



# A Pressure-drop Method

## for Real-time Monitoring the Solid Flux in Circulating Gas-solid Processes

*Sihong Gao\*, Yiping Fan, Chunxi Lu*

*State Key Laboratory of heavy Oil Processing, College of Chemical Engineering  
China University of Petroleum, Beijing*

## FLUIDIZATION XVI

*\*Reporter*

*E-mail Address: gaosihong@outlook.com*





## *Contents*

- Introduction
- Experimental setup
- Results & Conclusions

## FLUIDIZATION XVI

\*Reporter

E-mail Address: [gaosihong@outlook.com](mailto:gaosihong@outlook.com)





# 1. INTRODUCTION

## FLUIDIZATION XVI

*\*Reporter*

*E-mail Address: gaosihong@outlook.com*

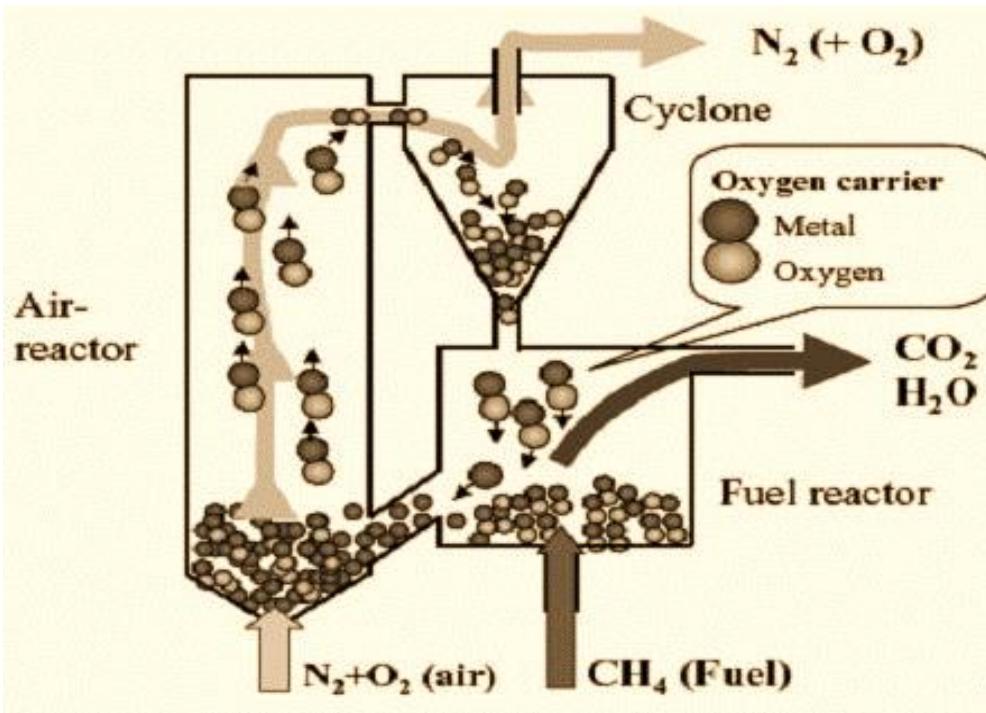




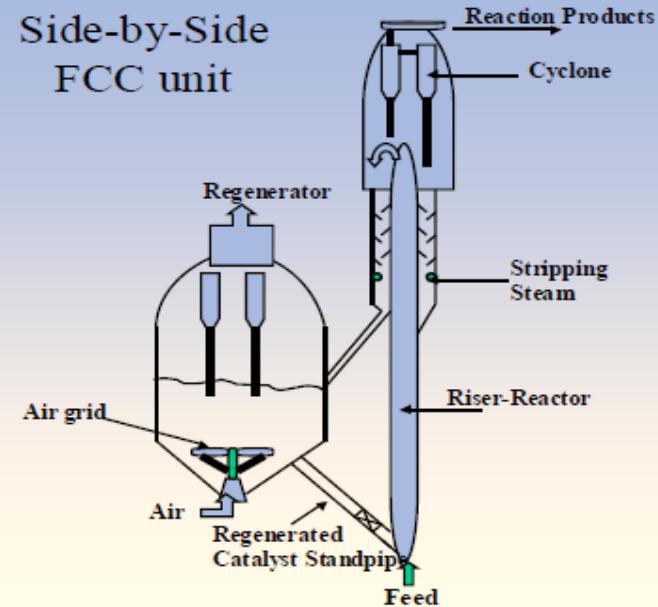
# Background

## ■ Circulating Gas-solid Processes

- **CFB, Circulating Fluidized Bed,** Applications: CLC / FCC / IGCC / PFBC / BG ....
- **CGB, Circulating Granular Bed,** Applications: CR / (M)GBF....



Side-by-Side  
FCC unit



Chemical Looping Combustion

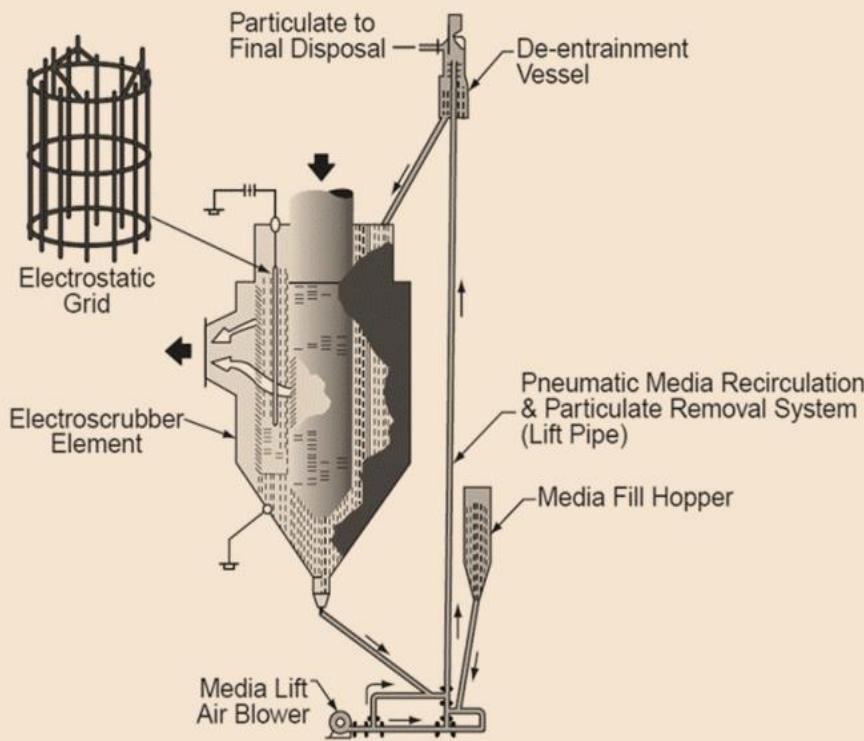
Fluidized Catalytic Cracking



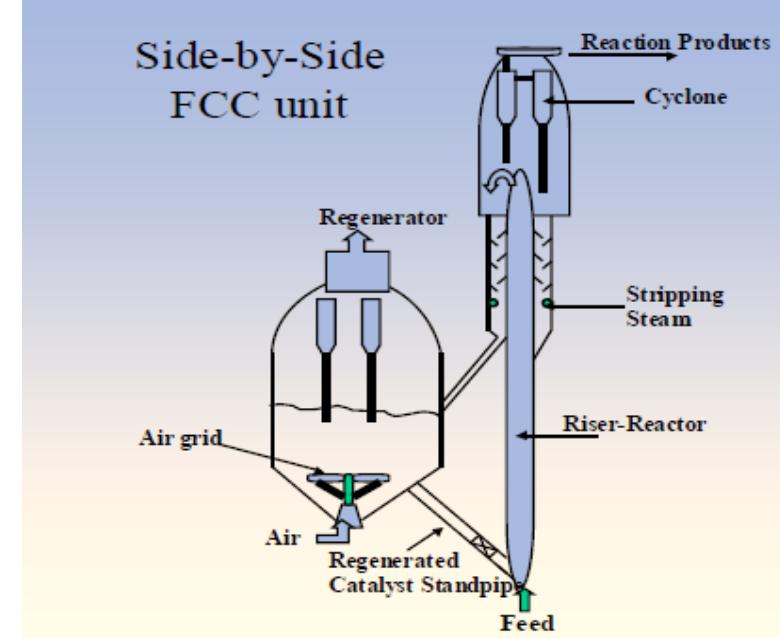
# Background

## ■ Circulating Gas-solid Processes

- **CFB, Circulating Fluidized Bed,** Applications: CLC / FCC / IGCC / PFBC / BG ....
- **CGB, Circulating Granular Bed,** Applications: CR / (M)GBF....



Electrostatic Granular Bed Filter



Fluidized Catalytic Cracking



# Background

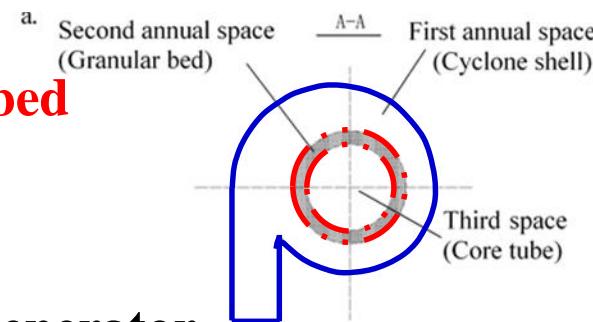
## ■ Solid Circulating Flux -- VITAL PARAMETER

- **Visual Observation** – original and basic
- **Solid Accumulation (volume method)** –original and basic
- **Fiber Optical Probe (particle velocity)** – low accuracy with many assumptions
- **X-Ray Densitometry** – high cost and additional estimation
- **Electrical capacitance tomography** – high cost and additional estimation
- **Extraction/Sampling Probe (solid velocity distribution)** – intrusive
- **Heat/Mass Transfer or Oxygen Balance** – limit and outline
- **Tracer Method (magnetic/radioactive)** – intrusive and high cost
- **Mechanical Meters (Impact /Spiral flow)** – online, sensitive but calibration and stability needed
- **Pressure Drop Method** – online, accurate, scalability, simple implementation.



# Background

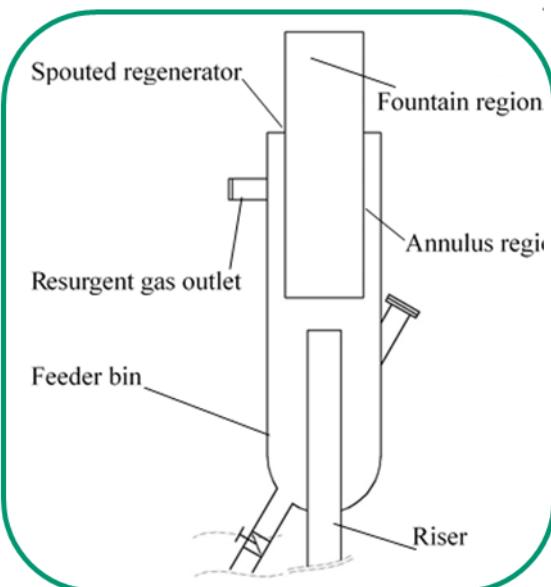
- **Cyclone & Granular bed**



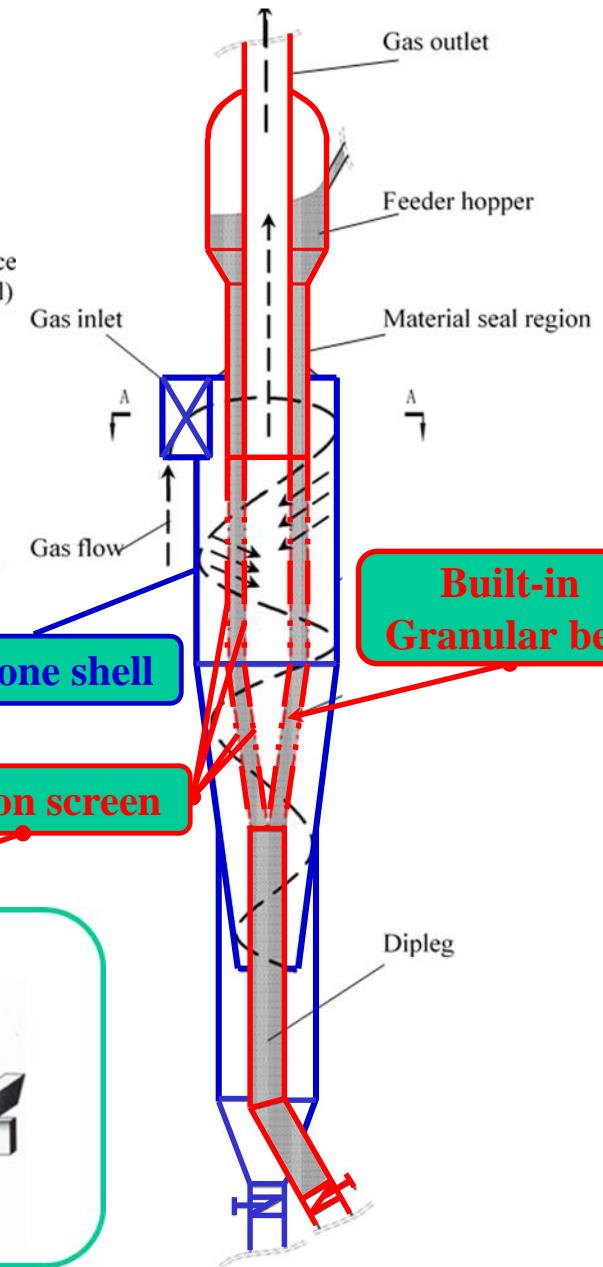
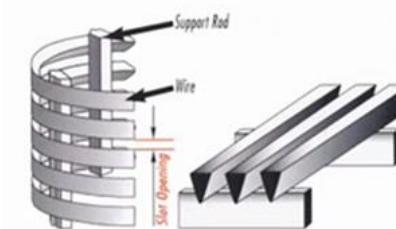
- **Johnson screen**

**Cyclone shell**

**Built-in  
Granular bed**



**Structure of Johnson screen**



**Detailed structure of the C-CGBF system**



2.

## EXPERIMENTAL SETUP

### FLUIDIZATION XVI

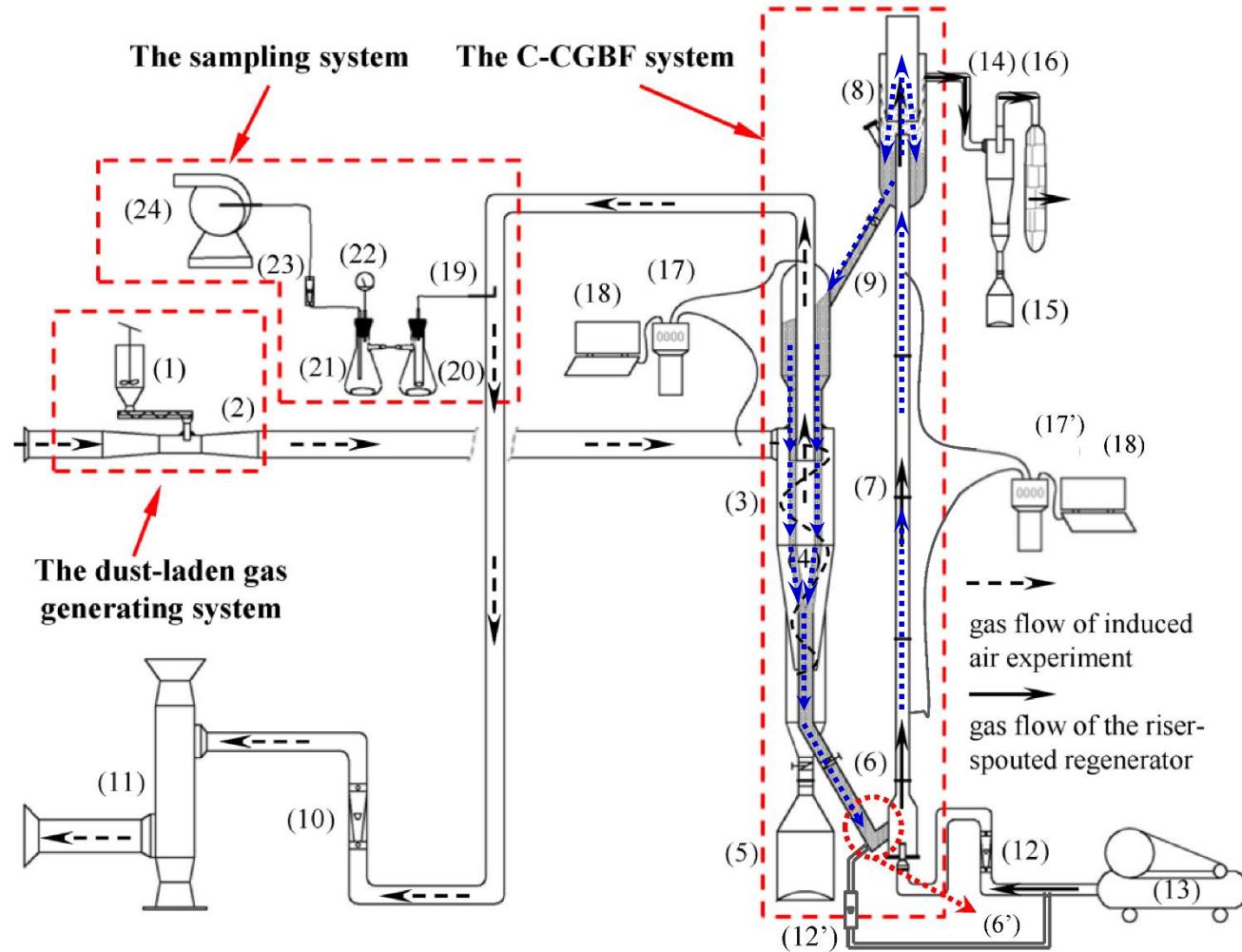
*\*Reporter*

*E-mail Address: gaosihong@outlook.com*





# Setup



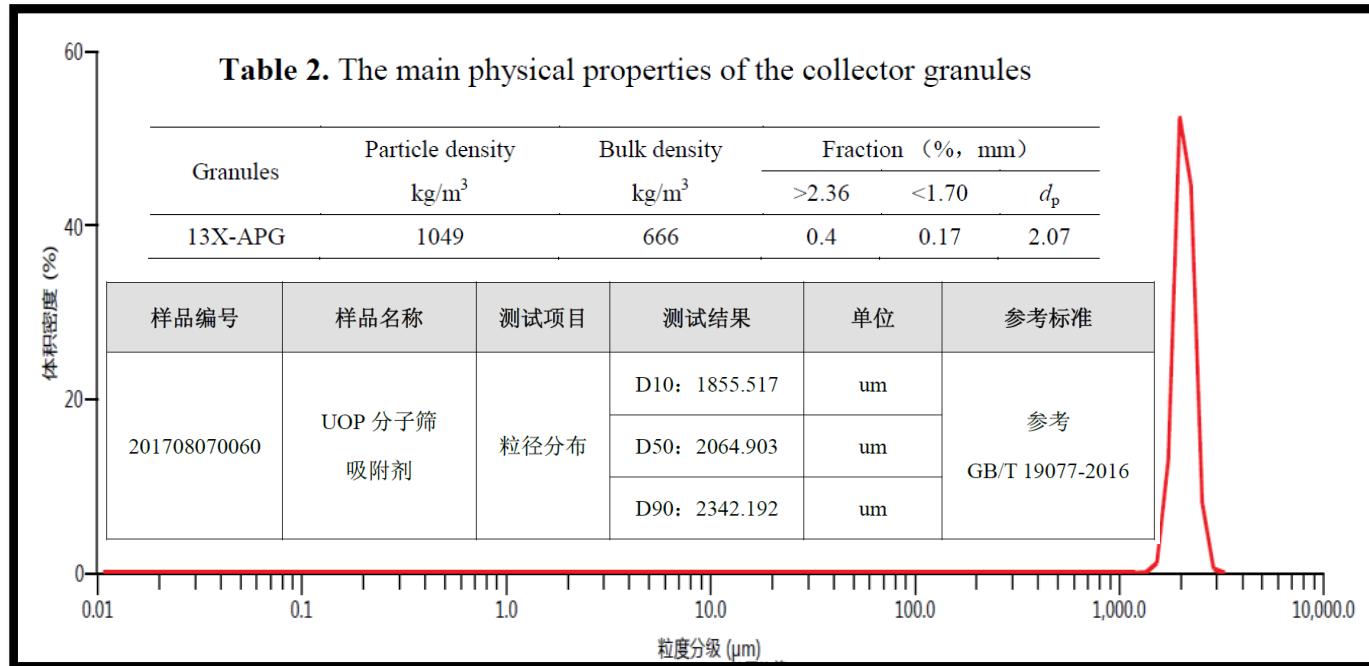
Schematic diagram of the experimental setup



# Materials

## ● Collector Granules:

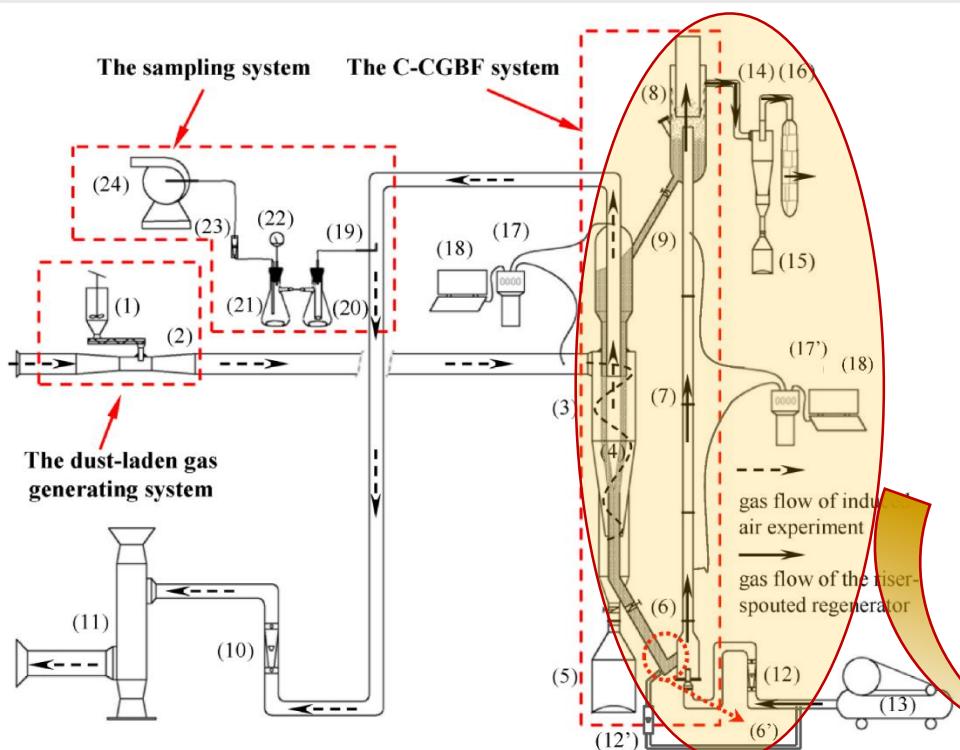
- UOP 13X-APG adsorbent granules,  $d_p = 2.07 \text{ mm}$ ;  $\rho_b = 666 \text{ kg/m}^3$ .



Size distribution of the UOP 13X-APG adsorbent granules (Mastersizer3000)



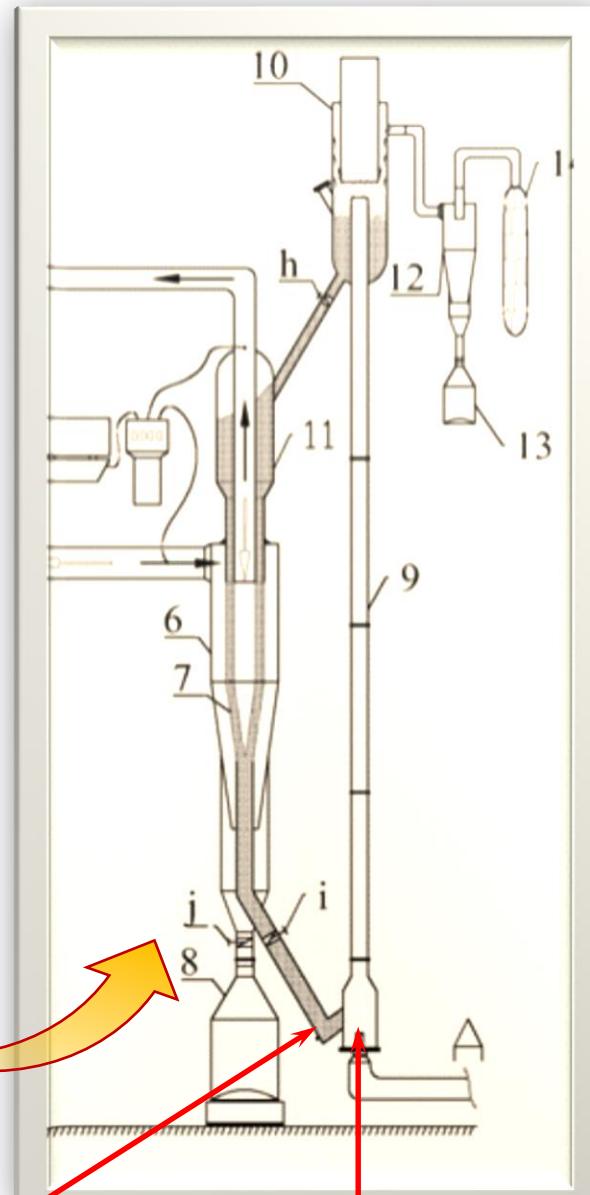
# Measurement



$$Q_r = Q_t + Q_l$$

Transporting Air,  $Q_t$

Main Lifting Air,  $Q_l$





# Analysis

## ■ Accumulation Method: $W_s = \rho_b V / t$

- $t$  means the time spent by a given volume  $V$  of the collector granules downward flowing out of the feeder hopper is recorded by a seconds-counter.

## ■ Pressure-drop Method

### ■ Pressure drop of the riser: $\Delta P_r = \bar{\rho}gh + f_g + f_s$

- the average density of the gas-solids flow in the 4 m riser,

$$\bar{\rho} = k W_s / Q_r$$

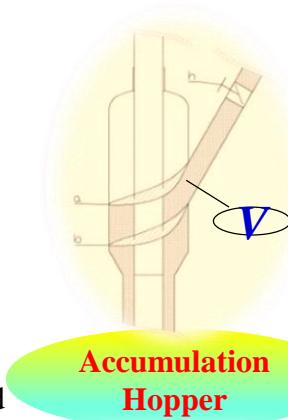
- $f_g$  is the friction loss caused by the pneumatic gas ;
- $f_s$  represents the pressure loss due to the collision between the solids and the riser wall, as well as the collision between the solids themselves.

$$f_s = \xi_s \cdot \bar{\rho} u_t^2 / 2$$

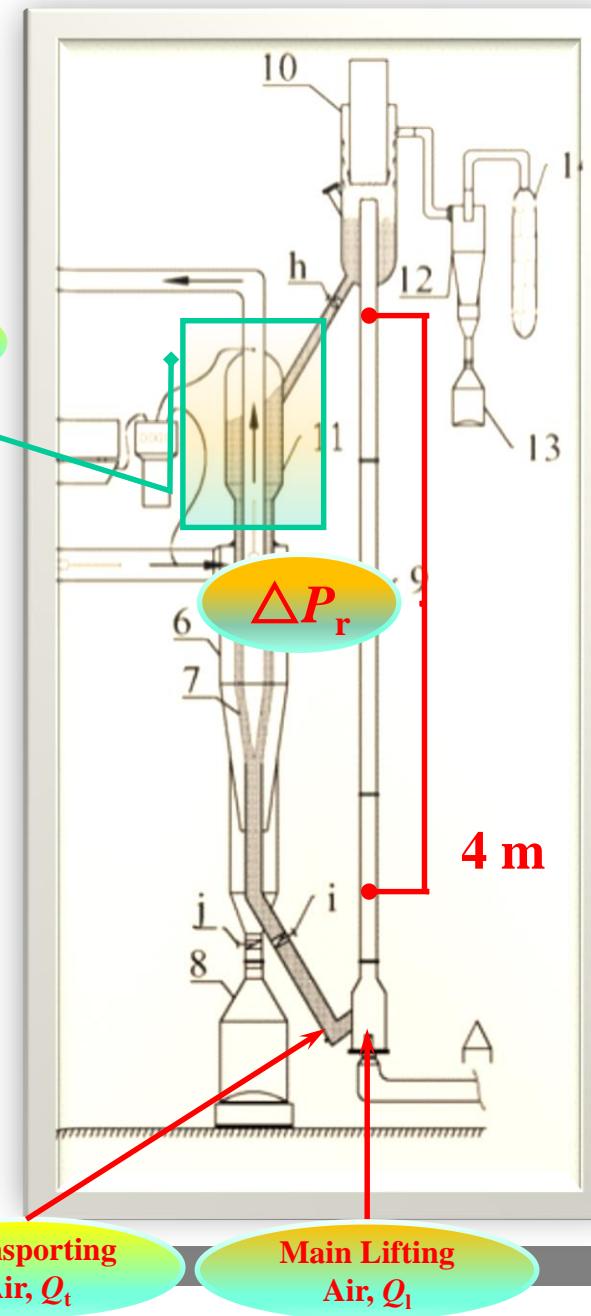
- Therefore :

$$\Delta P_r = W_s k (gh + \xi_s u_t^2) / Q_r + f_g$$

- there is a linear relationship between  $\Delta P_r$  and  $W_s$ , with an intercept of  $f_g$ .



Accumulation  
Hopper





3.

## RESULTS & CONCLUSIONS

### FLUIDIZATION XVI

*\*Reporter*

*E-mail Address: gaosihong@outlook.com*





# Results

## ● Experimental conditions:

$Q_r$ $m^3/h$	$Q_t$ $m^3/h$	$\Delta P_r$ kPa	$W_s$ kg/s
68	0	0.698	0.022
	2	0.817	0.027
	4	0.889	0.034
	6	1.026	0.042
	8	1.161	0.058
	10	1.557	0.086
	12	3.020	0.194
	14	2.879	0.224
	16	2.908	0.242

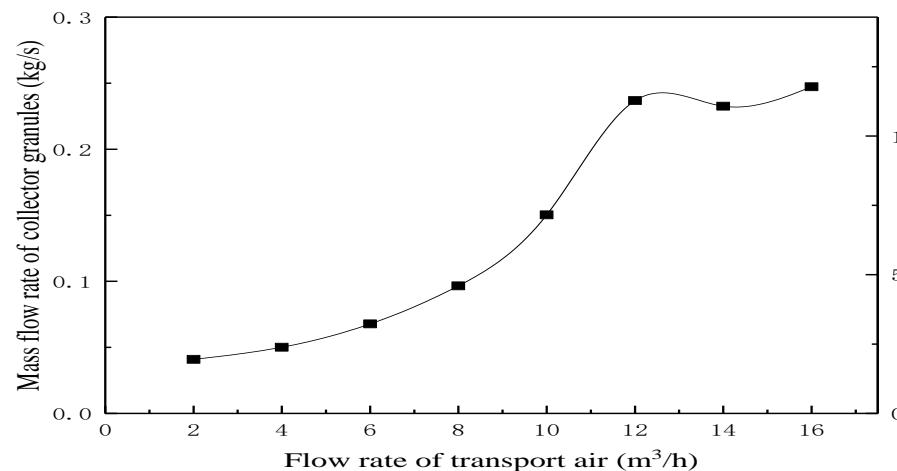
$Q_r$ $m^3/h$	$Q_t$ $m^3/h$	$\Delta P_r$ kPa	$W_s$ kg/s
98	0	0.409	0.029
	2	0.465	0.039
	4	0.547	0.048
	6	0.694	0.062
	8	0.971	0.091
	10	1.452	0.146
	12	2.383	0.274
	14	2.316	0.268
	16	2.297	0.275

$Q_r$ $m^3/h$	$Q_t$ $m^3/h$	$\Delta P_r$ kPa	$W_s$ kg/s
128	0	0.026	0.417
	2	0.040	0.537
	4	0.051	0.585
	6	0.067	0.705
	8	0.091	0.872
	10	0.159	1.368
	12	0.254	2.125
	14	0.262	2.032
	16	0.290	2.320

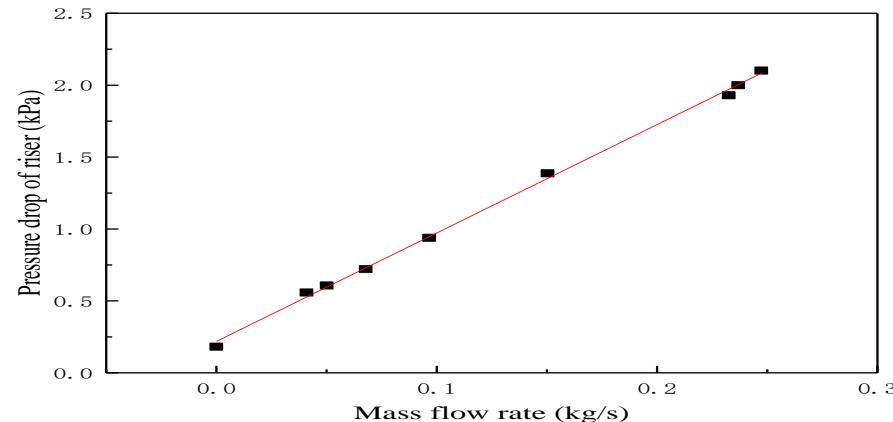
$Q_r$ $m^3/h$	$Q_t$ $m^3/h$	$\Delta P_r$ kPa	$W_s$ kg/s
158	0	0.012	0.496
	2	0.026	0.587
	4	0.046	0.709
	6	0.068	0.875
	8	0.142	1.438
	10	0.173	1.693
	12	0.228	2.263
	14	0.255	2.457
	16	0.291	2.642

$Q_r$ $m^3/h$	$Q_t$ $m^3/h$	$\Delta P_r$ kPa	$W_s$ kg/s
98	0	0.409	0.029
	2	0.465	0.039
	4	0.547	0.048
	6	0.694	0.062
	8	0.971	0.091
	10	1.452	0.146
	12	2.383	0.274
	14	2.316	0.268
	16	2.297	0.275

# Results

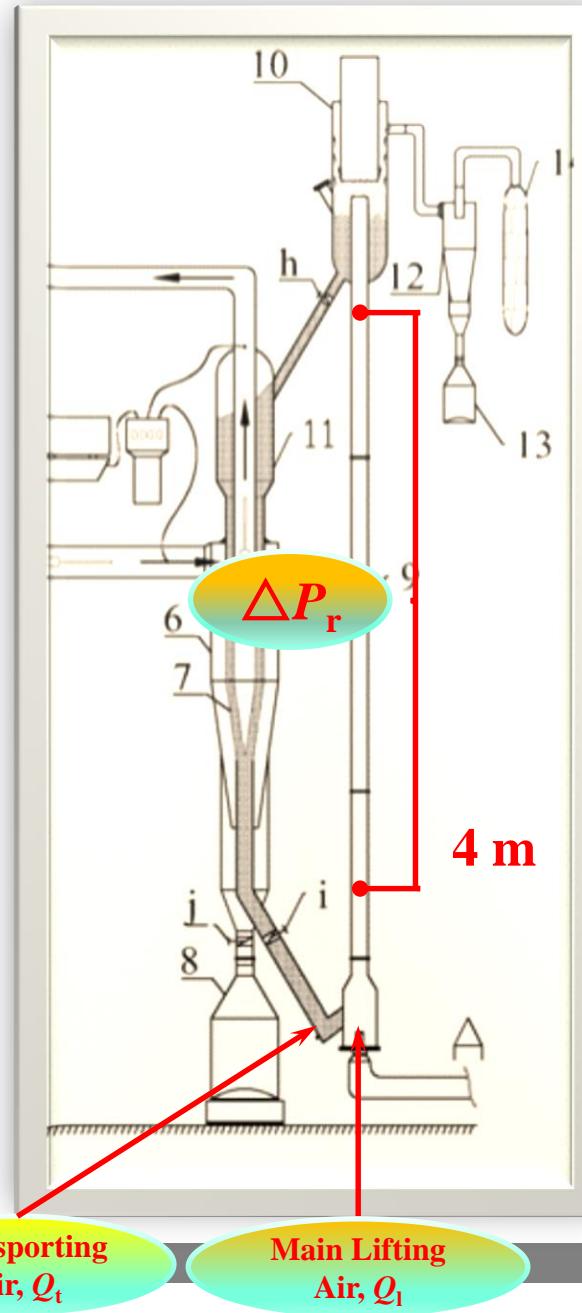


Granules circulation flux at different flow rates of the transporting air in the V valve,  $Q_r=98\text{ m}^3/\text{h}$



Relationship of the pressure drop of the 4 m riser and the granules circulation flux

Collector granules circle intensity ( $kg/m^2\text{s}$ )

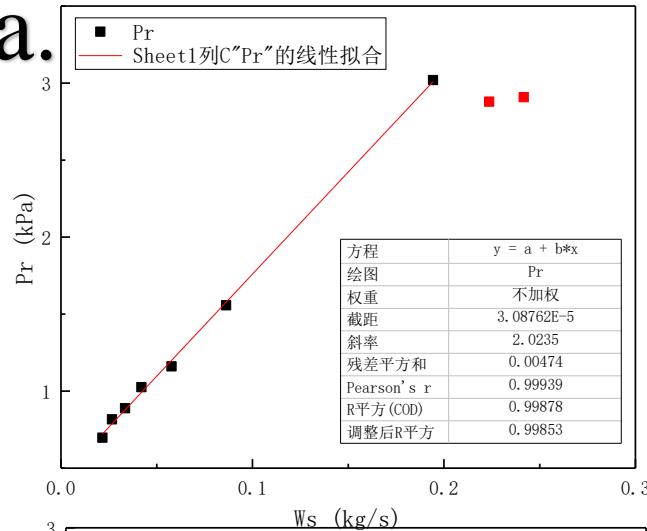




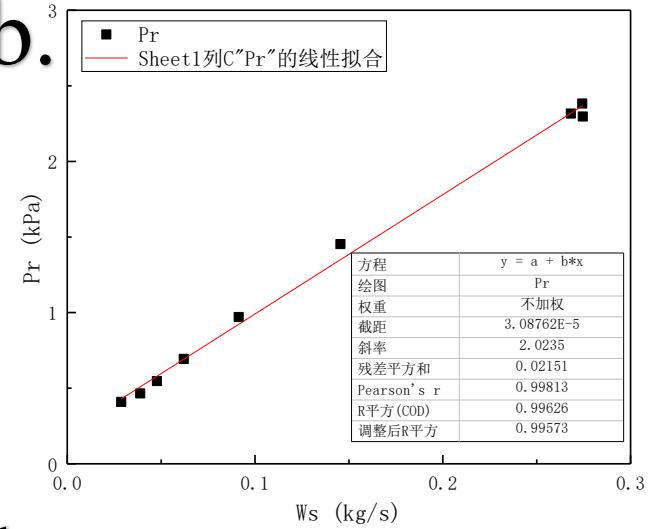
CHINA UNIVERSITY OF PETROLEUM  
胜利油田国家地质实验研究中心

# Results

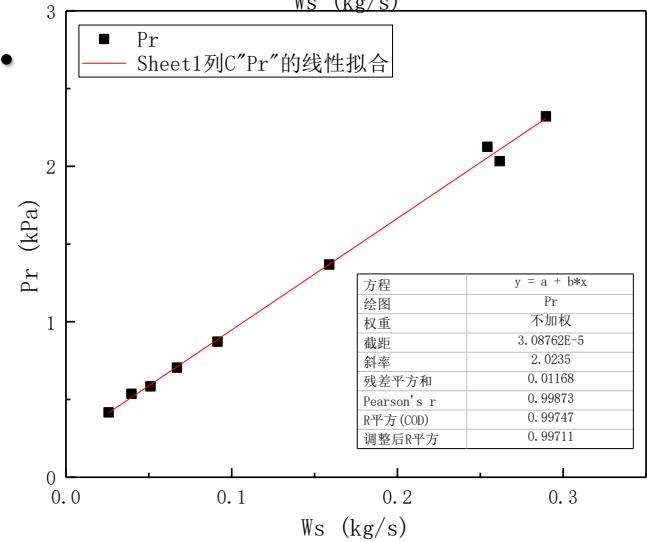
a.



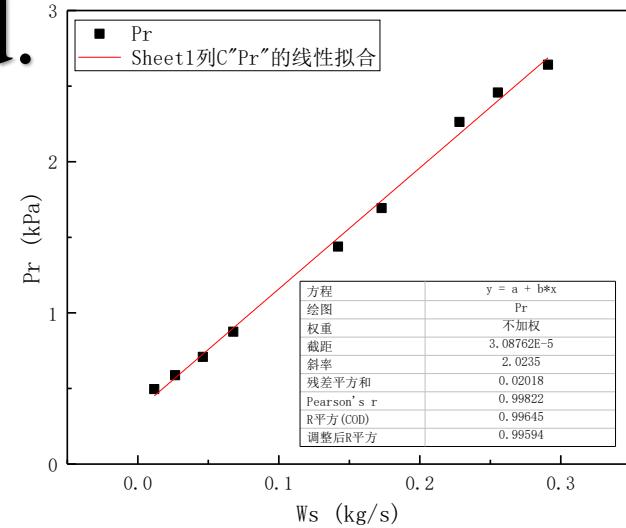
b.



c.



d.



a.  $Q_t=68 \text{ m}^3/\text{h}$ ; b.  $Q_t=68 \text{ m}^3/\text{h}$ ; c.  $Q_t=68 \text{ m}^3/\text{h}$ ; d.  $Q_t=68 \text{ m}^3/\text{h}$ .



# Conclusions

- There is a linear relationship between  $\Delta P_r$  and  $W_s$ , with an intercept of  $f_g$ .

$$\Delta P_r = KW_s + f_g$$

C     • The maximum circulation flux depends on the pressure balance between the material sealing in the moving bed and the riser-spouted bed regenerator;

L     • The real-time monitoring on the circulation flux by the pressure-drop method was accomplished;

S     • The theoretical meaning and accurate definition of the parameters in this correlation need further investigation.

W <sub>s</sub> (kg/s)	$\Delta P_r$ (kPa)			
	68 m <sup>3</sup> /h	98 m <sup>3</sup> /h	128 m <sup>3</sup> /h	158 m <sup>3</sup> /h
	K	13.251	7.890	7.178
0	0.43	0.20	0.23	0.36
0.020	0.70	0.36	0.37	0.52
0.040	0.96	0.52	0.52	0.68
0.060	1.23	0.68	0.66	0.84
0.080	1.49	0.83	0.80	1.00
0.100	1.76	0.99	0.95	1.16
0.120	2.02	1.15	1.09	1.32
0.140	2.29	1.31	1.23	1.48
0.160	2.55	1.46	1.38	1.64
0.180	2.82	1.62	1.52	1.80
0.200	3.08	1.78	1.67	1.96
0.220	3.35	1.94	1.81	2.12
0.240	3.61	2.10	1.95	2.28
0.260	3.88	2.25	2.10	2.44
0.280	4.14	2.41	2.24	2.60
0.300	4.41	2.57	2.38	2.76



中国石油大学  
CHINA UNIVERSITY OF PETROLEUM



## FLUIDIZATION XVI

\*Reporter

E-mail Address: [gaosihong@outlook.com](mailto:gaosihong@outlook.com)