

# The impact of multifunctional additives on $\text{NO}_x$ emissions and bed agglomeration in fluidized bed combustion of biomass

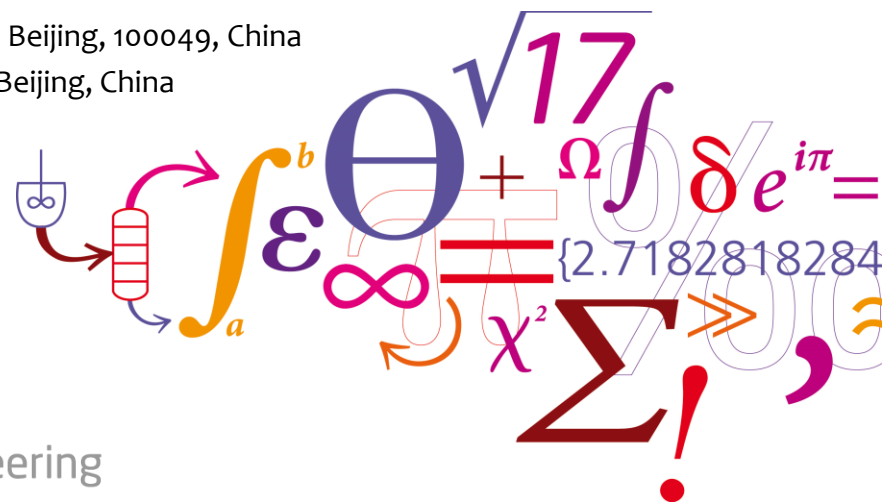
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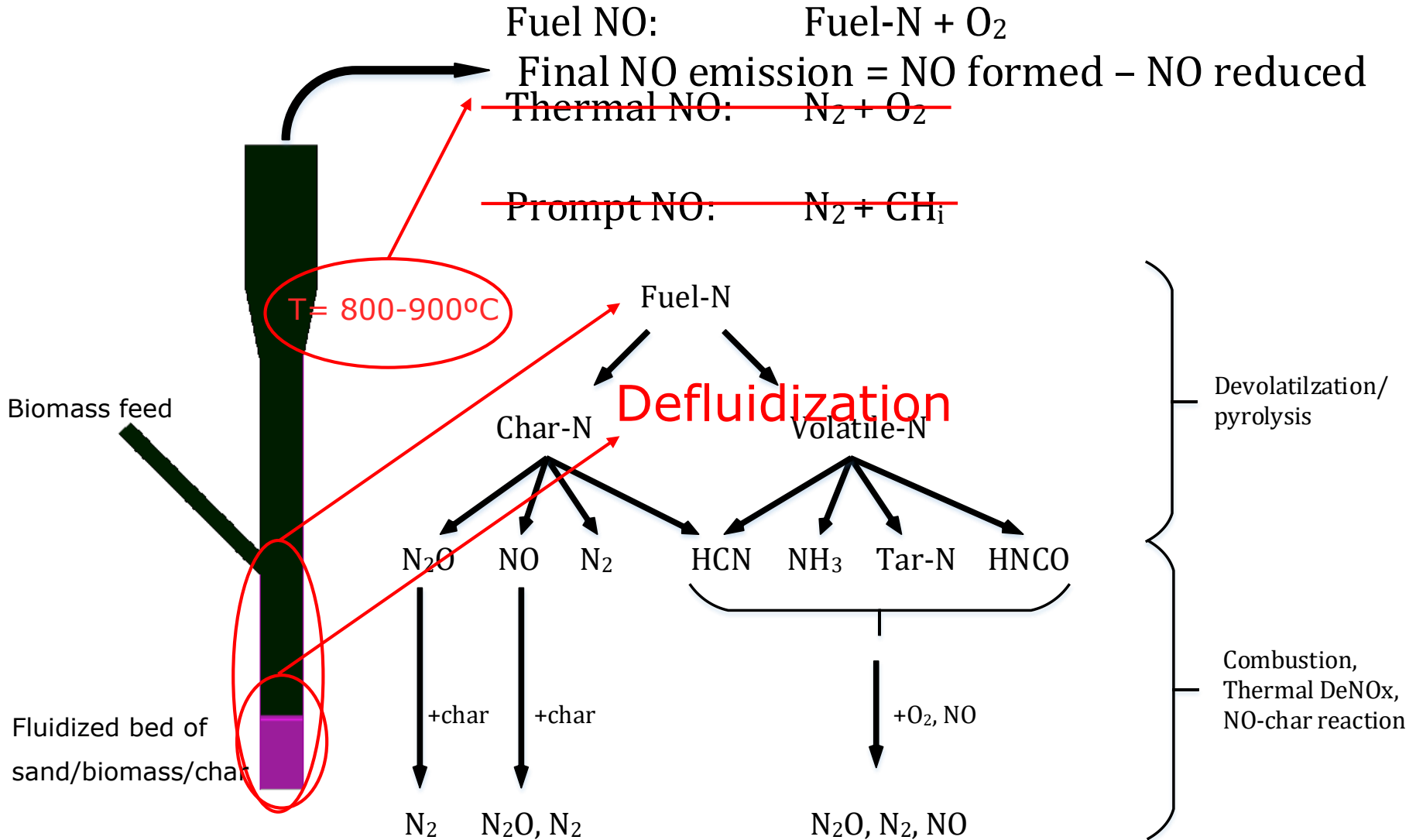
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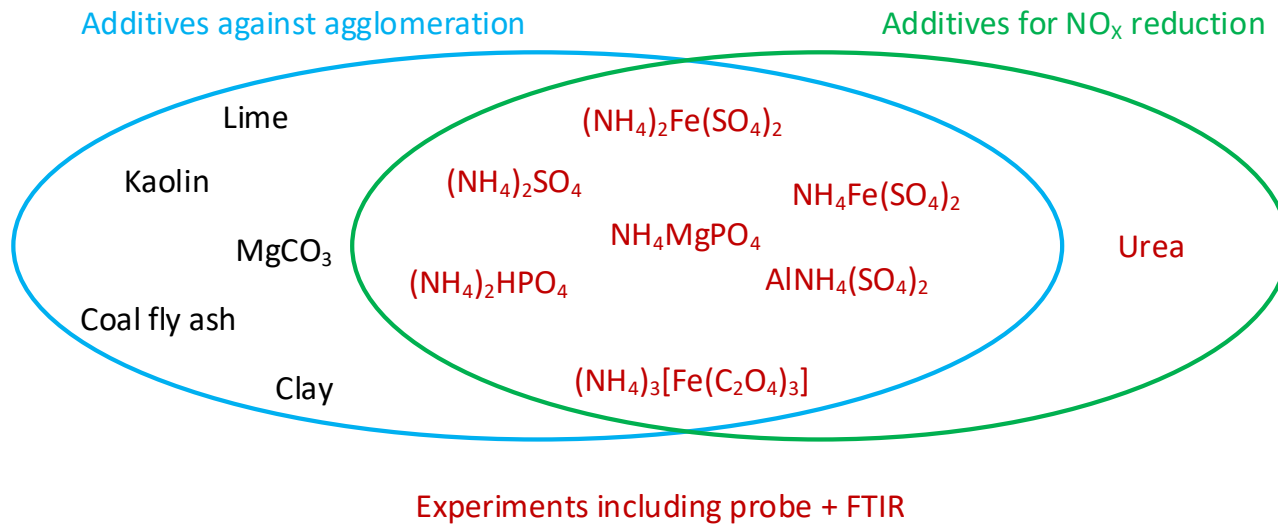


# Brief background



# Objectives

- Investigate the impact of multifunctional additives on  $\text{NO}_x$  emission and bed agglomeration



- Influence of

- Additives:  $\text{NH}_4\text{MgPO}_4$  and  $\text{NH}_4\text{Al}(\text{SO}_4)_2$
- Fuel type: Straw and sunflower husk
- Air staging:  $\lambda_{\text{primary gas}}/\lambda = 1$  and  $0.5$
- Additive particle size:  $(\text{NH}_4)_2\text{SO}_4$ :  $<45$  and  $<106 \mu\text{m}$

# Materials

- Straw dry, pre-mixed with additives
- $\text{NH}_3/\text{fuel-N} = 1.5$
- Additives without  $\text{NH}_4$  functionality: 4.7 g/100g straw

	Unit	Wheat straw
Moisture	% (wb)	12.5
Volatile matter		76.5
Ash		4.6
<b>N</b>		<b>0.69</b>
C	wt% (db)	48.7
H		5.8
O		40.2
Cl		0.18
S		0.08
Al	mg/kg (db)	230
Ca		3600
Fe		180
<b>K</b>		<b>8000</b>
Mg		630
Na		280
P		750
Si		11000
Ti		17

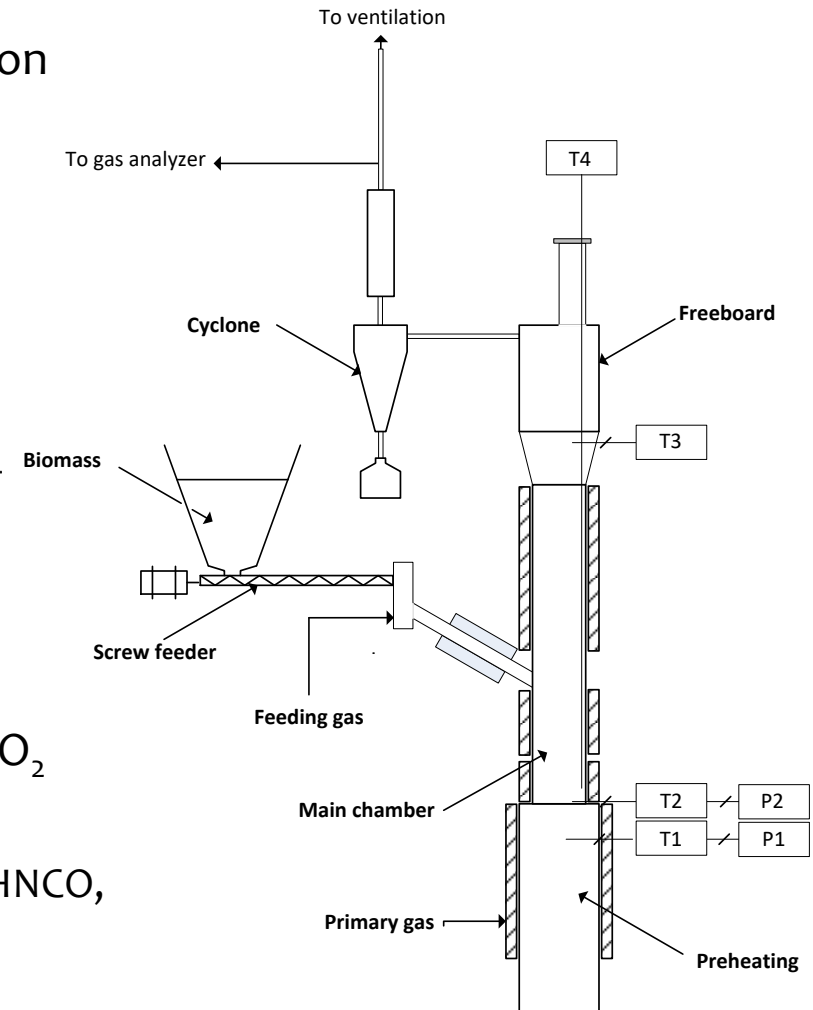
# Experimental setup

- Bubbling fluidized bed reactor for combustion

### Standard conditions

Parameter	Value
Bed temperature	850°C
$u_g/u_{mf}$	4
Primary gas flow	11.5 NL/min air
Feeding gas flow	15.5 NL/min N <sub>2</sub>
Silica sand bed	500 g, 10 cm static bed height, $D_{50}$ 273 $\mu$ m (Geldart B)
Excess air ratio	1.4
Fuel particle size	0.6 – 4 mm
Additive size	<106 $\mu$ m

- Ex-situ gas measurement: NO, CO, CO<sub>2</sub>, and O<sub>2</sub>
- Water cooled sampling probe + FTIR:
  - In situ measurements of: CO, NO, NO<sub>2</sub>, NH<sub>3</sub>, H<sub>2</sub>CO, N<sub>2</sub>O etc.



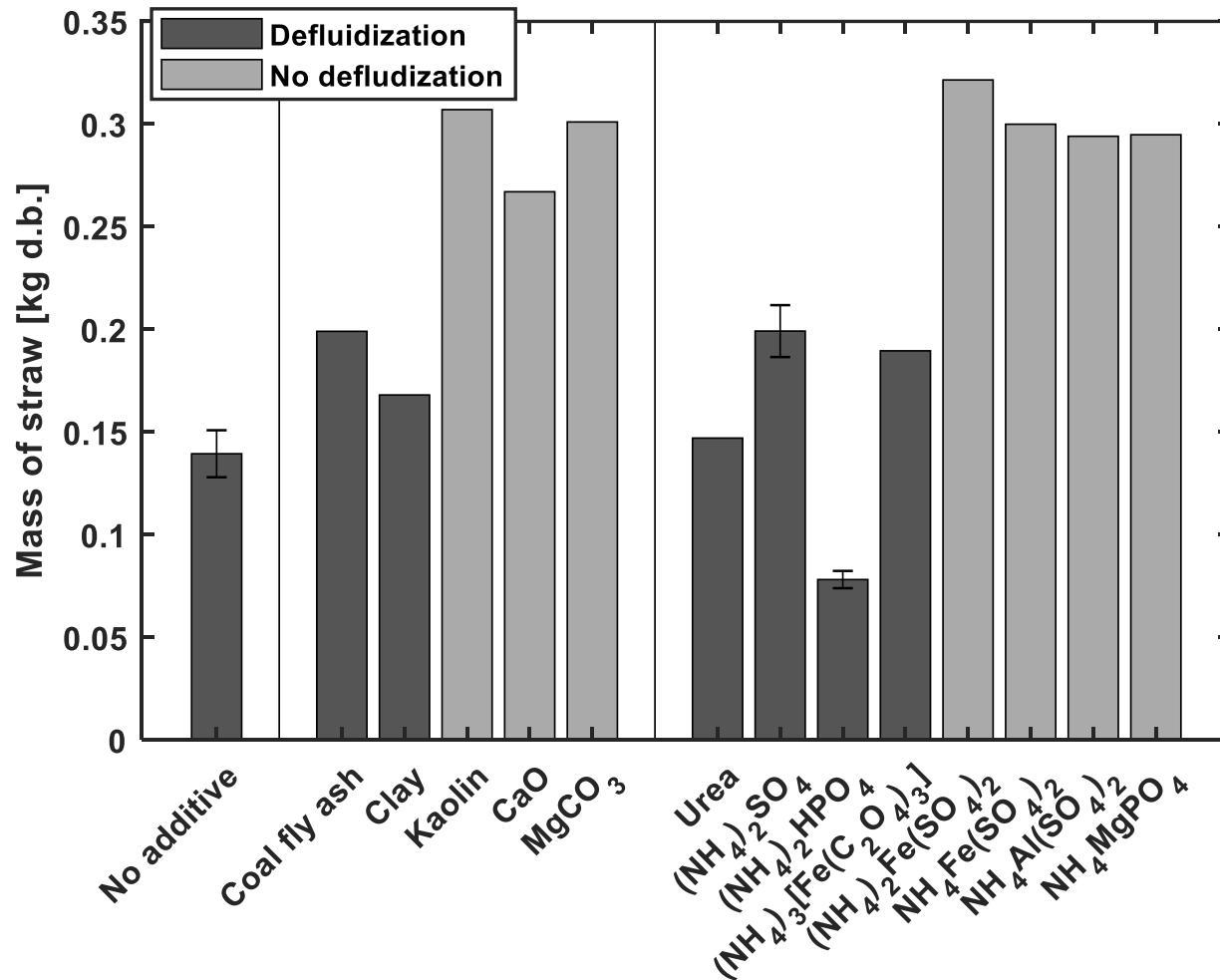
# Example video – straw combustion

Initial

Defluidization

Steady state

# Defluidization tendency – straw, unstaged



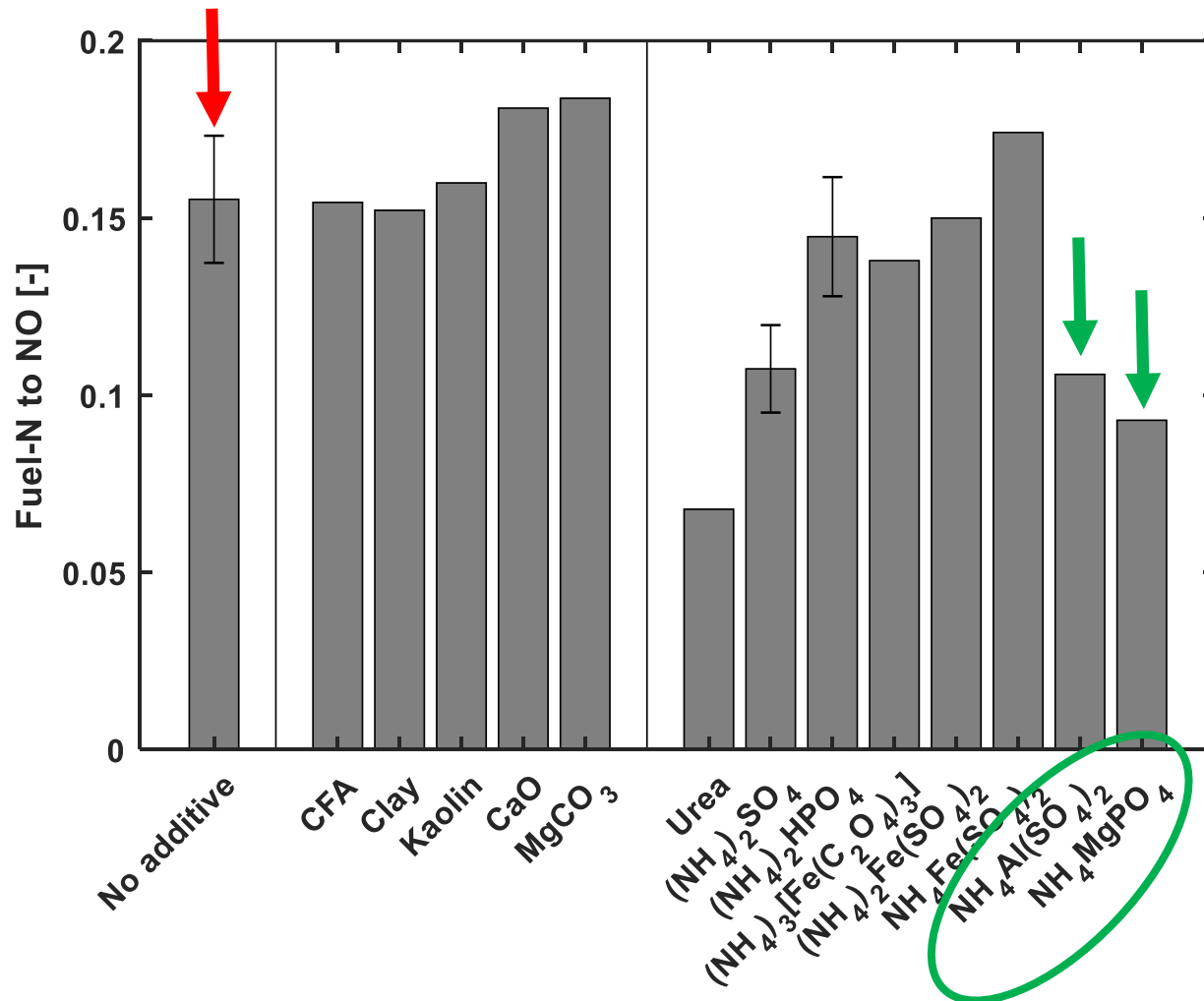
➤ NH<sub>4</sub> based additives that prevent defluidization

- (NH<sub>4</sub>)<sub>2</sub>Fe(SO<sub>4</sub>)<sub>2</sub>
- NH<sub>4</sub>Fe(SO<sub>4</sub>)<sub>2</sub>
- NH<sub>4</sub>Al(SO<sub>4</sub>)<sub>2</sub>
- (NH<sub>4</sub>)<sub>2</sub>MgPO<sub>4</sub>

➤ Metal additives that prevent defluidization

- Kaolin
- CaO
- MgCO<sub>3</sub>

# Fuel-N to NO – straw, unstaged



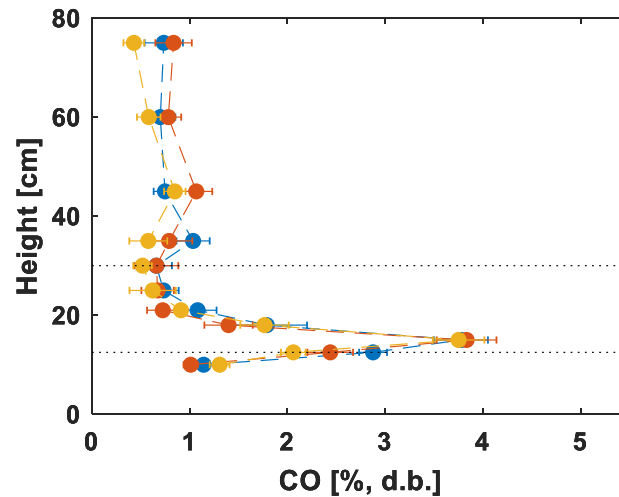
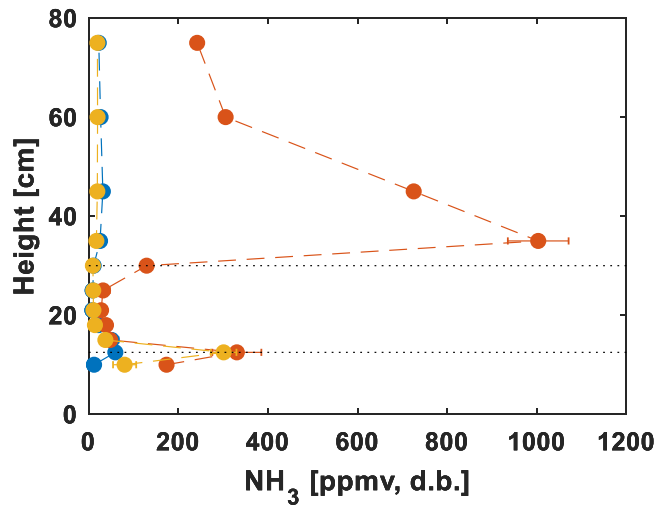
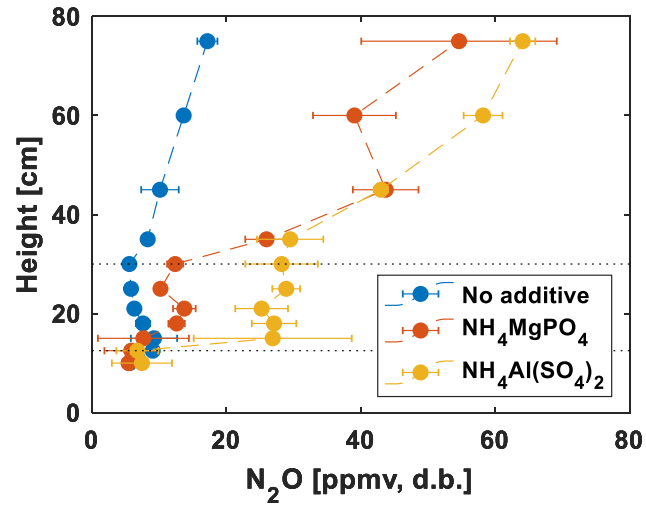
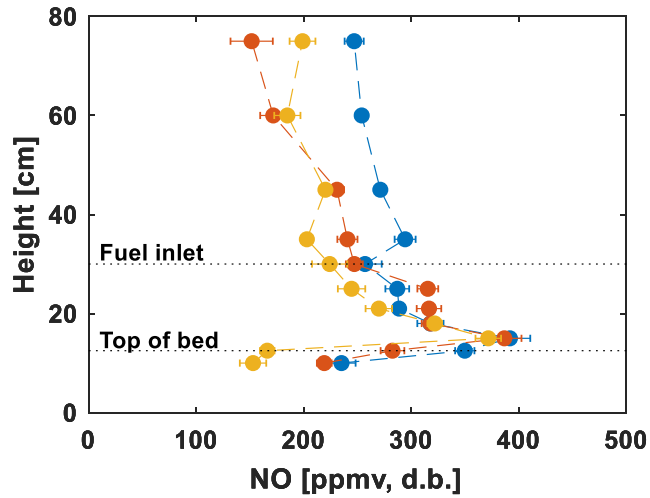
➤ NH<sub>4</sub> salt necessary to reduce conversion of fuel-N to NO

➤ Additives that reduce fuel-N to NO conversion and prevent defluidization

- NH<sub>4</sub>Al(SO<sub>4</sub>)<sub>2</sub>
- NH<sub>4</sub>MgPO<sub>4</sub>



# Concentration profiles



➤ NO and CO peaks and declines in the freeboard

- Reduction primarily by  $\text{CH}_i$  and CO

➤ Inhomogeneous distribution in bed

- Turnover of fuel

➤  $\text{NH}_3$  release from additives → Thermal De $\text{NO}_x$

- Above fuel feeding
- Top of bed

➤ Explanations for increase in  $\text{N}_2\text{O}$

- $\text{NH}_i + \text{NO}/\text{NO}_2$
- Other gaseous compounds (HCN not measured)

# Conclusions

- $\text{NH}_4$  salts can influence **both agglomeration tendency and  $\text{NO}_x$  chemistry** when dry mixed with fuel during continuous fluid bed combustion
- $\text{NH}_4\text{MgPO}_4$  and  $\text{NH}_4\text{Al}(\text{SO}_4)_2$  **prevented defluidization and reduced the conversion of fuel-N to NO** during **straw combustion**
- $\text{NH}_4\text{MgPO}_4$  and  $\text{NH}_4\text{Al}(\text{SO}_4)_2$  released  $\text{NH}_3$  above the fuel inlet and/or the fuel bed, thereby reducing NO by **thermal DeNO<sub>x</sub>**

# Questions and suggestions are most welcome

