Conduct a techno-economic and lifecycle analysis of implementing an automotive Bosch reactor
  - Determine the optimal operating conditions
  - Determine the optimal design

# AUTOMOTIVE CO<sub>2</sub> REDUCTION

- Preferred carbon product
  - Non-corrosive
  - Cheap to dispose
  - Non-gaseous
- Cost Goals
  - Minimize the amount of hydrogen required to store onboard
  - Determine feasibility of regenerative and non-regenerative catalysts
  - Need to mitigate carbon “coking” on catalyst surface

# BOSCH REACTION

- Composed of 4 different reactions

Reaction	Formula	$\Delta H$
Reverse Water Gas Shift	$\text{CO}_2 + \text{H}_2 \rightarrow \text{CO} + \text{H}_2\text{O}$	41 kJ/mol
Hydrogenation	$\text{CO} + \text{H}_2 \rightarrow \text{C(s)} + \text{H}_2\text{O}$	-131 kJ/mol
Boudouard	$2\text{CO} \rightarrow \text{C(s)} + \text{CO}_2$	-172 kJ/mol
Sabatier	$\text{CO}_2 + 4\text{H}_2 \rightarrow \text{CH}_4 + 2\text{H}_2\text{O}$	-165.4 kJ/mol

# REACTION RATES (EQUILIBRIUM CONSTANTS)

- Developed by solving each species' transport equation simultaneously with its energy balance
- Temperature dependent equilibrium constants developed by comparing fugacity ratios to differences in Gibb's free energies at actual and reference conditions (chemical activity)

$$K_i = \exp \left[ \frac{\lambda_1}{T^2} + \frac{\lambda_2}{T} + \lambda_3 \right]$$

Description	Reaction	Equation	$\lambda_1$	$\lambda_2$	$\lambda_3$
1. CO <sub>2</sub> Methanation	CO <sub>2</sub> + 4H <sub>2</sub> ⇌ CH <sub>4</sub> + 2H <sub>2</sub> O	Eq. 1	-730,726.0	24,125.3	-26.9616
2. CO Methanation	CO + 3H <sub>2</sub> ⇌ CH <sub>4</sub> + H <sub>2</sub> O	Eq. 2	-538,798.1	28,062.7	-30.7759
3. Reverse WGS	CO <sub>2</sub> + H <sub>2</sub> ⇌ CO + H <sub>2</sub> O	Eq. 4	-191,928.1	-3,937.4	3.8143
4. Hydrogenation	CO + H <sub>2</sub> ⇌ C(s) + H <sub>2</sub> O	Eq. 5	-121,003.4	16,573.0	-17.3858
5. Boudouard	2CO ⇌ C(s) + CO <sub>2</sub>	Eq. 6	70,924.7	20,510.4	-21.2000

# REACTION RATES (GAS PHASE EQUILIBRIA)

- Methanation
- RWGS
- Hydrogenation
- Boudouard

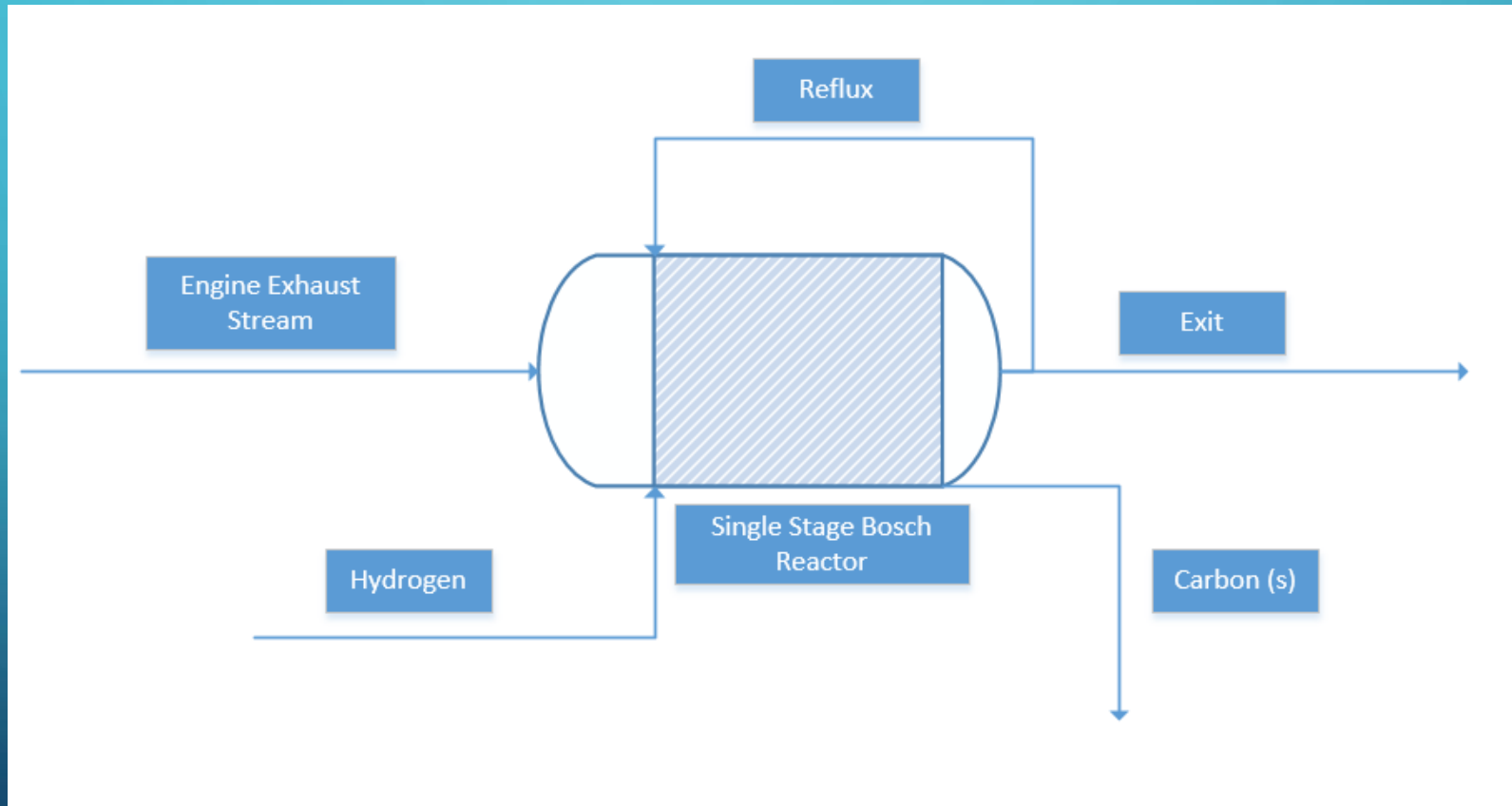
$$r_1 = \frac{k_1 K_{CO_2,1} K_{H_2,1}^4 z_{CO_2} z_{H_2}^4 P^5}{(1 + K_{CO_2,1} P z_{CO_2} + K_{H_2,1} P z_{H_2})^5} (1 - \eta)$$

$$r_3 = k_3 \rho P (z_{CO_2} z_{H_2} K_3 - z_{CO} z_{H_2O})$$

$$r_4 = k_4 \rho (z_{CO} z_{H_2} K_4 P - z_{H_2O})$$

$$r_5 = \frac{\rho_{cat} \epsilon_o k_B^+ K_{CO,5} \left( P z_{CO} - \frac{1}{K_B^*} \frac{z_{CO_2}}{z_{CO}} \right)}{\left( 1 + K_{CO,5} P z_{CO} + \frac{1}{K_{O,CO_2} K_{CO,5}} \frac{z_{CO_2}}{z_{CO}} \right)^2}$$

# PROPOSED REACTOR DESIGN





# CATALYST COKING

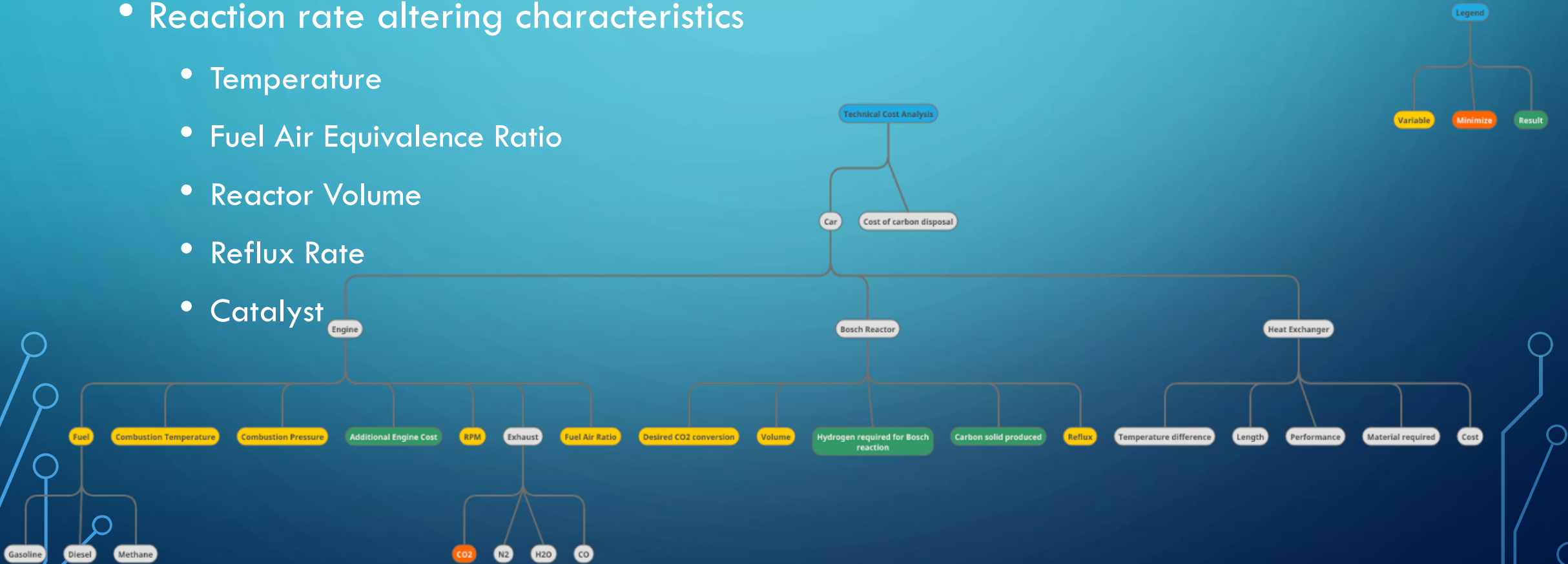
- Assume nickel catalyst is completely regenerative
  - Needs mechanical or magnetic agitation
- For  $\sim 105\text{kg CO}_2$  in 1 tank of fuel
  - 1.38 kg steel wool required (packing density =  $0.2\text{g/cm}^3$ )
    - Volume steel wool required to avoid coking disadvantage =  $0.0069\text{m}^3$





# PROCESS CONSIDERATIONS

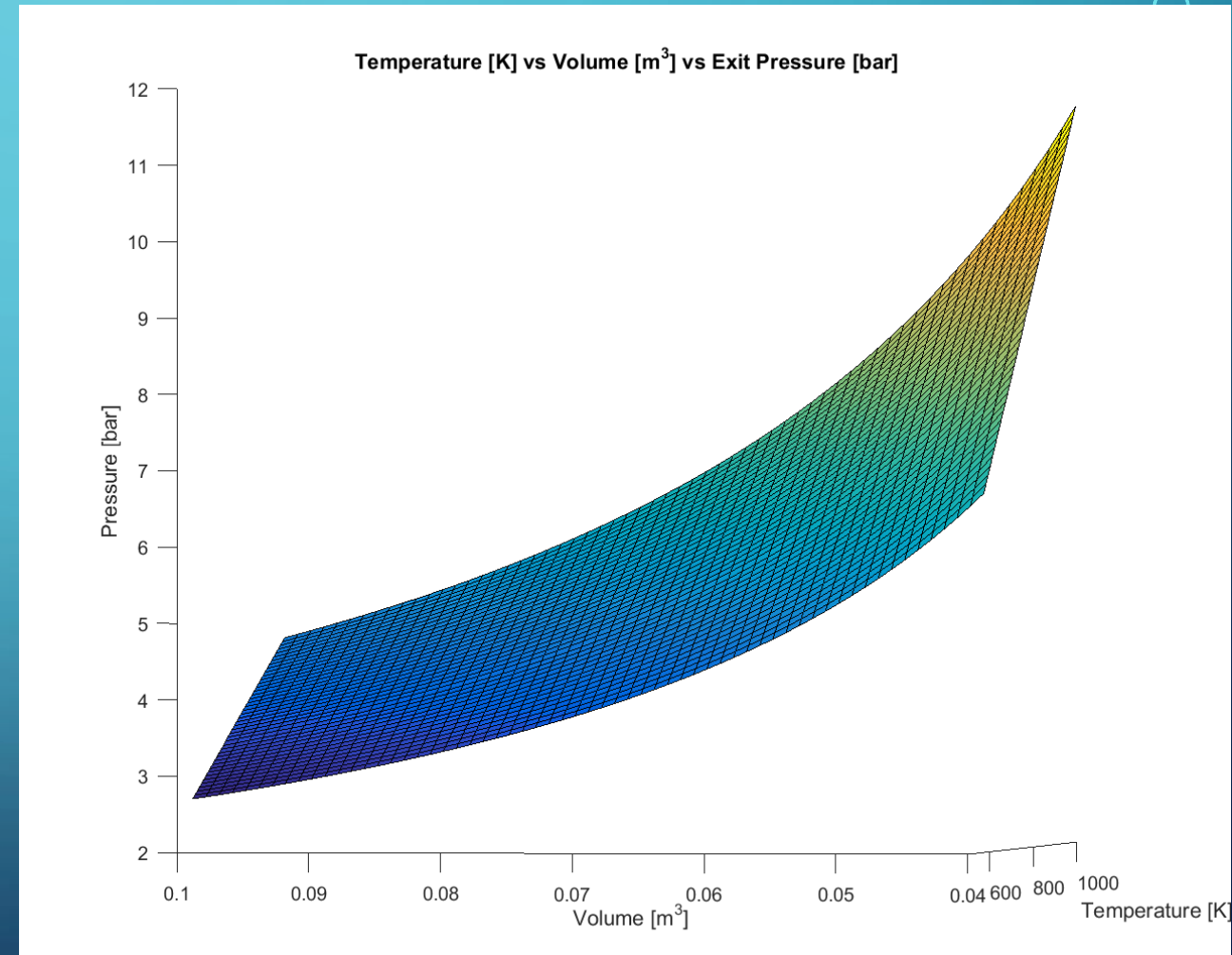
- Reaction rate altering characteristics
  - Temperature
  - Fuel Air Equivalence Ratio
  - Reactor Volume
  - Reflux Rate
  - Catalyst





# EFFECT OF REACTOR VOLUME

- Higher Volume  $\rightarrow$  Lower Conversion
  - Lower pressure (diffuse)
  - Lower reaction rate
- Lower Volume  $\rightarrow$  Higher Conversion
  - Higher pressure
  - Higher activity
  - Higher reaction rate
  - Need to minimize exit pressure



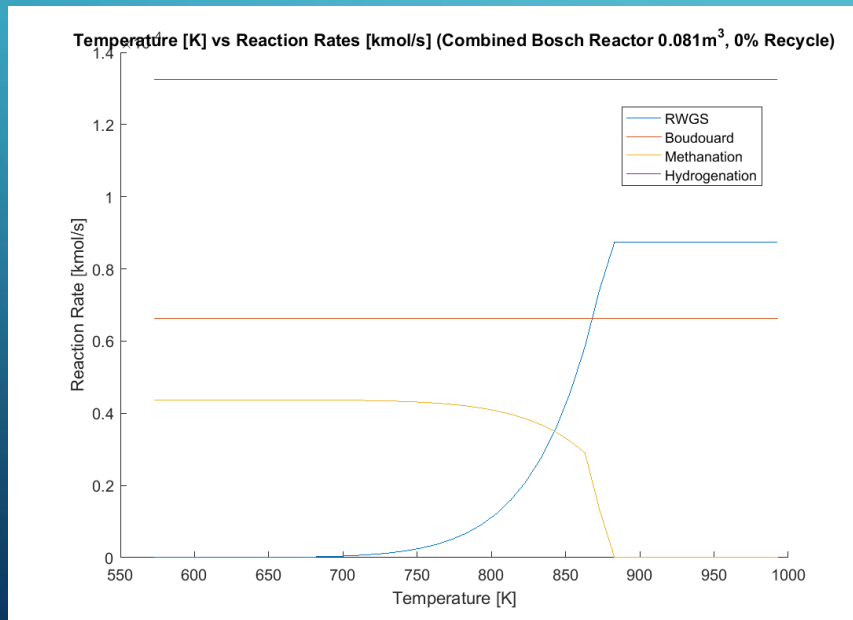
# EFFECT OF TEMPERATURE (RATES)

- Directly affects reaction rate constant

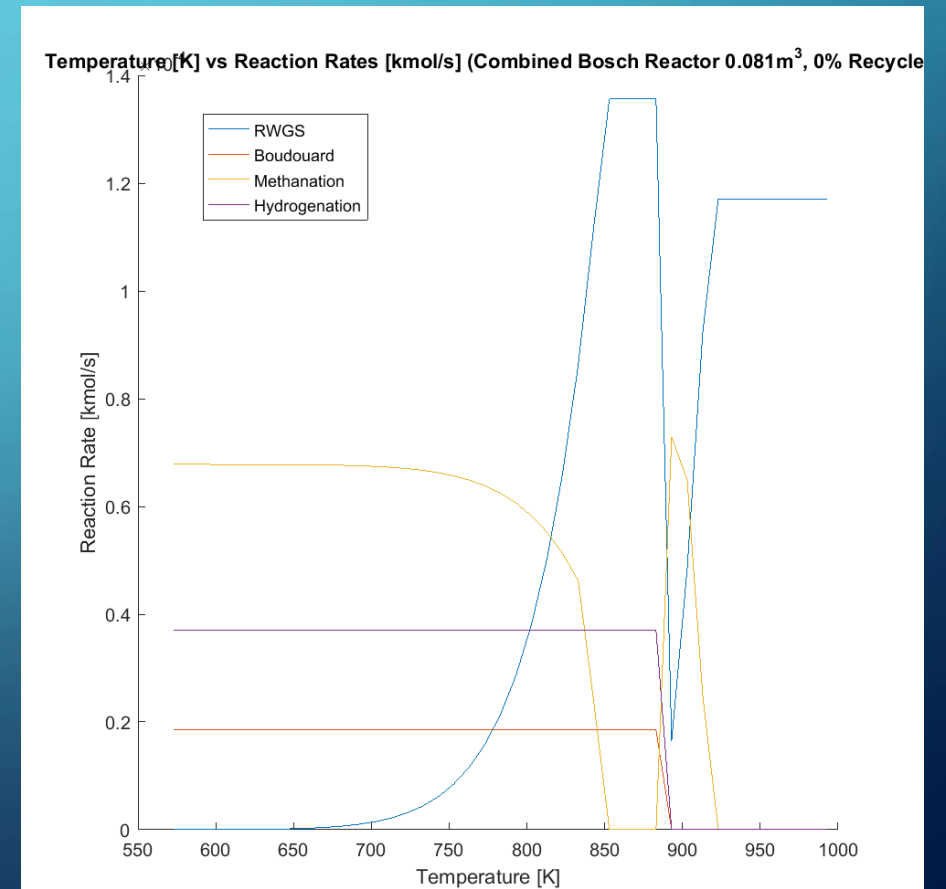
- Higher T  $\rightarrow$  RWGS

- Lower T  $\rightarrow$  Methanation

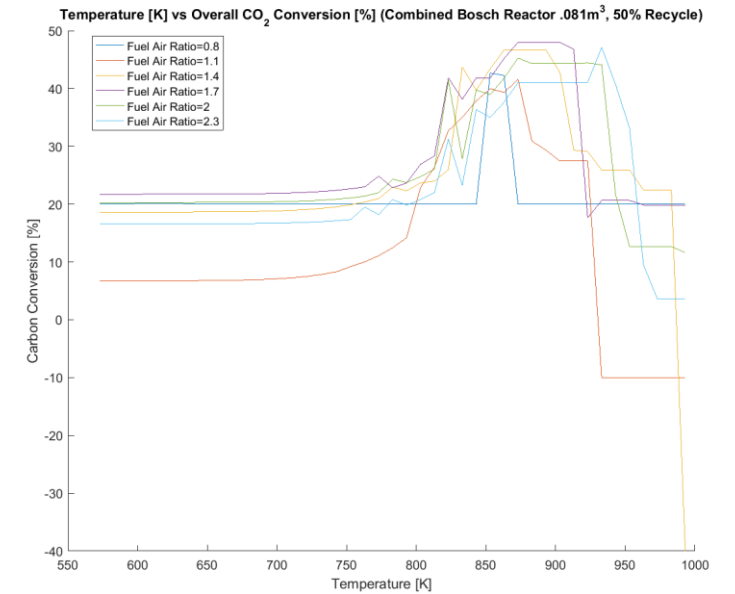
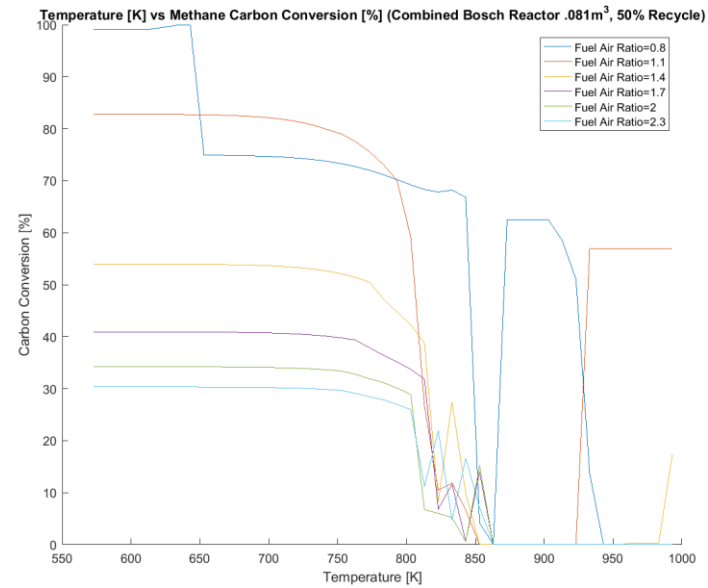
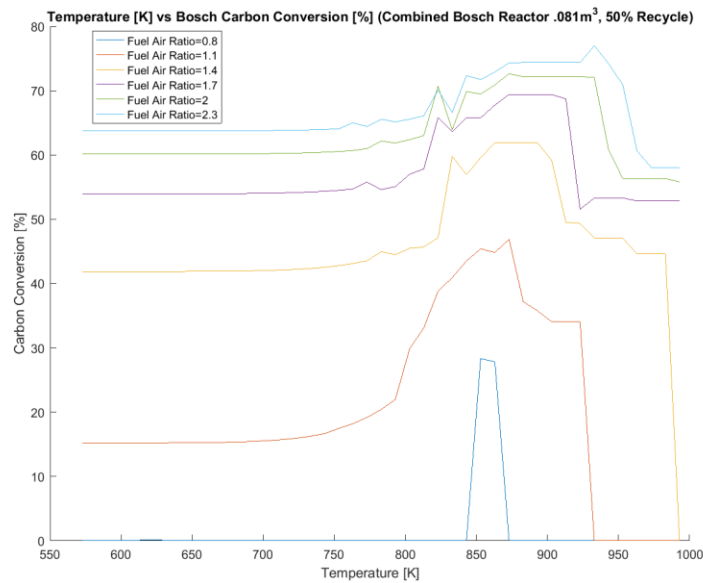
Fuel Air Ratio= 2.3



Fuel Air Ratio= 1.2

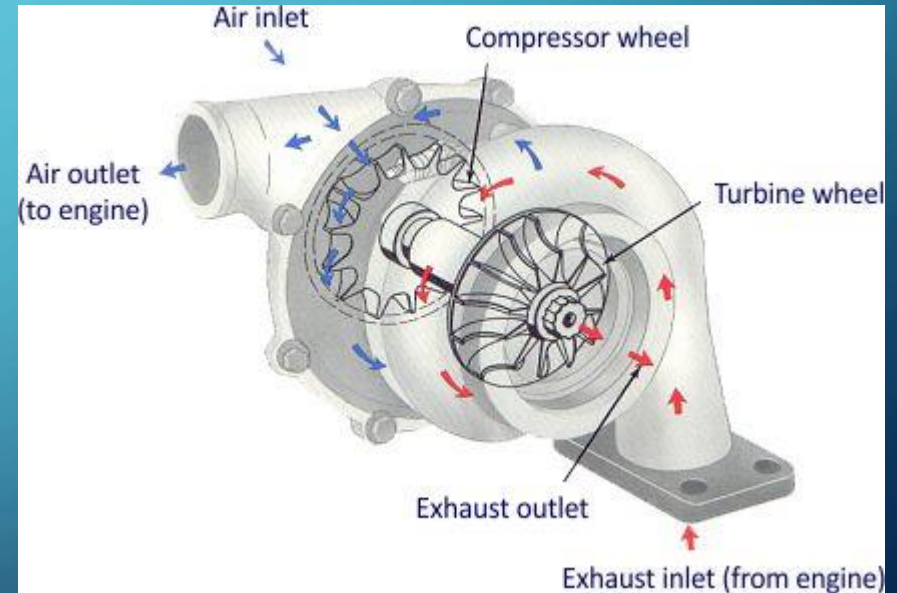


# EFFECT OF TEMPERATURE (CONVERSION)



# WHY INCREASE FUEL AIR RATIO?

- Produce more CO and H<sub>2</sub> in combustion equilibrium
- Bypass RWGS reduction (endothermic)
- Increased power generation
  - Higher fuel content
  - Improved turbo-diesel operation
- One less methanation stage
- Can mitigate higher fuel use by decreasing engine size
  - Lower Volumetric Flow Rate

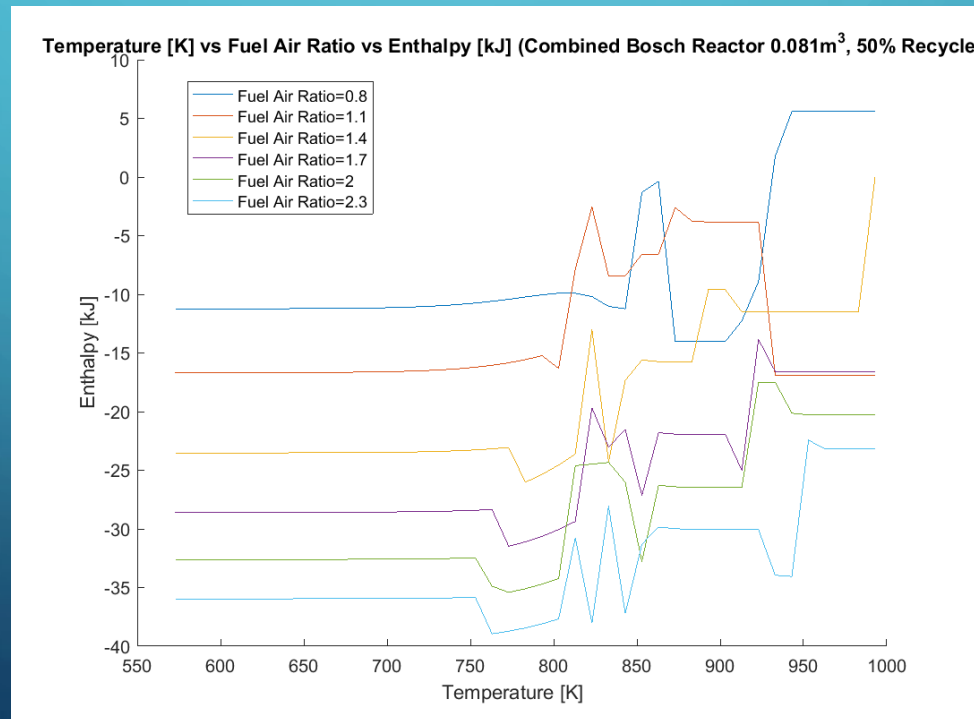


<https://www.dieselnets.com/tech/images/air/turbo/~turbocharger.jpg>



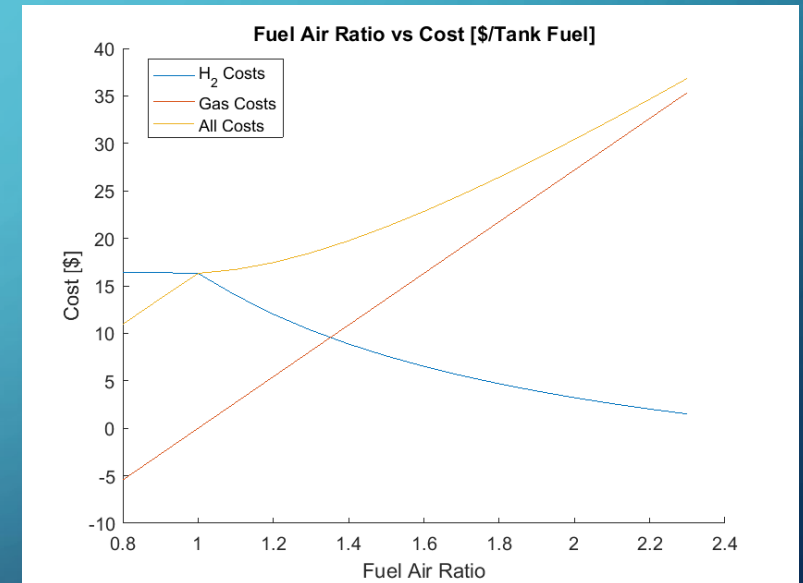
# ENERGY & CARBON BALANCE

- Carbon expelled per tank  $\approx 74\% * 30.1 \text{ kg C / tank} = 22.7 \text{ kg carbon / tank}$



# COST FACTORS

Cost Factor	Cost
H <sub>2</sub> Tanks	\$250/tank
Reactor Cost	\$1600 or \$50/tank
H <sub>2</sub> Cost / kg	\$1.80/kg
Additional Fuel Cost / gal	\$2.27/gal



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